

## **Commonwealth of Massachusetts**

## **Manufactured Buildings Program**

Transmittal Form for all correspondences relating to Manufactured Buildings and Building Components

To: Linda McAlister factured Buildings Program Phone Number: Date Transmitted											
Linda.McAlister e.ma.us	5	508-422-1955 7/12/17									
Commonwealth of Massachuse	tts		D	Department of Public Safety							
Board of Building Regulations a	50	50 Maple Street, Suite One									
Milford	М	lass	sachuse	etts		01757	7-3698				
The person forwarding this mate	erial shall d	complete the fol	lowi	ng	portion	of this	transmittal				
Name of Person Brett He		MC Number TPIA N					A Numb	er			
Transmitting Material				352				02			
The following information is being to and Standards and / or the Departm (Please check the appropriate box items under the section labeled others.)	ons of the	deta e tra	ailed be	low d	Please indic Model and / Number per transmitted	or Seri taining	al	_	se oup		
Building Plans for Review and App											
Building Plans forwarded as a record copy for your files (Review not required)							ON#6861			R-3	
Revised building plans for review. (Please clearly identify revisions on the plans.)											
Revised Building Plans forwarded as a record copy for your files (Review not required - Please clearly identify revisions on the plans.)											
Compliance Assurance Programs	Original	Submission		M	lodificati	ion to:	1				
Calculations Manual	Original	Submission		M	lodificati	ion to:					
Installation Manual	Original	Submission		M	lodificati	ion to:					
Systems Drawings	Original	Submission		M	lodificati	ion to:					
Other - Provide a detailed description of any other materials which are being transmitted. Identify any revisions clearly along with BBRS number. Also, identify the requested action.											
Site Location: 10 HARBOR WAY, POCASSET, Ma 02559 (BARNSTABLE COUNTY)											
The office transmitting this information has reviewed the above mentioned and attached materials and has found them, to the best of our knowledge and abilities, to be in compliance with the codes and \ or rules and regulations for the Commonwealth of Massachusetts' Manufactured Building Program, as applicable											
Signed By for TPIA:		BBRS No: as	ssigr	ned	by Ma		Signed By for MASS:				

**Print Form** 

HEET#	DRAWING INDEX  DESCRIPTION								
CV CV	COVER SHEET								
EV1	FRONT ELEVATION		ASSIFICATION						
EV2	REAR ELEVATION	OCCUPANT LOAD:	SINGLE FAMILY						
EV3	LEFT ELEVATION	USE GROUP:	R-3						
EV4	RIGHT ELEVATION	CONSTRUCTION TYPE:	VB WOOD FRAME UNPROTECTED						
FP1	1ST STORY FLOOR PLAN	CONSTRUCTION TIFE.	VB WOOD FRAME ONFROTECTED						
FP2	2ND STORY FLOOR PLAN								
SW1	1ST STORY SHEAR WALL PLAN	D	ESIGN LOADS						
SW2	2ND STORY SHEAR WALL PLAN	ROOF LIVE LOAD:	30 PSF GSL						
EL1	1ST STORY ELECTRICAL PLAN	ROOF DEAD LOAD:	10 PSF						
EL2	2ND STORY ELECTRICAL PLAN	CEILING DEAD LOAD:	10 PSF						
ELC	ELECTRICAL LOAD CALCS	CEILING LIVE LOAD:	20 PSF (STORAGE) / 30 PSF (HABITABLE)						
CS	CIRCUIT SCHEDULE	FLOOR LIVE LOAD:	40 PSF						
FND	FOUNDATION PLAN	FLOOR DEAD LOAD:	10 PSF						
TR1	12/12 RAFTER	HORIZONTAL WIND LOAD:	110 MPH @ 3 SEC GUST						
TR2	12/12 RAFTER CONNECTIONS	EXPOSURE:	C						
	·	GROUND SNOW LOAD:	30 PSF						
TR3	4.5/12 SHED RAFTER CONNECTIONS	SEISMIC CATEGORY:	В						
R4	4.5/12 SHED RAFTER CONNECTIONS								
TR5	4.5/12 RAFTER	APP	LICABLE CODES						
TR6	4.5/12 RAFTER CONNECTIONS	MA 1802 FAMILY DWELLIN	NG CODE -(780 CMR) 8TH EDITION						
R7	12/12 RAFTER	MA FUEL/GAS/PLUMBING	G (248 CMR)						
R8	S/L HEADER DETAIL	2009 INTERNATIONAL ME	ECHANICAL CODE W/ MA AMENDMENTS						
SE1	12/12 CROSS SECTION		NATIONAL ELECTRICAL CODE W/ MA AMENDMENTS INTERNATIONAL ENERGY CONS. CODE W/ MA AMENDMENTS						
E2	4.5/12 SHED CROSS SECTION		· · · · · · · · · · · · · · · · · · ·						
SE3	4.5/12 CROSS SECTION								
SE4	HIGH WIND SECTION								
SE5	HIGH WIND FASTENING	INSU	JLATION VALUES						
OWS	DOOR AND WINDOW SCHEDULE	ROOF TO EXTERIOR:	R-38						
PL1	PLUMBING DETAILS	EVERNOR WAY OF TO THE							
PL2	PLUMBING DETAILS	EXTERIOR WALLS TO EXTER	RIOR: R-21 HIGH DENSITY						
PL3	PLUMBING NOTES	FLOOR TO BASEMENT OR (	CRAWL SPACE: R-30 (ON-SITE)						
HL1	1ST STORY HEATLOSS	. ESS S Bridging III Off							
HL2	2ND STORY HEATLOSS								
ILZ	RES CHECK								
	HIGH WIND CALCS		ARE DESIGNED TO BE USED						
	RAFTER CALCS	HOUSING UNITS. ACCORDANCE WIT PACKAGE AND TI	RUCTION OF FACTORY BUILT THESE UNITS ARE DESIGNED IN TH THE APPROVED SYSTEMS HE APPLICABLE STATE AS LISTED ABOVE ON THIS						
		SET. THE CSL ON RE LOCAL BUILDING AUT HAVE BEEN CONCEAL BUILDING OFFICIAL M REMOVAL OF ELEMEN CONNECTIONS TO PR	A 48 HOUR NOTIFICATION IS REQUIRED PRIOR TO THE SET. THE CSL ON RECORD WILL RELAY THIS TO THE LOCAL BUILDING AUTHORITY. IF ANY CONNECTIONS HAVE BEEN CONCEALED PRIOR TO INSPECTION, THE BUILDING OFFICIAL MAY REQUEST HAVING THE REMOVAL OF ELEMENTS THAT CONCEAL THE CONNECTIONS TO PROVIDE ACCESS. THIS WOULD NOT CONSTITUTE DESTRUCTIVE DISSASSEMBLY". ALL						

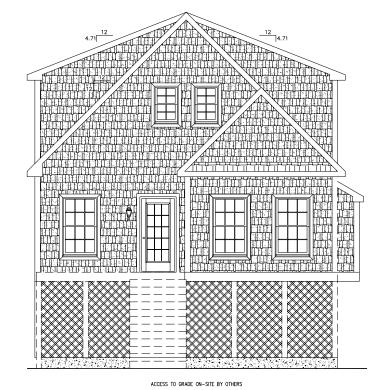


Custom Modular Homes, LLC

Icon - Legacy Custom Modular Homes, LLC

> 246 SAND HILL ROAD SELINSGROVE, PA 17870 PHONÉ 570-374-3280 FAÝ 570-374-1122 WWW.ICONLEGACY.COM

O#6861 FOUR BOX CAPE



FRONT ELEVATION

R.A. AND P.E. STAMP

## PFS CORPORATION Approval Limited to Factory Built Portion Only

State: Signature: Title: Massachusetts

\*\*Marold Raup\*\*
Staff Plan Reviewer

Date:

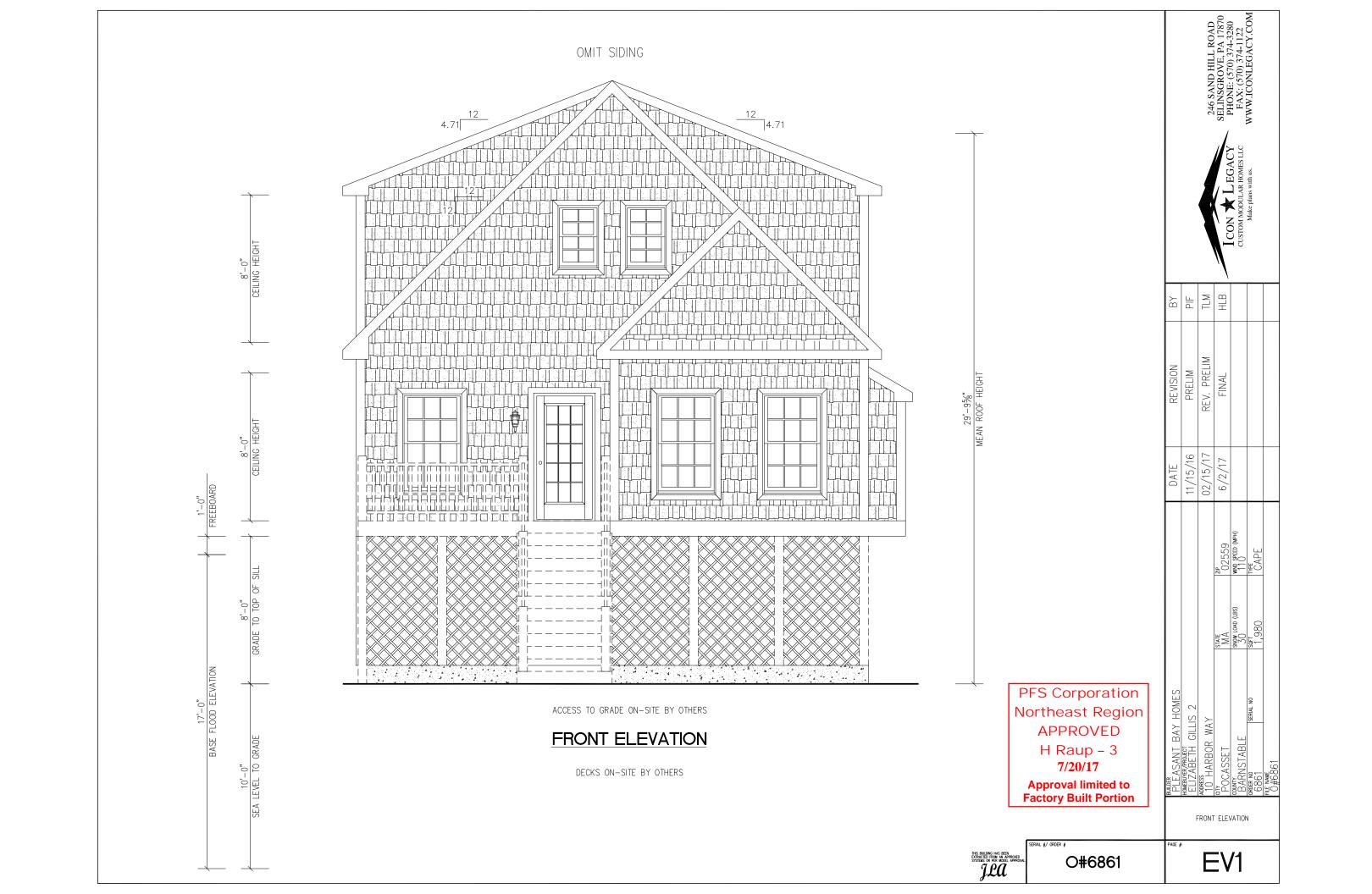
taff Plan Revier 7/20/17

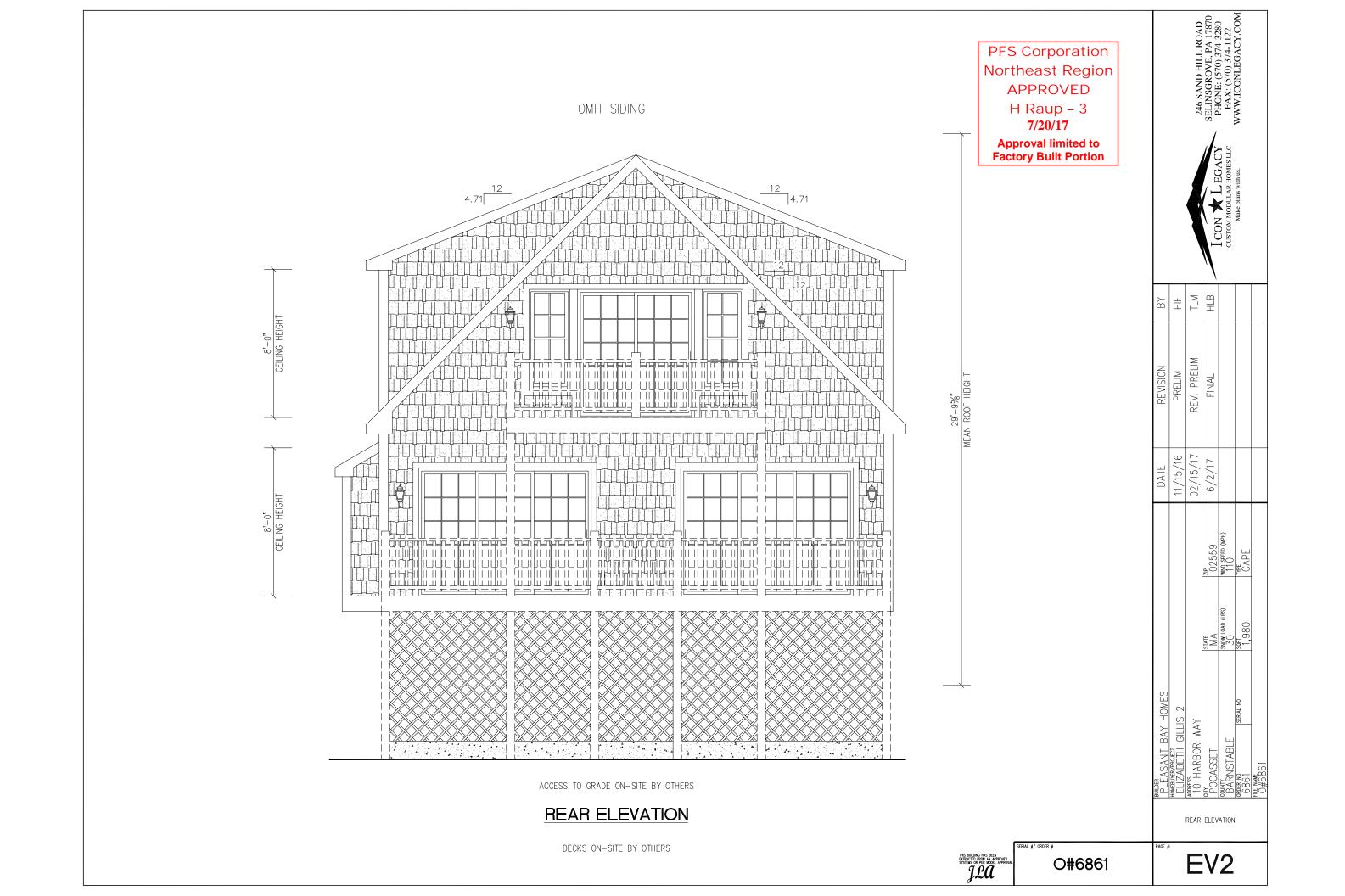
COVER PAGE

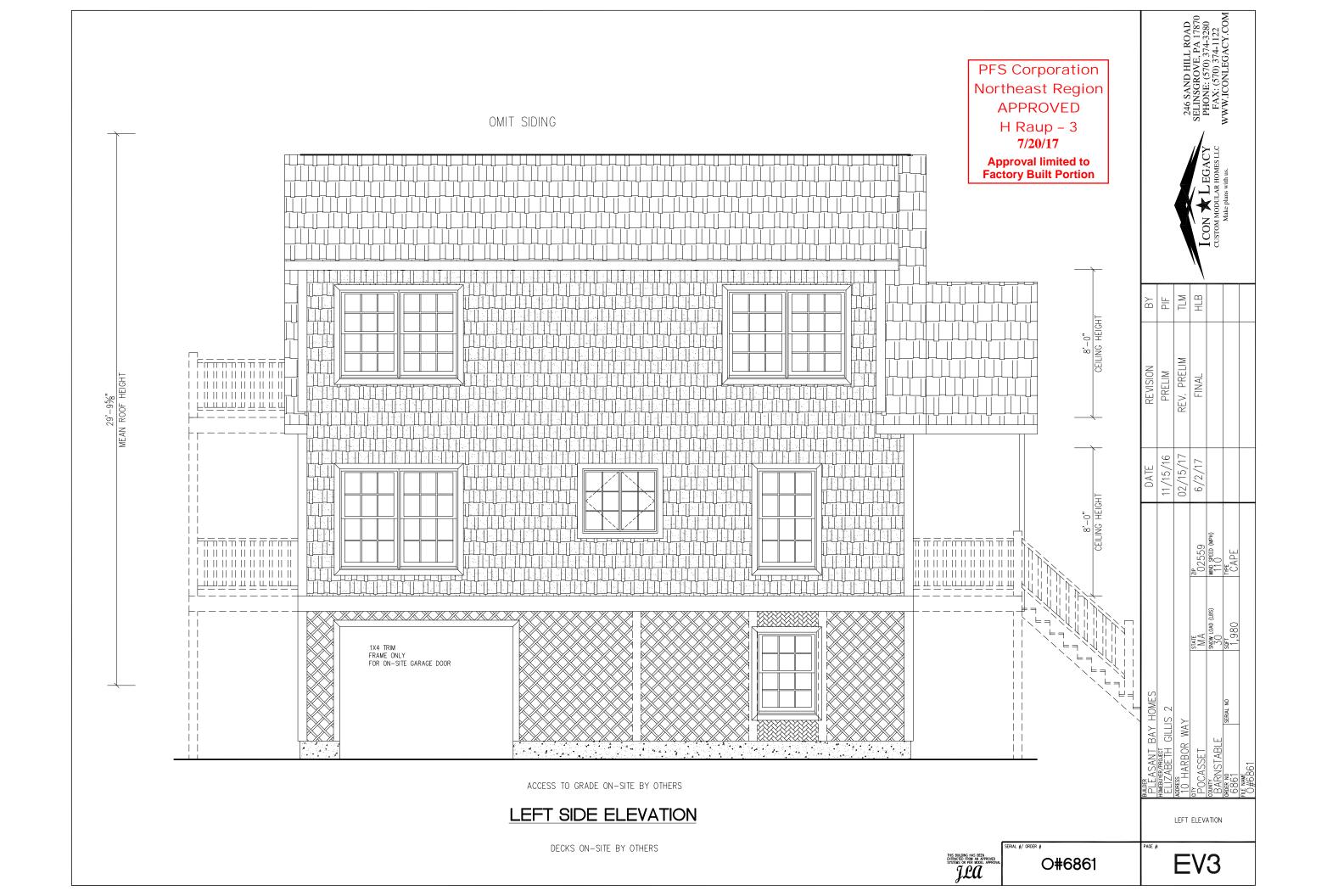


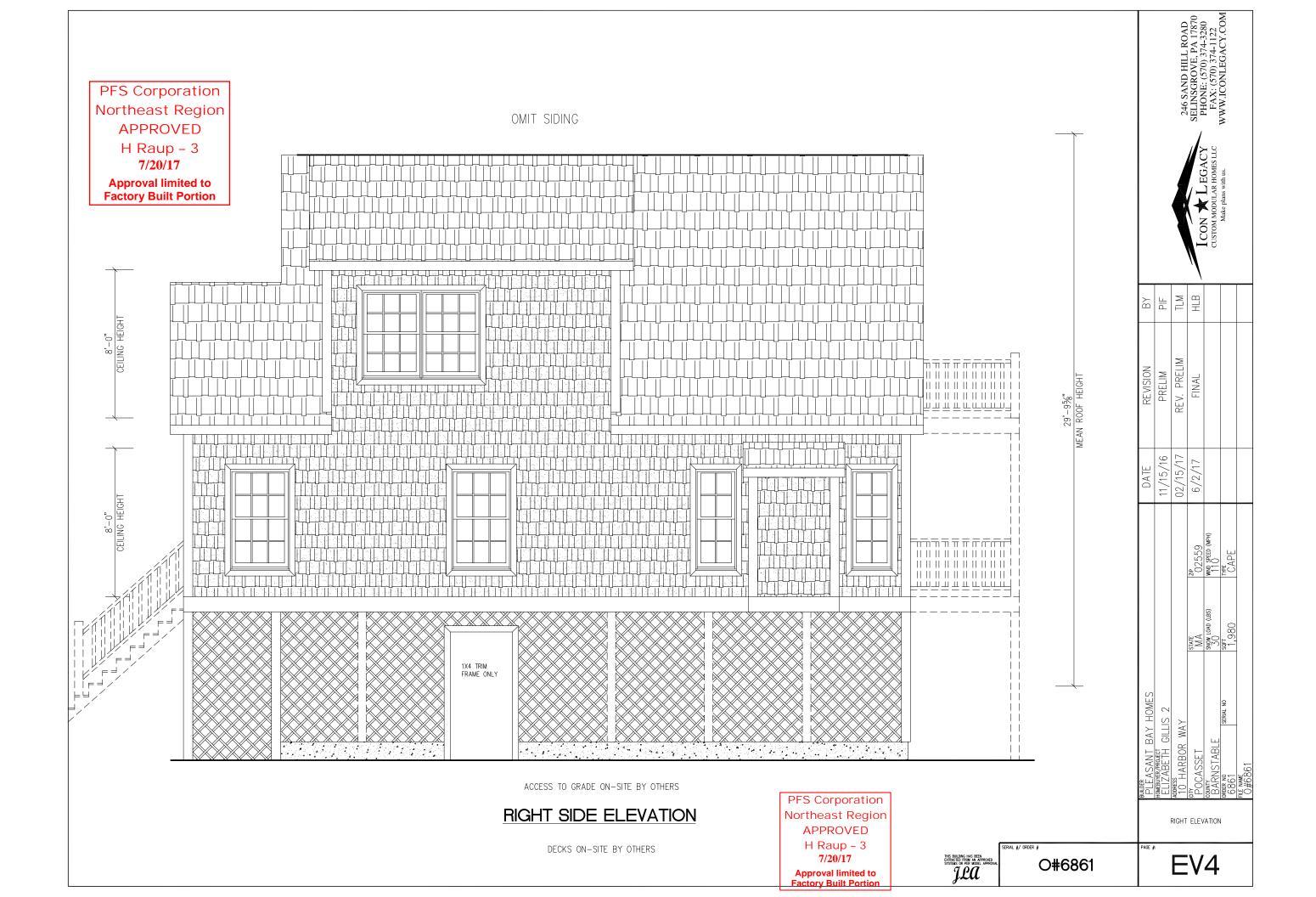
O#6861

CV









A 48 HOUR NOTIFICATION IS REQUIRED PRIOR TO THE SET. THE CSL ON RECORD WILL RELAY THIS TO THE LOCAL BUILDING AUTHORITY \*TEMPERATURE CONTROL VALVE TO BE INSTALLED TO ALL TUBS AND SHOWERS SITE ADDRESS IF ANY CONNECTIONS HAVE BEEN CONCEALED PRIOR TO INSPECTION, THE BUILDING OFFICIAL MAY REQUEST HAVING THE REMOVAL OF 10 HARBOR WAY \*BUILDER IS RESPONSIBLE TO COMPLY WITH R612.2 (WINDOW SILLS) OF THE 2015 IRC (DONE ON-SITE IF APPLICABLE) POCASSET, MA 02559 ELEMENTS THAT CONCEAL THE CONNECTIONS TO PROVIDE ACCESS. THIS WOULD NOT CONSTITUTE "DESTRUCTIVE OF THE 2013 INC. (UDNE ON-SITE IF APPLICABLE)

--WHERE THE OPENING OF AN OPERABLE WINDOW IS LOCATED MORE THAN

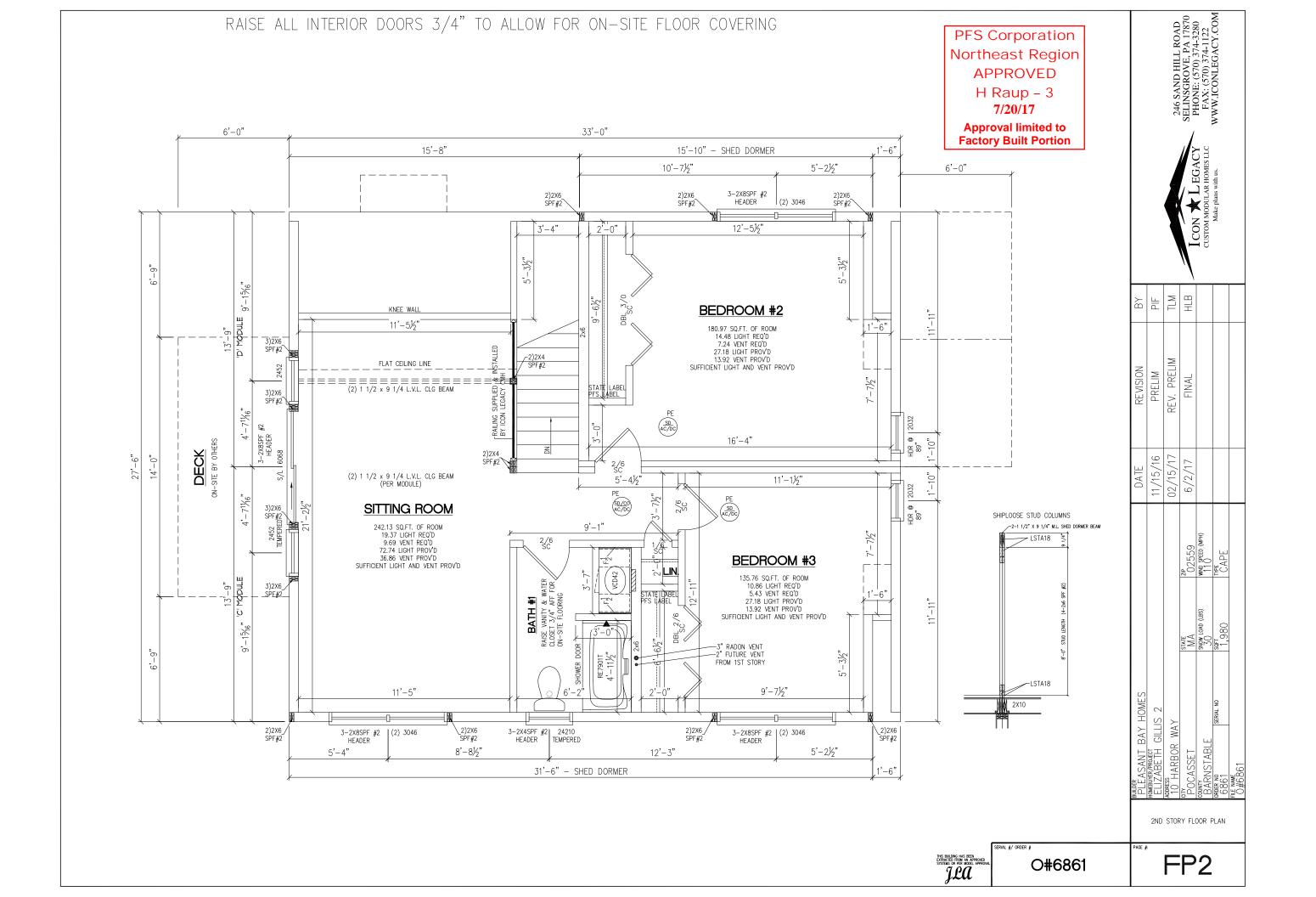
72 INCHES ABOVE THE FINISHED GRADE OR SURFACE BELOW

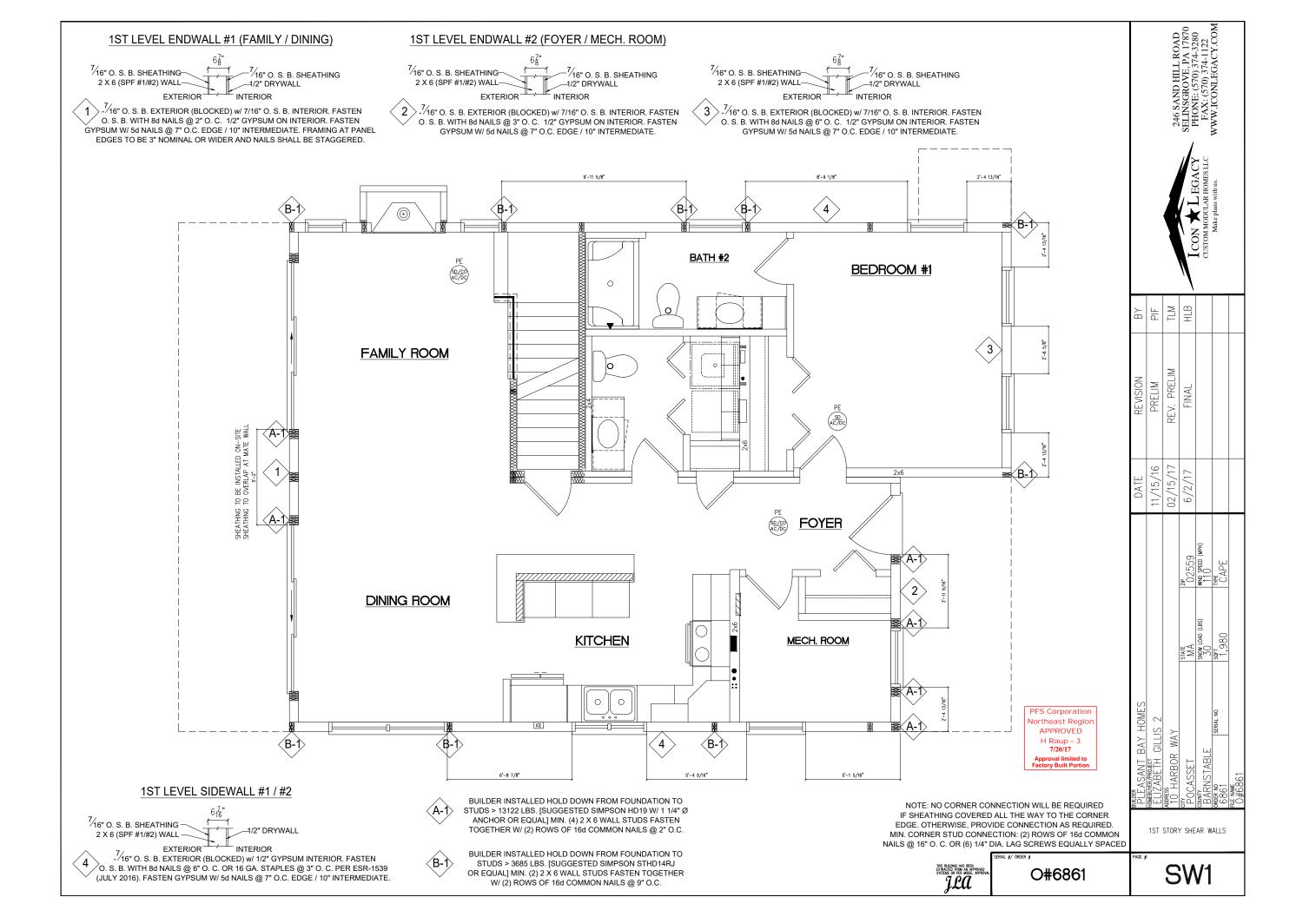
--WHERE THE LOWEST PART OF THE CLEAR OPENING OF THE WINDOW SHALL BE A MINIMUM

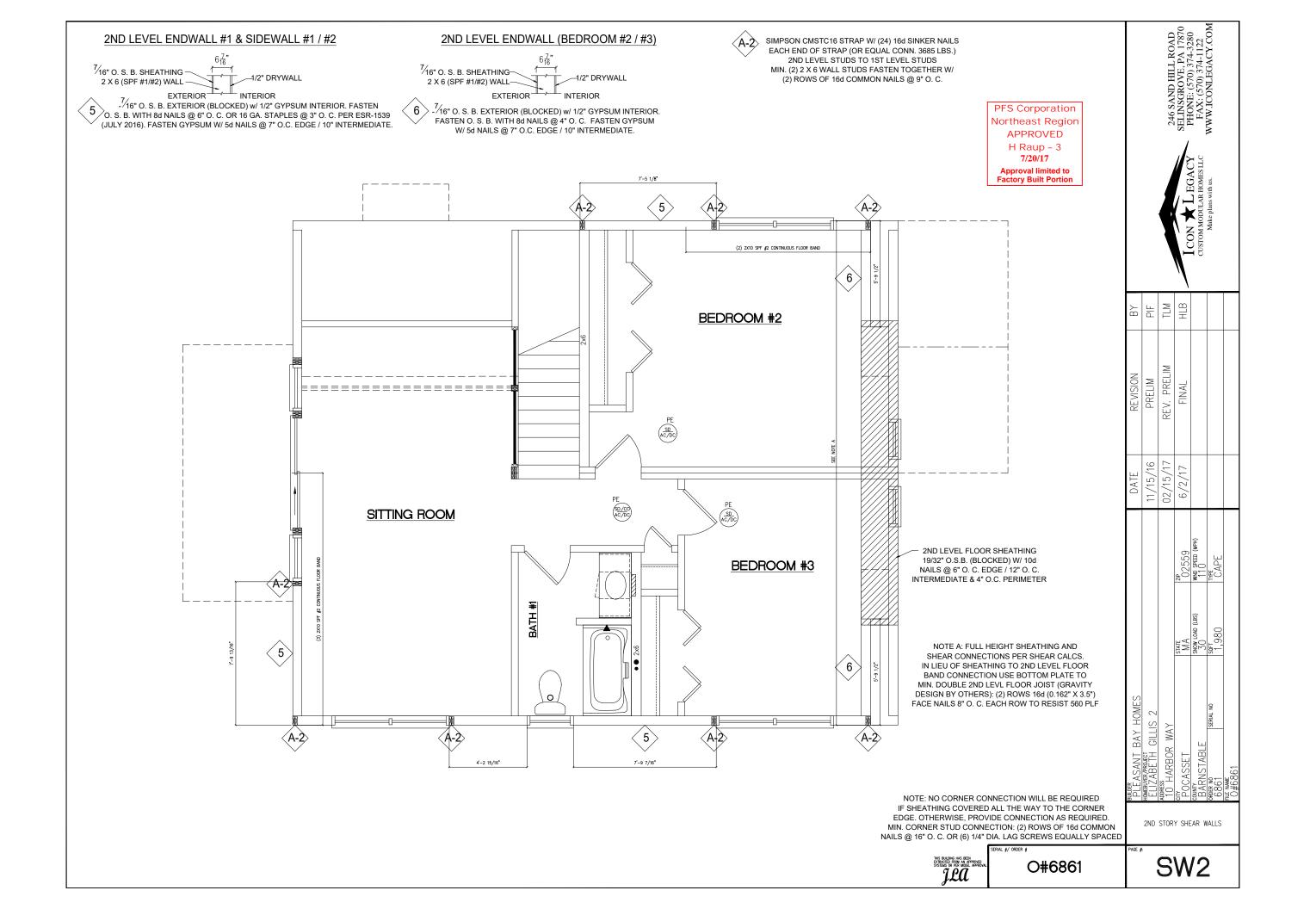
OF 24 INCHES ABOVE THE FINISHED FLOOR OF THE ROOM IN WHICH THE WINDOW IS LOCATED

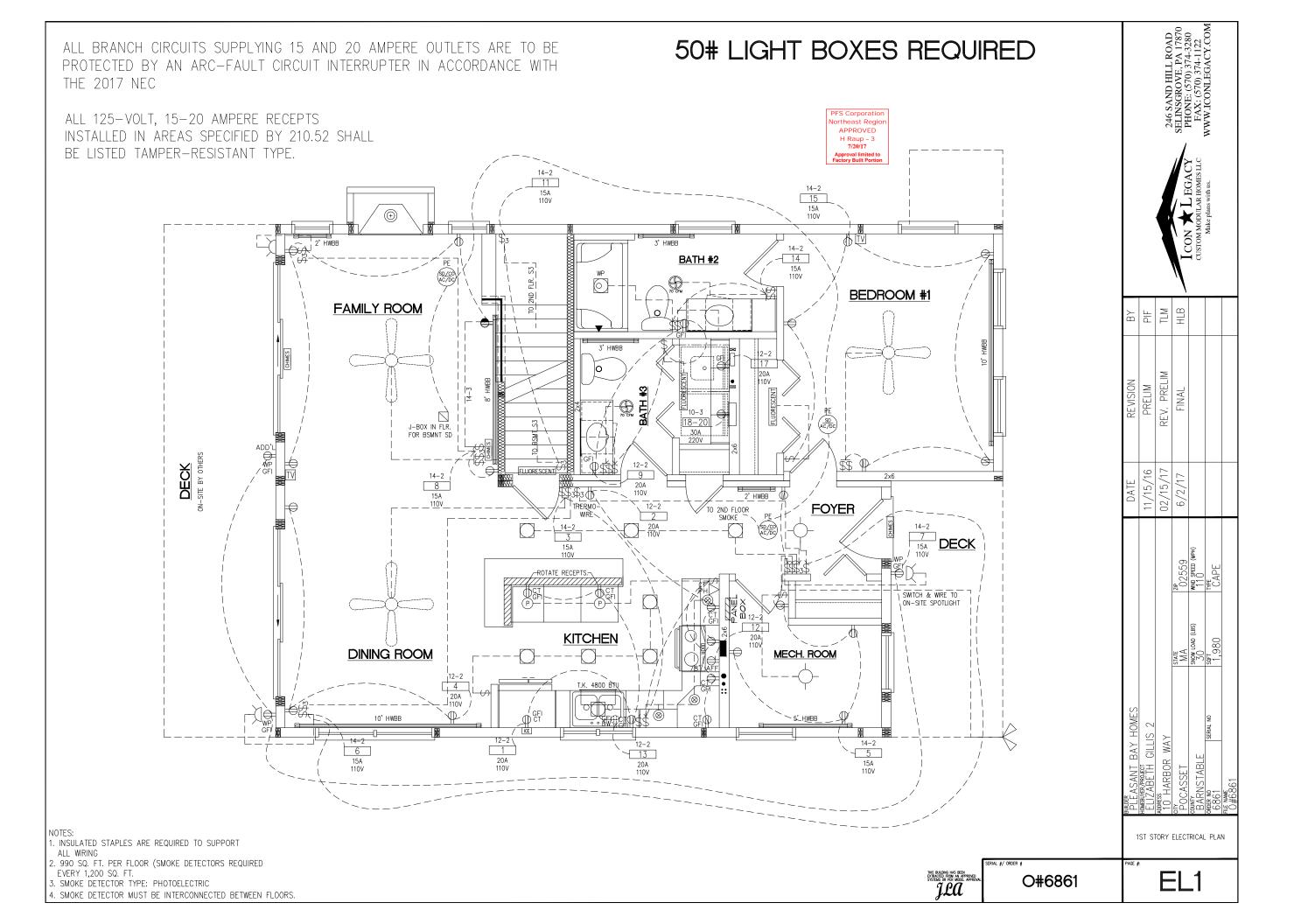
--OPERABLE SECTIONS OF WINDOWS SHALL NOT PERMIT OPENINGS THAT ALLOW PASSAGE OF A

4 INCH DIAMETER SPHERE WHERE SUCH OPENINGS ARE LOCATED WITHIN 24 INCHES OF THE FINISHED FLOOR BUILDER: DISSASSEMBLY". ALL CONNECTIONS ON SITE MUST BE INSPECTED BY THE LOCAL AUTHORITY. 256 PLEASANT BAY ROAD BUILDER TO INSTALL & SUPPLY WHOLE HOUSE VENTILATION & TO ALL CEILING GYP MUST BE MECHANICALLY FASTENED HARWICH, MA 02645 BE APPROVED & INSPECTED ON-SITE BY LOCAL BUILDING OFFICAL THIS HOUSE IS NOT LOCATED IN A FLOOD ZONE DUCT TIGHTNESS AND BLOWER DOOR TESTING DRYER SHOWN TO BE ELECTRIC. IF A GAS DRYER IS SUBSTITUTED ON-SITE IT MUST BE LISTED AS BATHROOM USE (Q2406) DONE ON-SITE BY BUILDERS' HERS RATER 5'-0" 45'-0" 6'-0" 39'-0" ON-SITE SHOWER 30'-6"  $\mathop{L_{\mathrm{EGAC}}}$ car homes i PANELIZED WALLS 1'-11½" .1'-10½ 11'-11½" 12'-8" COVERING 2)2X6 3-2X6SPF #2 3-2X6SPF #2 -2X4SPF #2 2)2X6 HEADER 3052 HEADER 2052 HEADER TEMPERED HEADER TEMPERED SPF#2 SPF#2 SPF#2 HEADER 4'-63/4"  $10'-6\frac{3}{4}'$ 11'-3" 4)2X6 SPF#2 BATH #2 RAISE VANITY & WATER CLOSET 3/4" AFF FOR FLOOR HEATILATOR FIREPLACE MODEL# NDV4236IL BEDROOM #1 LANDING ON-SITE FLOORING SURROUND ON-SITE BY OTHERS FIREPLACE AND FLUE 0 11.48 LIGHT REQ'D 5.74 VENT REQ'D BY ICON LEGACY CMH VLC15 84 w/ 36.09 LIGHT PROV'D 20.01 VENT PROV'D VCD42 SITE VLSK15 SUFFICIENT LIGHT AND VENT PROV'D **FAMILY ROOM**  $\leq$ ≥∘ REVISION PRELIM EV. PREL FINAL FOR **₽** ВАТН COMBINED LIGHT, VENT & AREA FOR FAMILY/DINING Δ AC/DC MO292.60 SQ.FT. OF ROOM 23.41 LIGHT REO'D 11.70 VENT REO'D  $\forall \exists \exists$ 4)2X6 123.70 LIGHT PROV'D SPF#2 50.56 VENT PROVID 3'-4" PAN. SUFFICIENT LIGHT AND VENT PROV'D DECK SITE BY OTHE 29, 2)2X6 SPF#2 11/15/16 SPF#2  $\bigcirc$ 2/6 SC W/SWEEP 2/0 SC 2) 1 1/2" x 9 1/4" L.V.L. (PER SIDE) 9 4)2X6 SPF#2 4 **FOYER**  $\sim$ 6'-3½" DOORS 45" HIGH WALL 36" BARTOP PANEL BACKER DECK 4'-7½" TREATED PORCH FLOOR INTERIOR B24 2ST B24 2ST **DINING ROOM** w/ 5/4 DECKING 4)2X6 KITCHEN MECH. ROOM MAA SNOW L § 82 € -WTDR09 \_ROUGH PLUMB. SUPPLY LINES 3" DRAIN FROM  $\leq$ UTK22 ONLY SPACE 2- 3/4" SUPPLIES SE 11'-0½" 0 WR3612 4)2X6\_ SPF#2 W2430  $\overline{\triangleleft}$ =0=  $^{
m J}_{
m ALL~HWBB~LINES}$   $^{
m J}$ 3-2X6SPF #2 | C235 | DATA PLATE, STATE | Z2)2X6 HEADER | C235 | DATA PLATE, STATE | Z2)2X6 & PFS LABEL LOC'N. SPF#2 3-2X10SPF #2 | (2) 3052 3-2X6SPF #2|3052 RUN TO THIS AREA HEADER SPF#2 FOR ON-SITE TIE IN TO Northeast Regio BOILER SYSTEM 17'-3½" 26'-3½" 5'-4" APPROVED H Raup - 3 NOTES: 2x10 SPF#2 P.T. FLOOR JOIST @ 16" O.C. w/APPROVED FASTENERS FOR P.T. LUMBER 7/20/17 EXTERIOR WALLS @ 16 O.C. Approval limited to Factory Built Portion FLOOR TO BE CONSTRUCTED IN ACCORDANCE 2. 2X4 MARRIAGE WALLS @ 16 O.C. WITH R502 INCLUDING TENSION DEVICE 3. 8'-0" CEILING HEIGHT 1ST & 2ND FLOORS MA STATE BUILDING CODE -(780 CMR) 8TH EDITION 4. ANDERSEN 400 TILT WASH DOUBLE HUNG WINDOWS 1ST STORY FLOOR PLAN MA FUEL/GAS/PLUMBING (248 CMR) 5. 48,000 TOTAL BTU HEAT LOSS 2009 INTERNATIONAL MECHANICAL CODE W/ MA AMENDMENTS 6. RAFTERS: 2017 NATIONAL ELECTRICAL CODE W/ MA AMENDMENTS FP1 - 12/12 STORAGE RAFTER @ 16 O.C. O#6861 2015 INTERNATIONAL ENERGY CONS. CODE W/ MA AMENDMENTS - 5/12 NON-STORAGE RAFTER @ 16 O.C.









ALL BRANCH CIRCUITS SUPPLYING 15 AND 20 AMPERE OUTLETS ARE TO BE PROTECTED BY AN ARC-FAULT CIRCUIT INTERRUPTER IN ACCORDANCE WITH THE 2017 NEC

50# LIGHT BOXES REQUIRED

ALL 125-VOLT, 15-20 AMPERE RECEPTS INSTALLED IN AREAS SPECIFIED BY 210.52 SHALL BE LISTED TAMPER-RESISTANT TYPE.

14-2 22 15A 110V BEDROOM #2 14-2 19 15A 110V SITTING ROOM 14-2 21 15A 110V PFS Corporation BEDROOM #3 J<sup>‡</sup>BOX FOR R/ADON PUMP Northeast Region **APPROVED** H Raup – 3 7/20/17 **Approval limited to Factory Built Portion** 

OTES:

. INSULATED STAPLES ARE REQUIRED TO SUPPORT ALL WIRING

2. 990 SQ. FT. PER FLOOR (SMOKE DETECTORS REQUIRED EVERY 1,200 SQ. FT.

3. SMOKE DETECTOR TYPE: PHOTOELECTRIC
4. SMOKE DETECTOR MUST BE INTERCONNECTED BETWEEN FLOORS.

THIS BUILDING HAS BEEN REVER THE EXTRACTED FROM AN APPROVED SYSTEMS OR PER MODEL APPROVAL

O#6861

EL2

2ND STORY ELECTRICAL PLAN

ERSANT BAY HOMES

WYER/PROJECT

IZABETH GILLIS 2

REVISION
PRELIM
REV. PRELIM
FINAL

PFS Corporation
Northeast Region
APPROVED
H Raup – 3
7/20/17
Approval limited to

				proval limited to tory Built Portion		EGACY HOMES LLC
EL	ECTRICAL LOAD CALCULA	TION FOR ON#6861-	MA			L EG/ODULAR HOME
HOUSE SQFT:	0	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				I CON WEEPIA
AIR CONDITIONING AND HEAT						IC
AIR CONDITIONING:	O WATTS			O WATTS		'\
CENTRAL ELECTRIC SPACING HEATING:	0 WATTS (X 0.65)			O WATTS	<u></u>	
LESS THAN FOUR SEPARATELY CONTROLLED ELECTRIC SPACE HEATING UNITS:	0 WATTS (X 0.65)			0 WATTS	\ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	
FOUR OR MORE SEPARATELY CONTROLLED ELECTRIC SPACE HEATING UNITS:	0 WATTS (X 0.45)			O WATTS		
*NOTE: USE THE LARGER OF THE AIR CONDIT	IONING OR THE DIVERSIFIED DEMA	AND OF THE HEATING LOAD			REVISION	
OTHER LOADS		WATTS OR VOLT-AMPS	CIRCUIT AMPACITY	WIRE SIZE		
GENERAL LIGHTING:	$(0 \times 3)$	0	15A	14-2		
SMALL APPLIANCES:	(4 X 1,500)	6,000	20A	10-3	DATE	
RANGE:		11,400	50A	8-3		
DISHWASHER: GARBAGE DISPOSAL:		1,200 750	20A 15A	12-2 14-2		
WASHER:		1,500	20A	12-2		Q (MPH)
PRYER:		5,800	30A	10-3		202559 WIND SPEED (MPH) TYPE
URNACE:		0	N/A	N/A		Z W I
VATER HEATER:		5,500	30A	10-3		l les)
		32,150				A LOAD (
						STATE MA SNOW L SQFT
FIRST 10kW OF OTHER LOADS @ 100%:	(00.450 0.40)		=	10,000	ASANT BAY HOMES	L NO
REMAINDER OF OTHER LOADS @ 40%:	(22,150 x 0.40)		=	8,860		/AY
AIR CONDITIONING OR HEAT FROM ABOVE:  TOTAL CALCULATED LOAD::			=	18,860	T BA	OR V
REQUIRED SERVICE SIZE:	(18,860 / 240)		=	79 AMPS	ASAN ER/PROJE	SS SALLING STANDING S
NSTALLED PANEL SIZE:	, , , , , , , , , , , , , , , , , , ,		=	200 AMPS	BUILDER PLE, HOMEBUY	ADDRESS ADDRESS COUNTY ORDER &
					ELE	ECTRICAL LOAD CALC
				THIS BULDING IMAS BEEN PROPERTY OF THE PROPERT	PAGE #:	ELC

## CIRCUIT SCHEDULE

*WIRE	WITH	GROUND	ALL	CIRCUITS	

CRT	BRK	WIRE	LOCATION VOL	T CF	RT BRK	WIRE	LOCATION	VOLT
11	20A	12-2	SMALL APPLIANCE 110	2	2 20A	12-2	SMALL APPLIANCE	110
3	15A	14-2	GENERAL LIGHTING 110		1 20A	12-2	DINING ROOM	110
5	15A	14-2	MECH. ROOM 110	(	5 15A	14-2	GENERAL LIGHTING	110
7	15A	14-2	WP GFI EXTERIOR RECEPTS 110	3	3 15A	14-2	LIVING ROOM	110
9	20A	12-2	SMALL APPLIANCE 110	1	0 20A	12-2	BATH GFI	110
11	15A	14-2	GENERAL LIGHTING 110	1	2 20A	12-2	MICROWAVE	110
13	20A	12-2	DISHWSAHER 110	1	4 15A	14-2	GENERAL LIGHTING	110
15	15A	14-2	BEDROOM#1 110	1	6 15A	14-2	BEDROOM#3	110
17	20A	12-2	WASHER 110	1	8 30A	10-3	DRYER	220
19	15A	14-2	GENERAL LIGHTING 110	2	0 30A	10-3	DRIER	220
21	15A	14-2	SITTING ROOM 110	2	2 15A	14-2	BEDROOM#2	110
23				2	4			
25				2	6			
27				2	8			
29				3	0			
31				3	2			
33				3	4			
35				3	6			
37				3	8			
39				4	0			
								1

PFS Corporation
Northeast Region
APPROVED
H Raup – 3
7/20/17
Approval limited to
Factory Built Portion

CIRCUIT SCHEDULE

THIS BUILDING HAS BEEN EXTRACTED FROM AN APPROVED SYSTEMS OR PER MODEL APPROVAL

O#6861

CS

THIS FOUNDATION PLAN IS FOR DIMENSIONS ONLY. FOUNDATION WALLS, FOOTINGS, COLUMNS, PIERS, AND SLAB TO BE DESIGNED BY OTHERS TO MEET STATE AND/OR LOCAL CODES USING EXISTING SOIL ANALYSIS. MANUFACTURER. ASSUMES NO RESPONSIBILITY FOR ERRORS IN THE CONSTRUCTION OF THE FOUNDATION. ANY AND ALL DIMENSIONS ARE TO BE CHECKED AND VERIFIED (AGAINST THE FLOOR PLAN "BUILDER COPY") BY BUILDER/DEALER PRIOR TO FOUNDATION CONSTRUCTION. THE BUILDER/DEALER MUST CONTACT MANUFACTURER. WITH ANY DISCREPANCIES PRIOR TO THE START OF CONSTRUCTION.

MANUFACTURER. WILL NOT ASSUME ANY RESPONSIBILITY IF BUILDER/DEALER/OWNER EXCEEDS MAXIMUM SPACING OF SUPPORTS AS SHOWN ON THIS DRAWING.

2x SILL PLATE

CONCRETE FOOTING

**ENDWALL ANCHOR BOLTS (TYP.)** 1/2" @ 14" O. C. OR 5/8" @ 20" O. C.

4,272#

G.F.J RECEPT. DEY OTHERS

**⟨B-**↑

(OR EQUAL SHEAR CONN. OF 10,768 LBS)

THE FOUNDATION TO BE DESIGNED AND SEALED BY MA PE OR RA AND MUST BE DESIGNED TO THE LOADS PROVIDED, INCLUDING HOLD DOWNS AND ALL FLOOD PLAIN REQUIREMENTS. FOUNDATION TO BE INSPECTED AND APPROVED BY LOCAL BUILDING INSPECTOR

FOUNDATION WAL

5'-3"

5534#~

6'-0"

11,067#

BY PIF ZIP 02559 110 110 CAPE

FOUNDATION PLAN

FND

O#6861

BUILDER INSTALLED HOLD DOWN FROM FOUNDATION TO STUDS > 13122 LBS. [SUGGESTED SIMPSON HD19 W/ 1 1/4"  $\emptyset$ ANCHOR OR EQUAL] MIN. (4) 2 X 6 WALL STUDS FASTEN TOGETHER W/ (2) ROWS OF 16d COMMON NAILS @ 2" O.C.

33'-0"

SIDEWALL ANCHOR BOLTS (TYP.) INSTALLED BY OTHERS

SIDEWALL ANCHOR BOLTS (TYP.) 1/2" @ 53" O. C. OR 5/8" @ 72" O.C.

15,638#

12'-0" HOLD DIM.

1/2" @ 53" O. C. OR 5/8" @ 72" O.C.

(OR EQUAL SHEAR CONN. OF 7,543 LBS)

(OR EQUAL SHEAR CONN. OF 7,543 LBS)

39'-0"

- CONCRETE FLOOR -

11,067#

CEILING MOUNT SMOKE DETECTOR

INTEGRAL PILASTERS OR EQUAL REQUIRED @ 10'-0"

O.C. WHEN BACKFILL EXCEEDS 4'-0" IN HEIGHT(SEE CODE AUTHORITY FOR LOCAL REQUIREMENTS)

5'-3"

11,067#

**ENDWALL ANCHOR BOLTS (TYP.)** 1/2" @ 14" O. C. OR 5/8" @ 20" O. C.

(B-1)

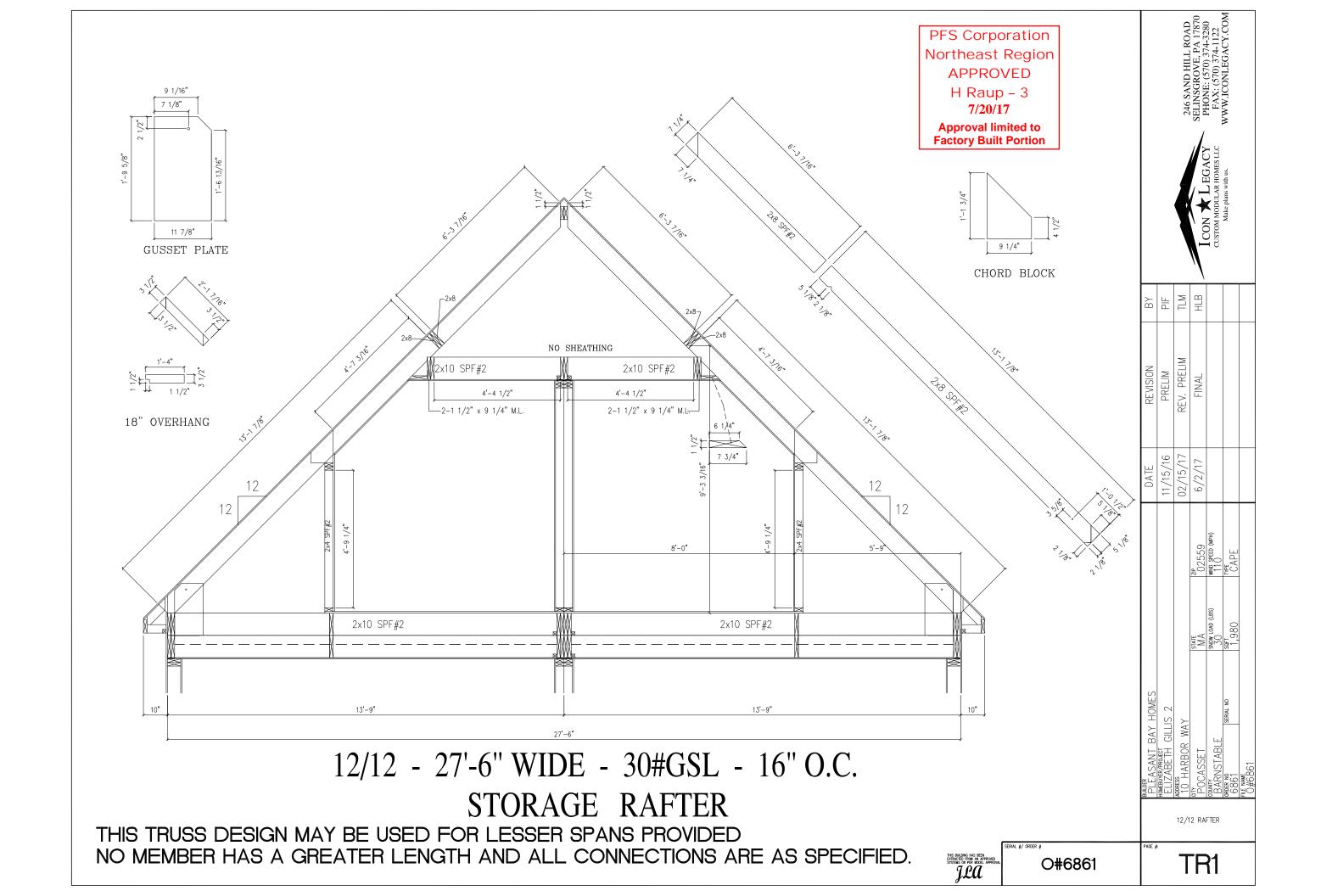
(OR EQUAL SHEAR CONN, OF 10,768 LBS)-

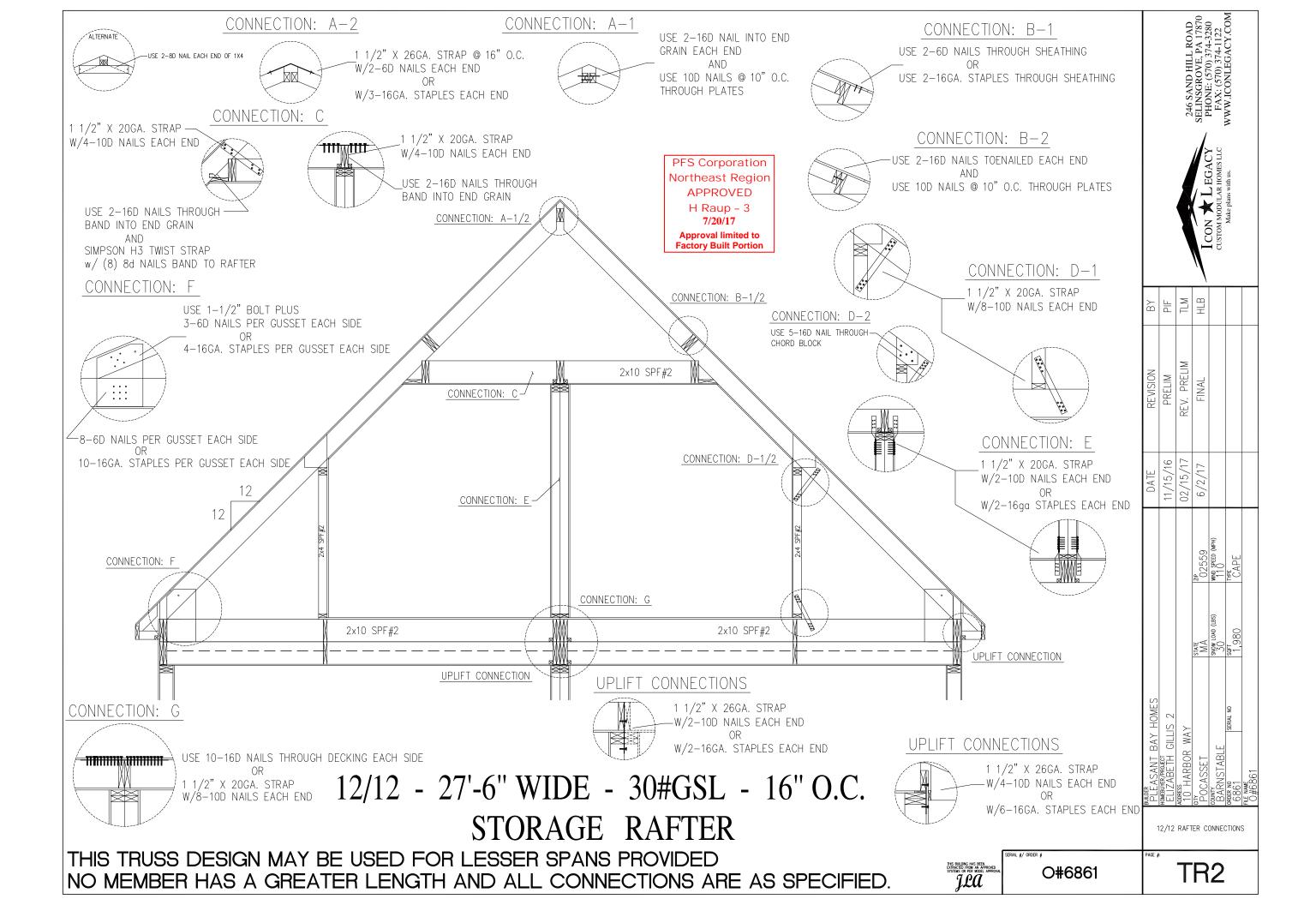


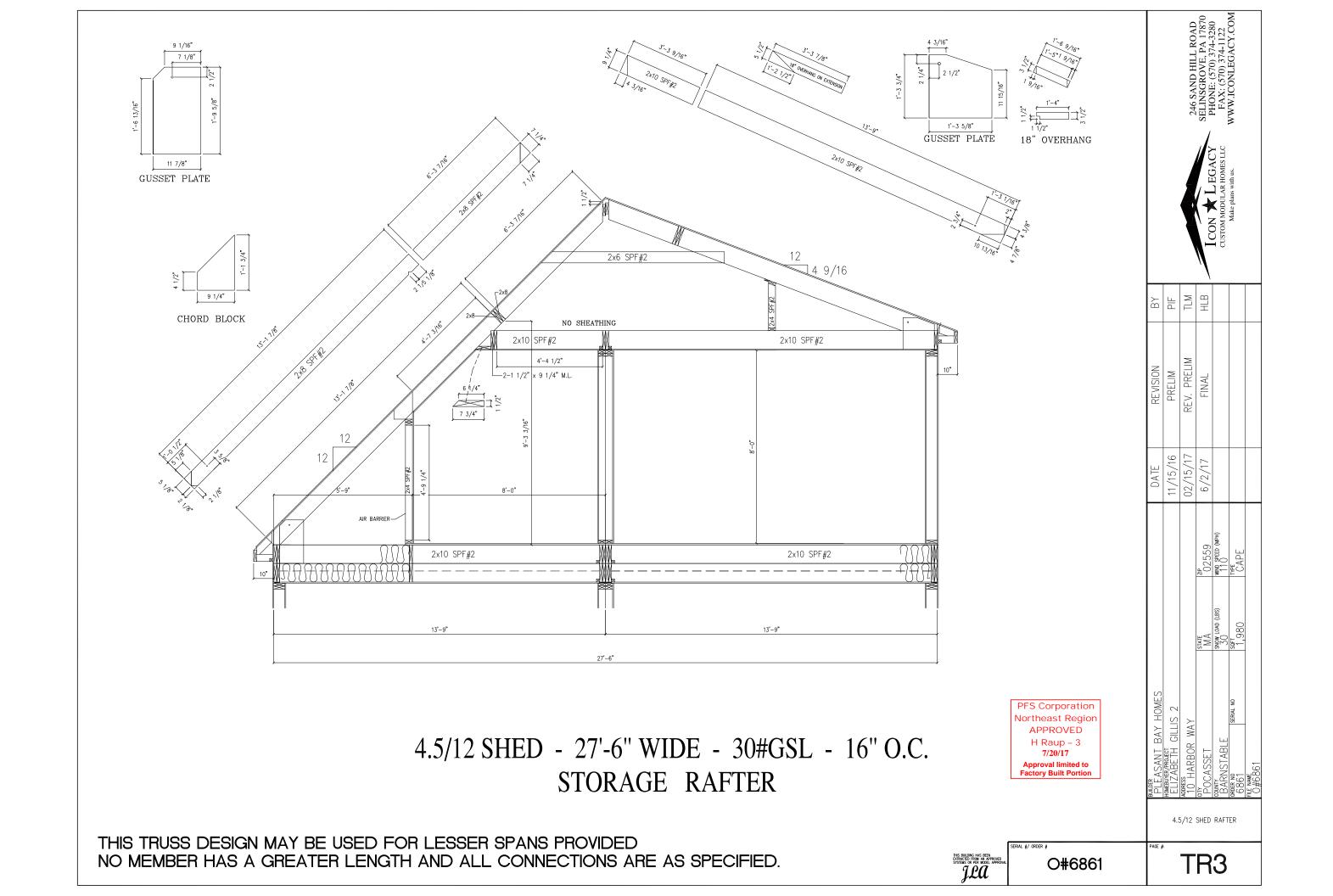
BUILDER INSTALLED HOLD DOWN FROM FOUNDATION TO STUDS > 3685 LBS. [SUGGESTED SIMPSON STHD14RJ OR EQUAL] MIN. (2) 2 X 6 WALL STUDS FASTEN TOGETHER W/ (2) ROWS OF 16d COMMON NAILS @ 9" O.C.

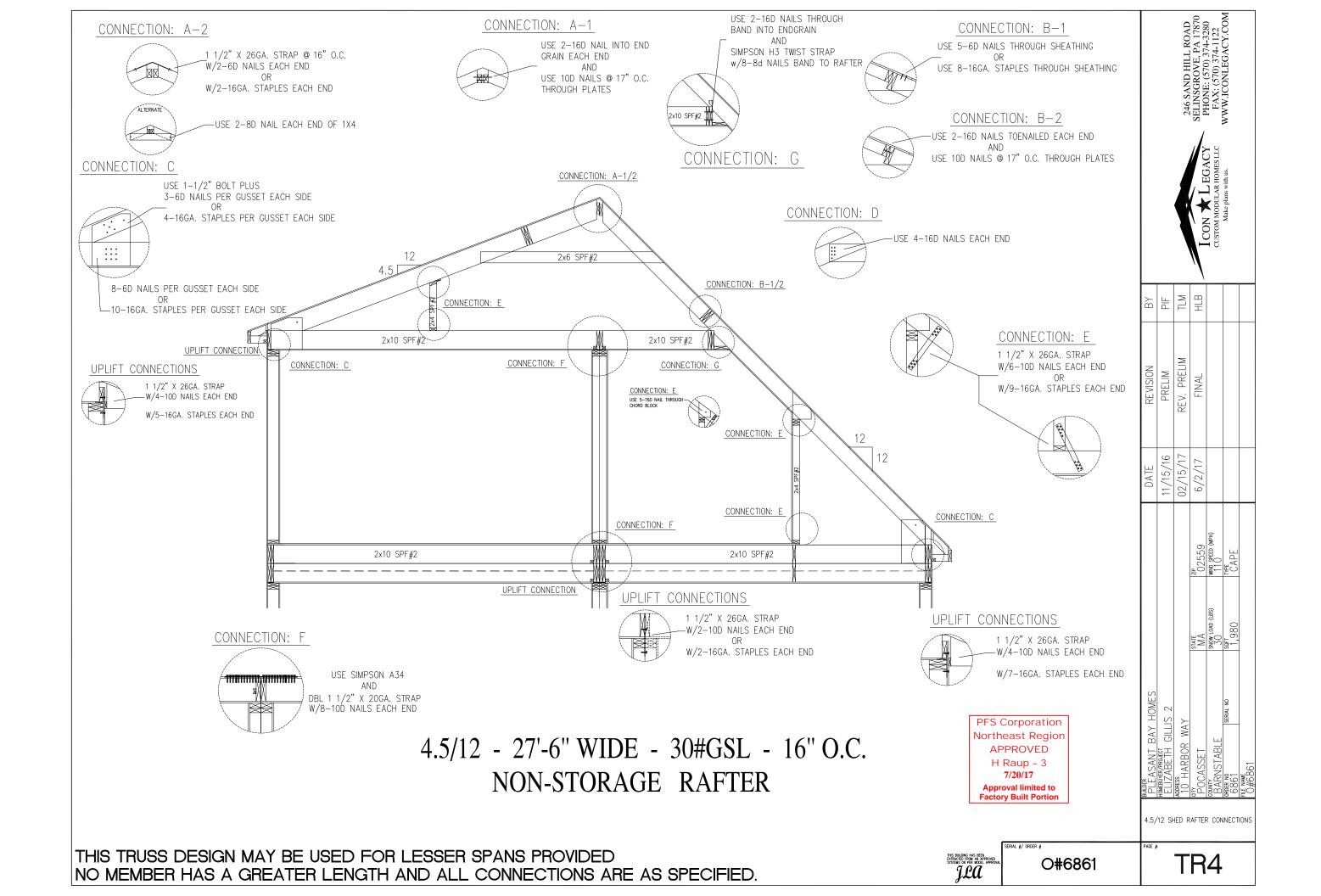
**PFS** Corporation Northeast Region **APPROVED** H Raup - 3 7/20/17

Approval limited to **Factory Built Portion** 

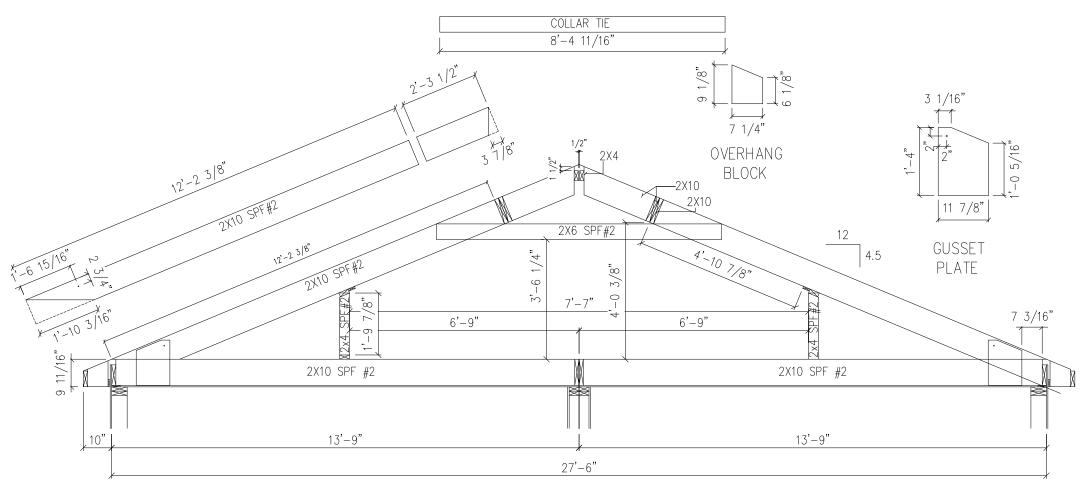








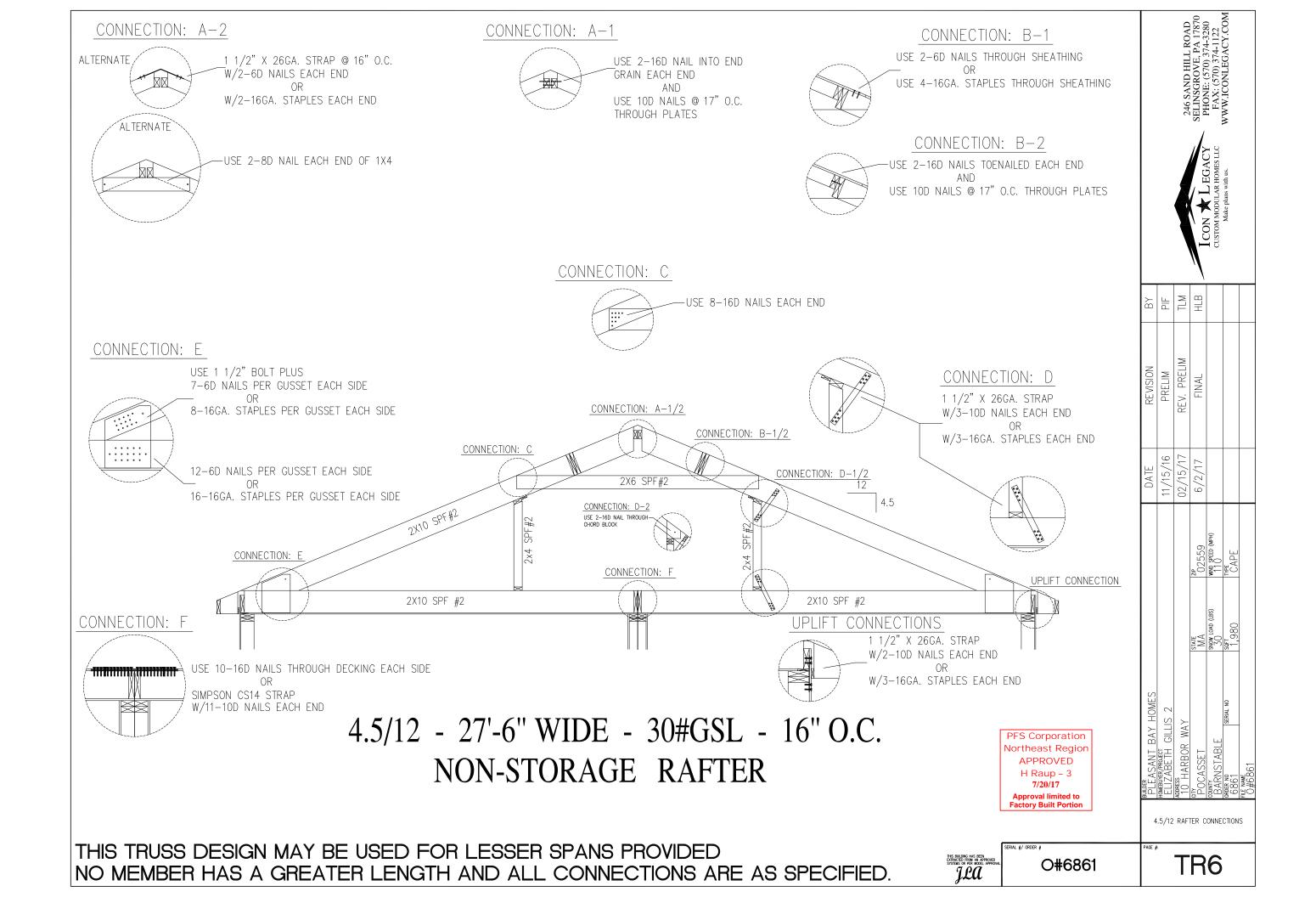


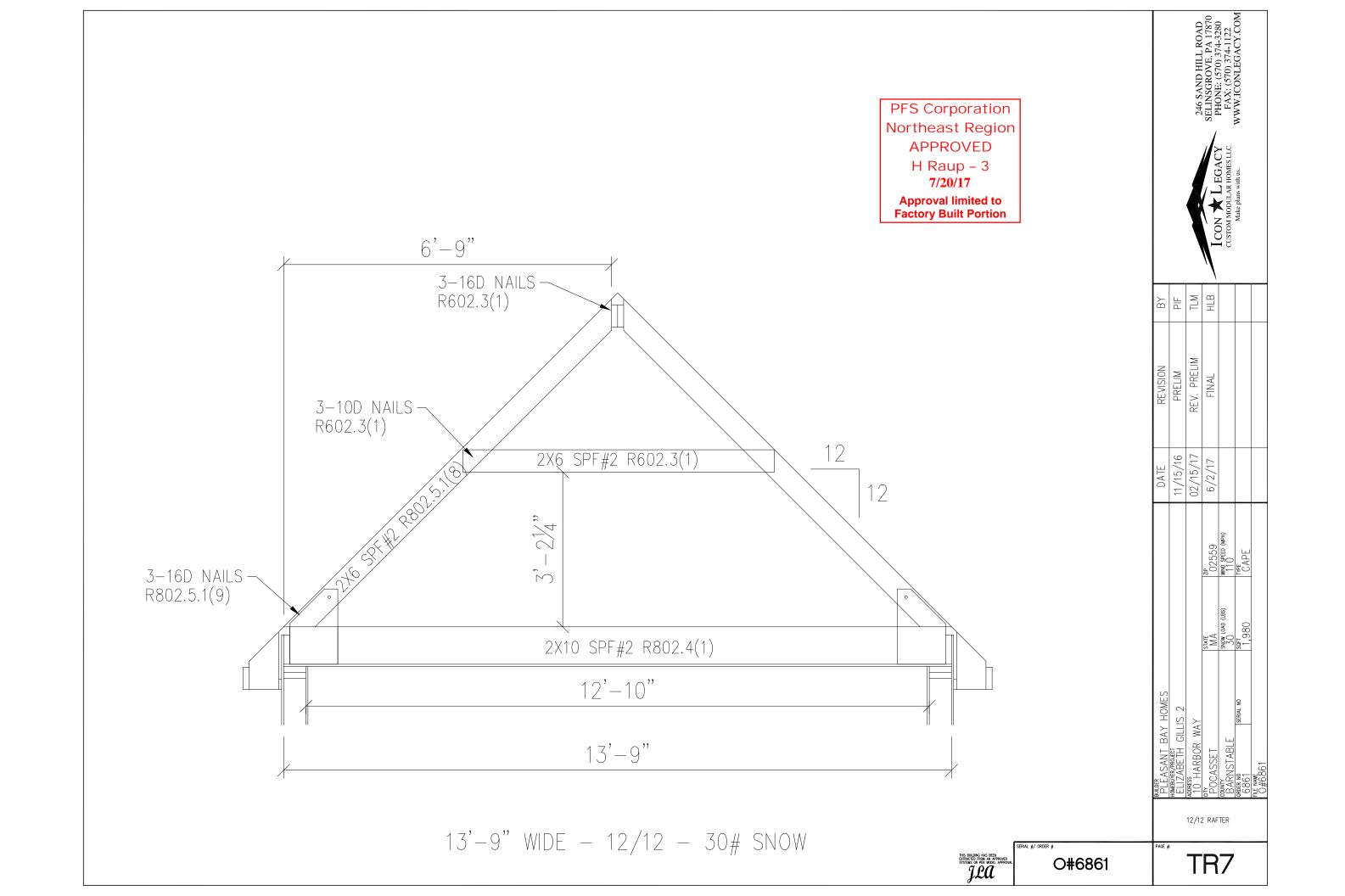


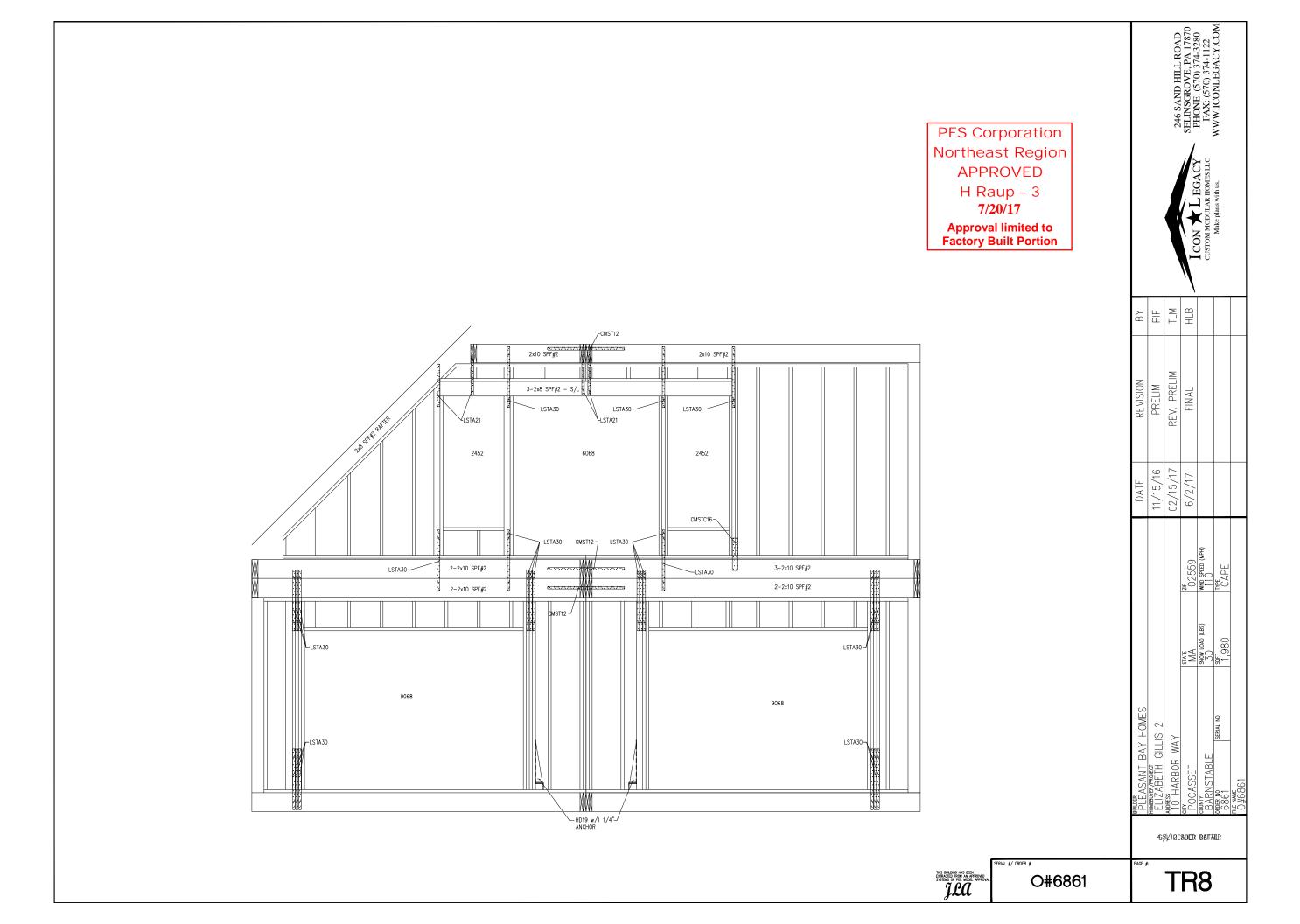
4.5/12 - 27'-6" WIDE - 30#GSL - 16" O.C. NON-STORAGE RAFTER

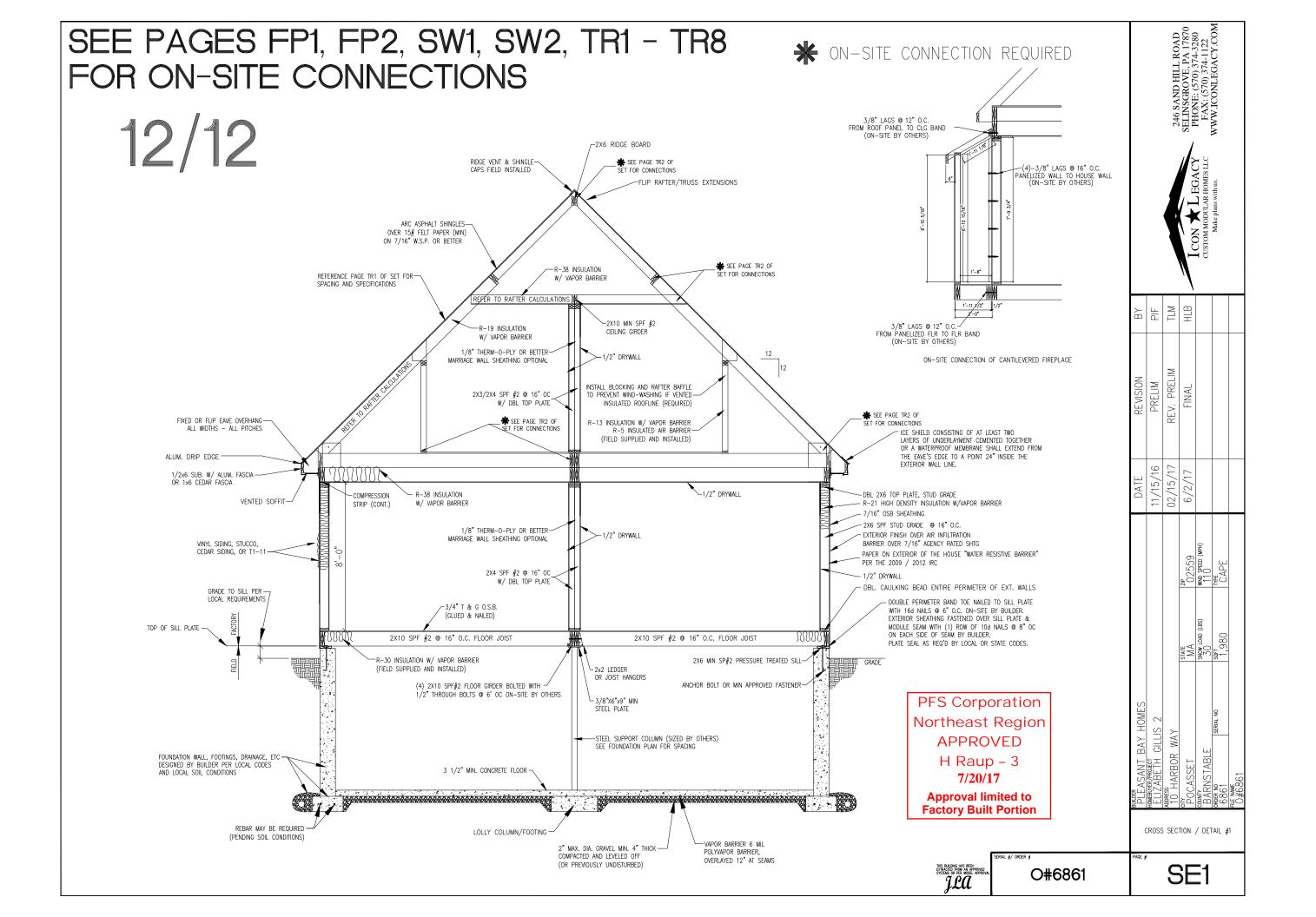
THIS TRUSS DESIGN MAY BE USED FOR LESSER SPANS PROVIDED NO MEMBER HAS A GREATER LENGTH AND ALL CONNECTIONS ARE AS SPECIFIED.

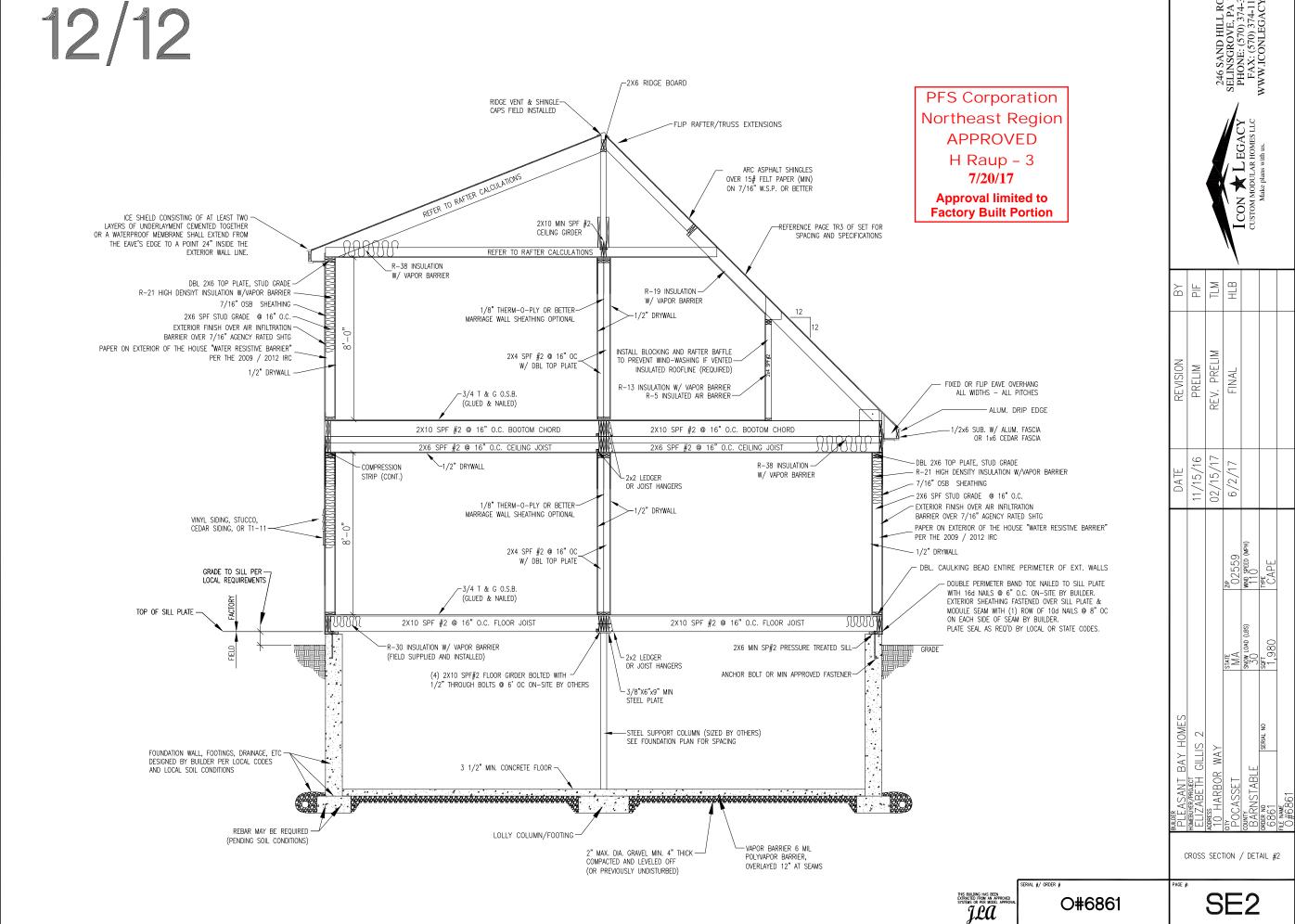
BUILDER SEINE WAS REEN FOR SEIN AND SEIN AND STEER BARROUS BARROUS SEIN AND STEER BARROUS BA



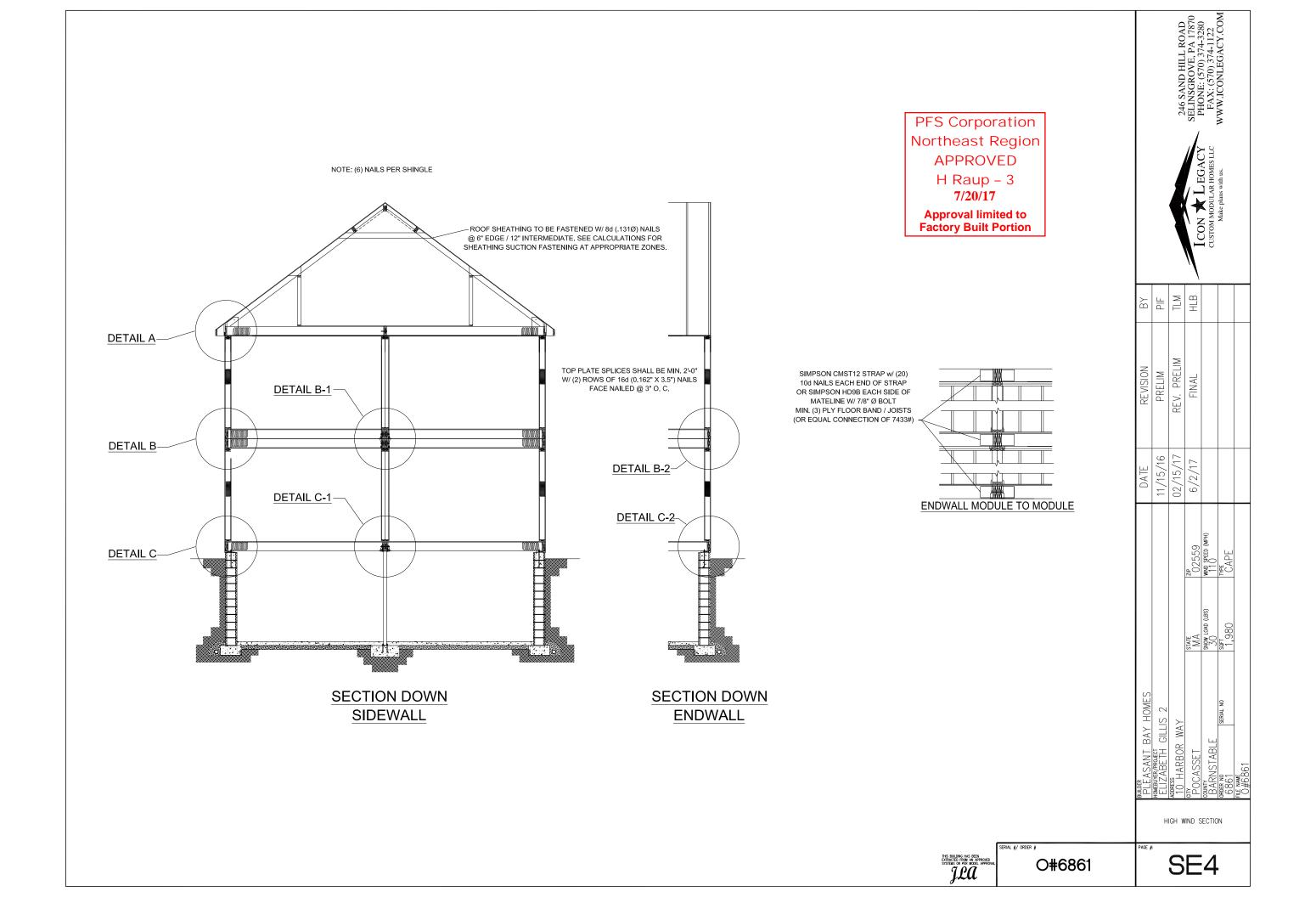


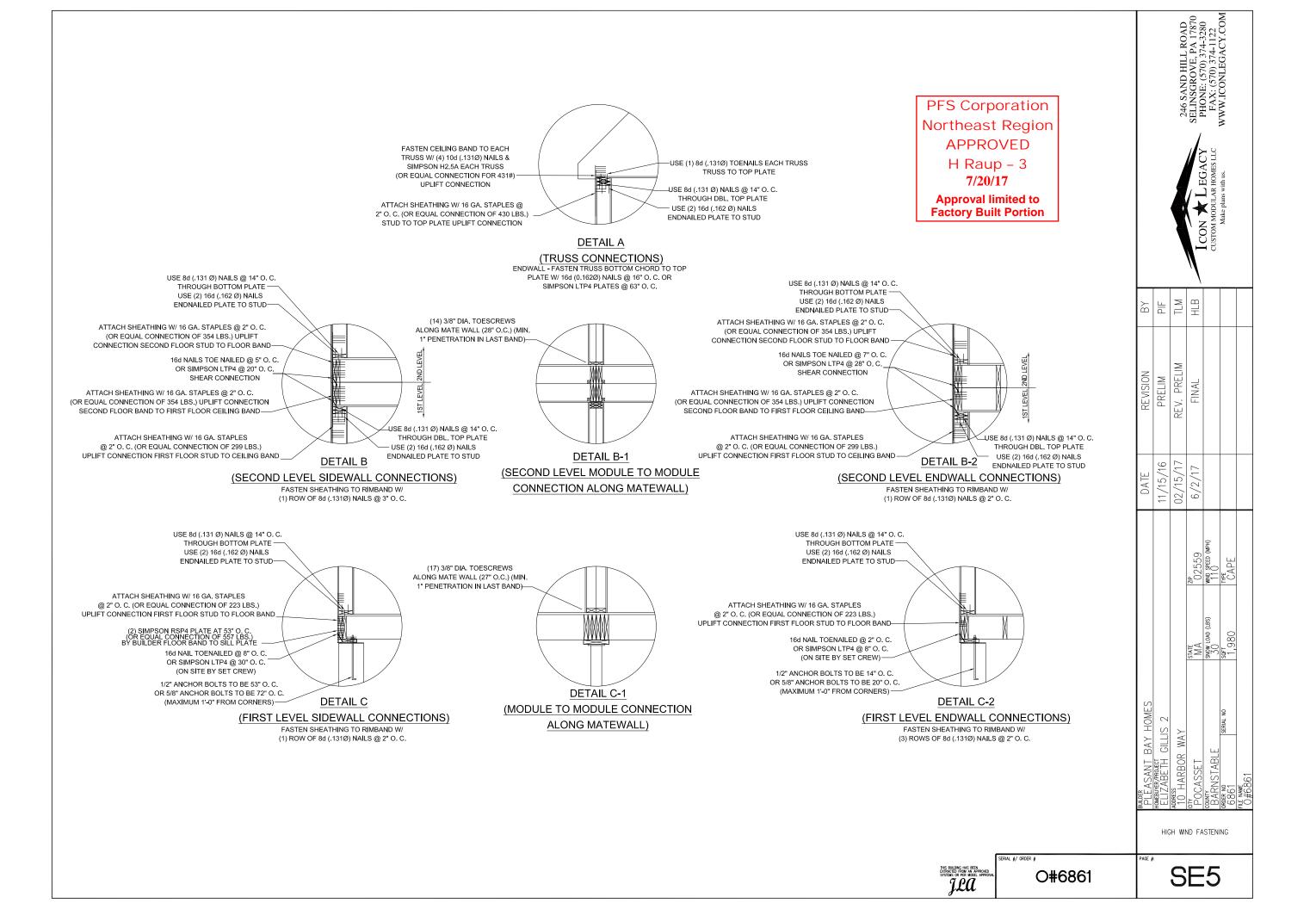






4.5/12 PFS Corporation Northeast Region **APPROVED** H Raup - 3 -2X6 RIDGE BOARD 7/20/17 RIDGE VENT & SHINGLE-CAPS FIELD INSTALLED **Approval limited to** -FLIP RAFTER/TRUSS EXTENSIONS **Factory Built Portion** ARC ASPHALT SHINGLES -OVER 15# FELT PAPER (MIN) ON 7/16" W.S.P. OR BETTER REFERENCE PAGE TR3 OF SET FOR SPACING AND SPECIFICATIONS FIXED OR FLIP EAVE OVERHANG ICE SHIELD CONSISTING OF AT LEAST TWO ALL WIDTHS - ALL PITCHES -2X10 MIN SPF #2 LAYERS OF UNDERLAYMENT CEMENTED TOGETHER
OR A WATERPROOF MEMBRANE SHALL EXTEND FROM CEILING GIRDER ALUM. DRIP EDGE THE EAVE'S EDGE TO A POINT 24" INSIDE THE REFER TO RAFTER CALCULATIONS EXTERIOR WALL LINE. 1/2x6 SUB. W/ ALUM. FASCIA OR 1x6 CEDAR FASCIA R-38 INSULATION\_ ─1/2" DRYWALL W/ VAPOR BARRIER W/ VAPOR BARRIER -DBL 2X6 TOP PLATE, STUD GRADE - R-21 HIGH DENSIYT INSULATION W/VAPOR BARRIER - 7/16" OSB SHEATHING 1/8" THERM-O-PLY OR BETTER-- 2X6 SPF STUD GRADE @ 16" O.C. MARRIAGE WALL SHEATHING OPTIONAL VINYL SIDING, STUCCO. - EXTERIOR FINISH OVER AIR INFILTRATION CEDAR SIDING, OR T1-1 BARRIER OVER 7/16" AGENCY RATED SHTG PAPER ON EXTERIOR OF THE HOUSE "WATER RESISTIVE BARRIER" 2X4 SPF #2 @ 16" OC PER THE 2009 / 2012 IRC W/ DBL TOP PLATE PRELIM - 1/2" DRYWALL -3/4 T & G O.S.B. (GLUED & NAILED) RE REFER TO RAFTER CALCULATIONS REFER TO RAFTER CALCULATIONS 2X6 SPF #2 @ 16" O.C. CEILING JOIST 2X6 SPF #2 @ 16" O.C. CEILING JOIST -DBL 2X6 TOP PLATE, STUD GRADE ~1/2" DRYWALL · COMPRESSION R-21 HIGH DENSITY INSULATION W/VAPOR BARRIER STRIP (CONT.) -2x2 LEDGER OR JOIST HANGERS 15, 7/16" OSB SHEATHING - 2X6 SPF STUD GRADE @ 16" O.C. 1/8" THERM-O-PLY OR BETTER-- EXTERIOR FINISH OVER AIR INFILTRATION -1/2" DRYWALL MARRIAGE WALL SHEATHING OPTIONAL BARRIER OVER 7/16" AGENCY RATED SHTG VINYL SIDING, STUCCO. CEDAR SIDING, OR T1-11 PAPER ON EXTERIOR OF THE HOUSE "WATER RESISTIVE BARRIER" PER THE 2009 / 2012 IRC ZIP 02559
WIND SPEED (MPH)
TYPE
CAPE 2X4 SPF #2 @ 16" OC W/ DBL TOP PLATE DBL. CAULKING BEAD ENTIRE PERIMETER OF EXT. WALLS GRADE TO SILL PER -LOCAL REQUIREMENTS DOUBLE PERIMETER BAND TOE NAILED TO SILL PLATE -3/4 T & G O.S.B. WITH 16d NAILS @ 6" O.C. ON-SITE BY BUILDER. (GLUED & NAILED) EXTERIOR SHEATHING FASTENED OVER SILL PLATE & MODULE SEAM WITH (1) ROW OF 10d NAILS @ 8" OC TOP OF SILL PLATE -ON EACH SIDE OF SEAM BY BUILDER. 2X10 SPF #2 @ 16" O.C. FLOOR JOIST 2X10 SPF #2 @ 16" O.C. FLOOR JOIST PLATE SEAL AS REQ'D BY LOCAL OR STATE CODES. R-30 INSULATION W/ VAPOR BARRIER 2X6 MIN SP#2 PRESSURE TREATED SILL-(FIELD SUPPLIED AND INSTALLED) 2x2 LEDGER OR JOIST HANGERS (4) 2X10 SPF#2 FLOOR GIRDER BOLTED WITH ANCHOR BOLT OR MIN APPROVED FASTENER-1/2" THROUGH BOLTS @ 6' OC ON-SITE BY OTHERS -3/8"X6"x9" MIN -STEEL SUPPORT COLUMN (SIZED BY OTHERS) SEE FOUNDATION PLAN FOR SPACING FOUNDATION WALL, FOOTINGS, DRAINAGE, ETC DESIGNED BY BUILDER PER LOCAL CODES AND LOCAL SOIL CONDITIONS 3 1/2" MIN. CONCRETE FLOOR HARBOR yjäniniintentennenninentenniniiniiniintenneng y production of the second sec REBAR MAY BE REQUIRED -LOLLY COLUMN/FOOTING (PENDING SOIL CONDITIONS) - VAPOR BARRIER 6 MIL 2" MAX. DIA. GRAVEL MIN. 4" THICK -COMPACTED AND LEVELED OFF POLYVAPOR BARRIER, OVERLAYED 12" AT SEAMS CROSS SECTION / DETAIL #3 (OR PREVIOUSLY UNDISTURBED) SE3 O#6861





PFS Corporation Northeast Region APPROVED H Raup - 3 7/20/17 Approval limited to Factory Built Portion

ANT BAY HOMES			DATE	REVISION	ВУ	
ROLLIS 2			11/12/16	PRELIM	PIF	
RBOR WAY			02/15/17	REV. PRELIM	TLM	
SET	STATE MA	ar 02559	6/2/17	FINAL	HLB	
	AD (LBS)	WIND SPEED (MPH)				
SERIAL NO		CAPE				

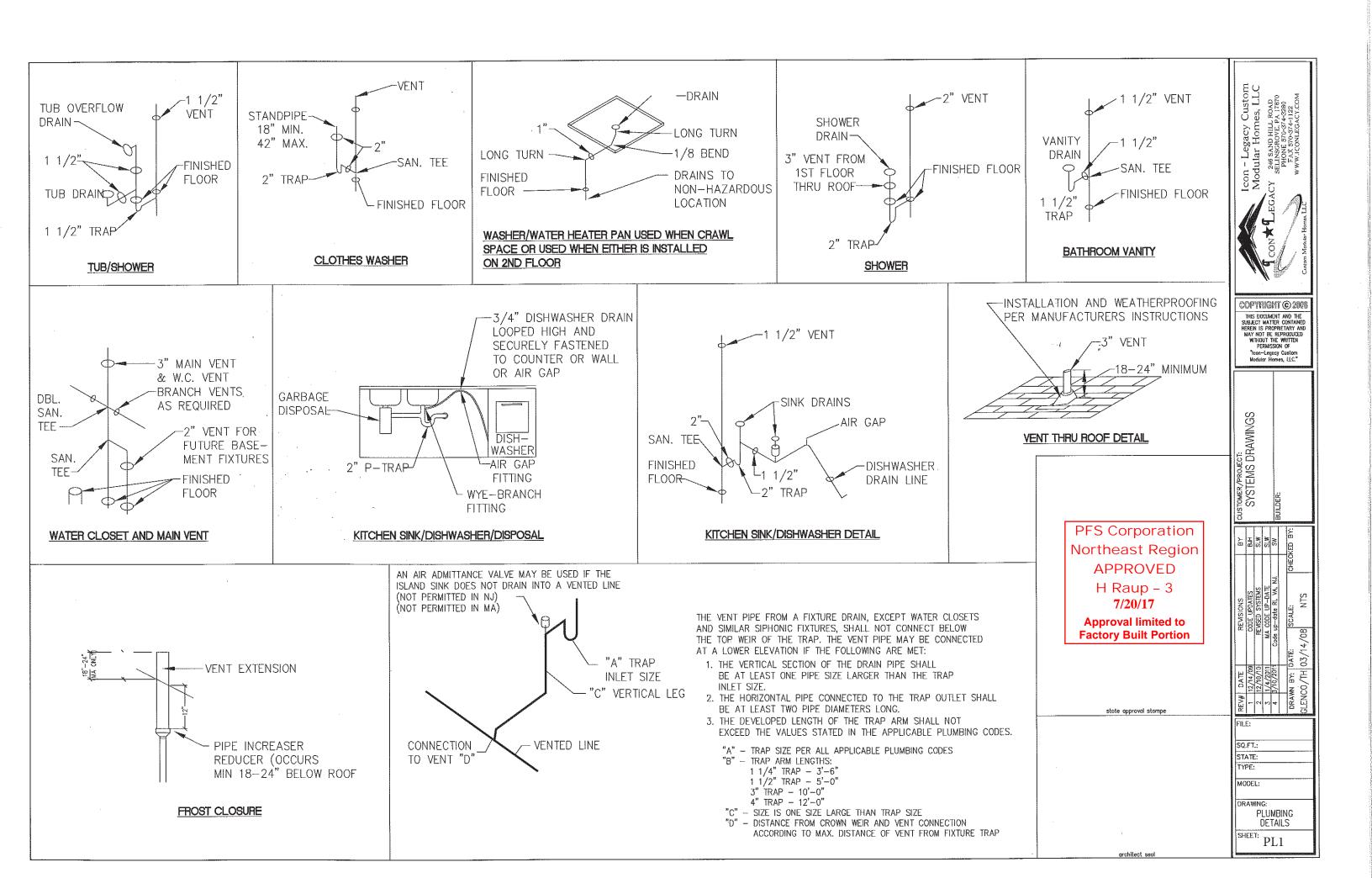
DOOR & WINDOW SCHEDULE

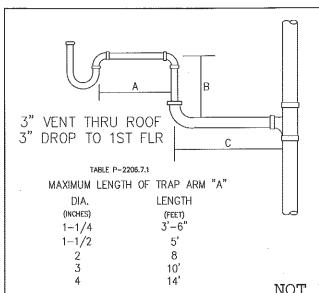
O#6861

THIS BUILDING HAS BEEN EXTRACTED FROM AN APPROVED SYSTEMS OR PER MODEL APPROVA

DWS

	DOOR AND WINDOW SCH	- DIII E							
WINDOWC	DOON AND WINDOW SCHI	LDULL		OLEAD ODENING	OLEAD ODENING				
WINDOWS DESCRIPTION	ROUGH OPENING	AREA	LIGHT	CLEAR OPENING WIDTH (EACH)	CLEAR OPENING HEIGHT (EACH)	VENT	U-FACTOR	OTY	TOTAL AREA
ANDERSEN 400 SERIES CASEMENT C235	48 1/2" X 41 3/8"	13.94	13.6	18.290	36.000	9.20	0.31	1	13.94
ANDERSEN 400 SERIES TILT-WASH DOUBLE HUNG TW2032	26 1/8" X 40 7/8"	7.42	4.2	21.875	16.250	2.48	0.31	2	14.84
ANDERSEN 400 SERIES TILT-WASH DOUBLE HUNG TW2052	26 1/8" X 64 7/8"	11.77	7.4	21.875	28.250	4.31	0.31	2	23.54
ANDERSEN 400 SERIES TILT-WASH DOUBLE HUNG TW24210	30 1/8" X 36 7/8"	7.71	4.5	25.875	14.250	2.58	0.31	1	7.7
ANDERSEN 400 SERIES TILT-WASH DOUBLE HUNG TW2452	30 1/8" X 64 7/8"	13.57	8.9	25.875	28.250	5.10	0.31	2	27.14
ANDERSEN 400 SERIES TILT-WASH DOUBLE HUNG TW3046-2	75 7/8" X 56 7/8"	29.97	20.6	33.875	24.250	11.46	0.31	3	89.9
ANDERSEN 400 SERIES TILT-WASH DOUBLE HUNG TW3052	38 1/8" X 64 7/8"	17.18	12.0	33.875	28.250	6.67	0.31	6	103.08
ANDERSEN 400 SERIES TILT-WASH DOUBLE HUNG TW3052-2	75 7/8" X 64 7/8"	34.18	24.1	33.875	28.250	13.34	0.31	1	34.18
							TOTAL AF	REA:	314.34
EXTERIOR DOORS	DOLLOU ODENINO	<b>ADE A</b>	LIOUT	CLEAR OPENING	CLEAR OPENING	) /FALT	II FAOTOD		TOTAL ARE
DESCRIPTION TORS ( TEXT STATE)	ROUGH OPENING	AREA	LIGHT	WIDTH (EACH)	HEIGHT (EACH)	VENT	U-FACTOR	QTY	TOTAL AREA
PLASTPRO 3068 (< 50% GLASS)	38 1/2" X 82 1/8"	21.96	0.0	0.000	0.000	20.00	0.17	1	21.96
PLY GEM PRO SERIES CLASSIC SLIDING PATIO DOOR 9068	108" X 80"	60.00	42.5	27.125	75.750	14.30	0.25	2	120.00
PLY GEM PRO SERIES CLASSIC SLIDING PATIO DOOR CLSPDR6068	72" X 80"	40.00	30.8	29.031	75.772	15.28	0.25	11	40.00 181.9
PLY GEM PRO SERIES CLASSIC SLIDING PATIO DOOR CLSPDR6008	/2 X 80	40.00	30.8	29.031	/5.//2	15.28	U.ZO TOTAL AF	RFA:	_



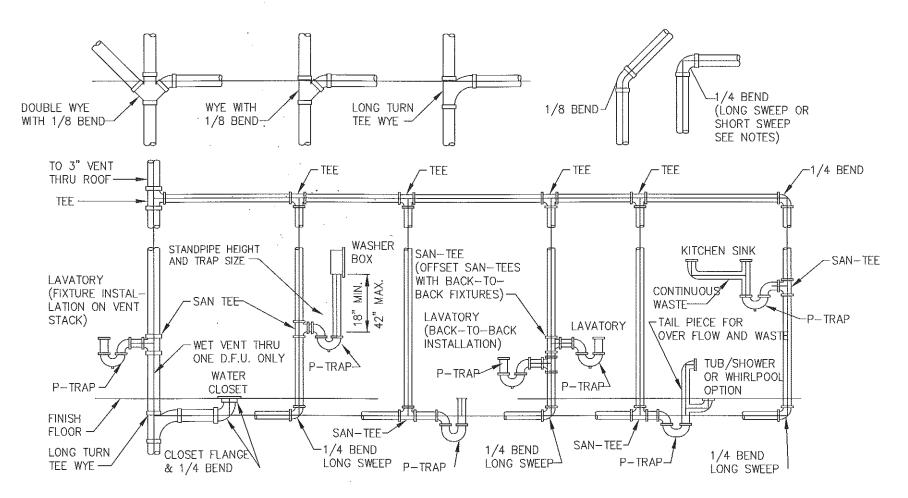


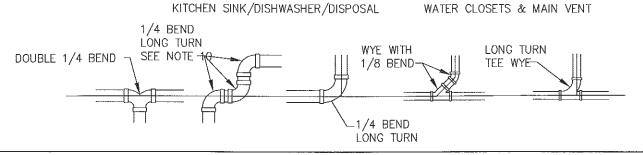
ALLOWABLE FALL IN TRAP ARM: THE TOTAL FALL IN TRAP ARM DUE TO PIPE SLOPE SHALL NOT EXCEED ONE PIPE DIAMETER, NOR SHALL THE VENT PIPE CONNECTION TO A FIXTURE DRAIN, EXCEPT FOR WATER CLOSETS AND SIMILAR FIXTURES, BE BELOW THE WEIR OF THE TRAP,

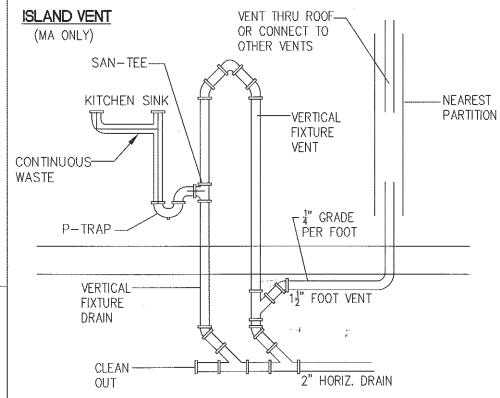
VERTICAL LEG FOR WASTE FIXTURE DRAINS: A VERTICAL LEG ( "B" IN DIAGRAM) MAY BE INSTALLED IN THE TRAP ARM OF A WASTE-FIXTURE DRAIN IN LIEU OF THE USUAL TRAP ARM TO VENT CONNECTION. TYPICAL INSTALLATIONS INCLUDE ISLAND SINKS AND FIXTURES NOT ADJACENT TO A WALL. VERTICAL LEG TRAP ARM INSTALLATIONS SHALL MEET THE FOLLOWING CRITERIA:

- 1. MINIMUM TRAP DIAMETER SHALL MEET CODES
- 2. THE DIAMETER OF SECTION "A" SHALL BE EQUAL TO THE DIAMETER OF THE TRAP.
- 3. THE LENGTH OF SECTION "A" SHALL BE NOT LESS THAN 8" AND IN ACCORDANCE WITH TABLE P-2206.7.1.
- 4. THE DIAMETER OF SECTION "B" SHALL BE ONE PIPE SIZE LARGER THAN THE DIAMETER OF SECTION : A".
- 5. THE LENGTH OF SECTION "B" SHALL BE NOT MORE THAN 36 INCHES
- 6. THE DIAMETER OF SECTION "C" SHALL BE ONE PIPE SIZE LARGER THAN THE DIAMETER OF SECTION "B".
- 7. THEIR IS NO RESTRICTION ON THE LENGTH OF SECTION "C".
- 8. BENDS SHALL BE THE DIAMETER OF THE LARGEST CONNECTED SECTION.

#### NOT PERMITTED IN MASSACHUSETTS









FILE:

SQ.FT.:
STATE:
TYPE:
MODEL:

SHEET:

DRAWING: PLUMBING DETAILS

PL2

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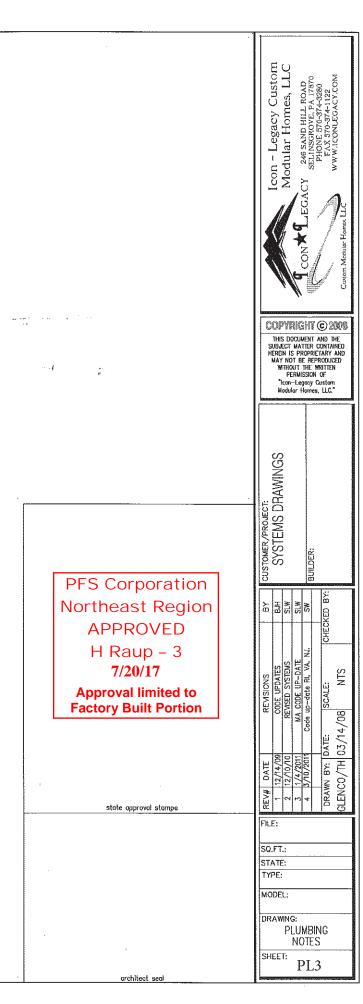
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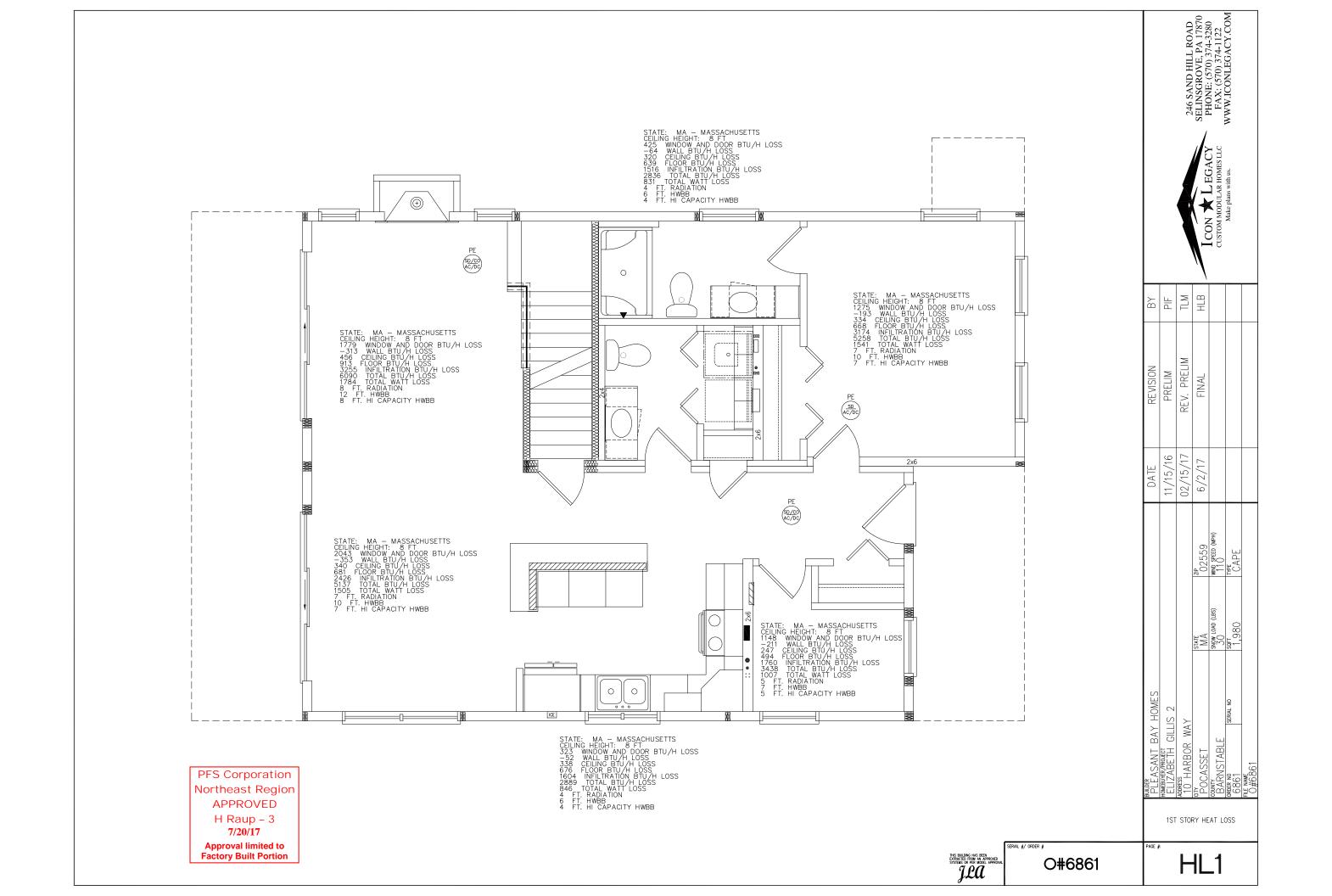
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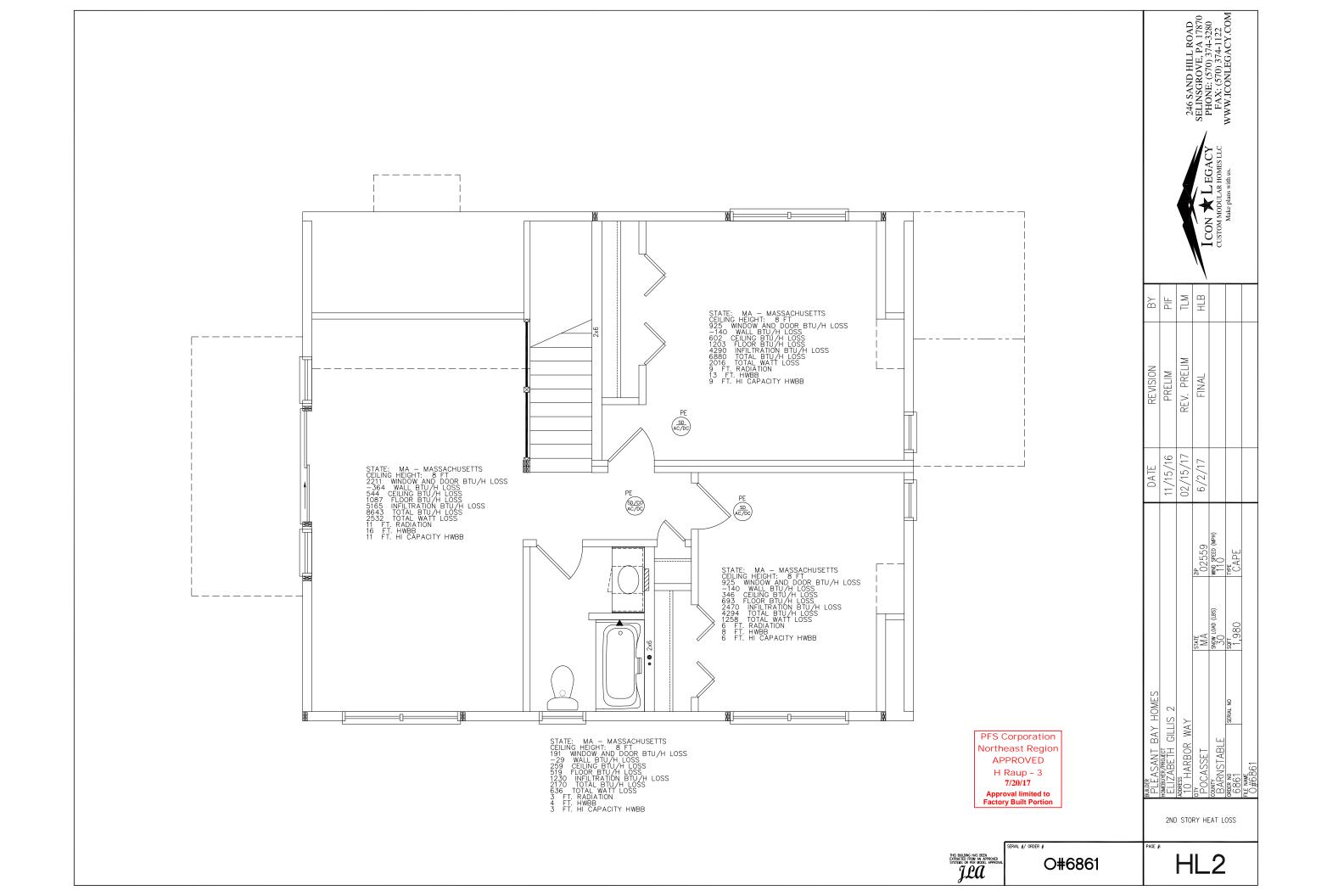
#### **PLUMBING NOTES:**

- ALL PLUMBING CONSTRUCTION AND MATERIAL BELOW THE MODULAR FLOOR AND BETWEEN FLOORS IS THE RESPONSIBILITY OF THE BUILDER/CONSTRACTOR AND IS TO BE DONE IN ACCORDANCE W/STATE AND LOCAL CODES.
- CONCEALED PIPING IN UNHEATED AREAS, INCLUDING OUTSIDE WALLS, SHALL BE PROTECTED AGAINST FREEZING IN PLANT. PIPING SHALL BE KEPT OUT OF UNHEATED AREAS WHERE POSSIBLE.
- ALL WASTE AND VENT LINES IN MODULES ARE ABS OR PVC PIPE. ALL SUPPLY LINES IN MODULES ARE COPPER, PEX, OR CPVC.
- 4. PITCH ON HORIZONTAL WASTE LINES IS \$\frac{1}{8}" PER FOOT FOR GREATER THAN 3" DIAMETER PIPE, \$\frac{1}{4}" PER FOOT FOR 3" DIAMETER PIPE OR LESS.
- 5. WASTE LINES: INSTALL WYE WITH CLEANOUT PRIOR TO EXITING WALL FOR CONNECTION TO DISPOSAL SYSTEM. 4" MINIMUM WASTE LINE TO SEPTIC (BY BUILDER IN FIELD).
- 6. WASHER SHALL HAVE MINIMUM 2" TRAP.
- 7. REMOVABLE TRAPS UNDER ALL SINKS TO PROVIDE CLEANOUT ACCESS.
- GARBAGE DISPOSAL MUST HAVE SEPARATE TRAP, DISHWASHER CANNOT DISCHARGE INTO GARBAGE DISPOSAL.
- 9. KITCHEN SINK SHALL HAVE 2" DRAIN WHEN A GARBAGE DISPOSAL OR DISHWASHER ARE CONNECTED.
- 10. HORIZONTAL TO HORIZONTAL AND VERTICAL TO HORIZONTAL DRAIN CHANGES IN DIRECTION SHALL BE 45° WYES, LONG SWEEP 90° ELBOWS, LONG SEEP TY'S, 6TH, 8TH, OR 16TH BENDS, APPROVED COMBINATIONS OF THESE OR EQUIVALENT LONG SWEEP FITTINGS. SHORT SWEEPS ARE PERMITTED IN SINGLE BRANCH HORIZONTAL TO VERTICAL CHANGES IN DIRECTION ON 3" PIPE AND LARGER.
- ALL HORIZONTAL VENT BRANCH PIPING SHALL BE LOCATED, A MINIMUM OF 6" ABOVE THE FLOOD LEVEL OF THE HIGHEST FIXTURE IN THAT BRANCH.
- 12. PVC-DWV PIPE SUPPORTS: AT BRANCHES, CHANGES IN DIRECTION, AND AT THE BASE, EACH FLOOR AND MID STORY (VERTICAL) MAXIMUM EVERY 4'-0" AT THE END OF BRANCHES, AND CHANGE OF DIRECTIONS OR ELEVATION,
- 13. PIPE PENETRATING FIRE RATED ASSEMBLIES INCLUDING FLOOR/CEILING SHALL BE FIRE STOPPED WHERE REQUIRED BY ALL CODES WITH MATERIAL EQUIVALENT TO CONSTRUCTION THROUGH WHICH IT PENENTRATES AND BE SUITABLE TO PIPE MATERIAL, OR USE METAL PIPE FROM A MINIMUM OF ABOVE THE FIRE RATED ASSEMBLY AND DOWN
- FIRE STOPPING SHALL BE PROVIDED AND VERIFIED BEFORE IT IS COVERED OR CONCEALED IN THE CONSTRUCTION PROCESS.
- 15. ANY STRUCTURAL MEMBER SUBJECT TO HOLE DRILLING, CUTTING, OR NOTHCING SHALL BE LEFT IN A SAFE STRUCTURAL CONDITION BY BEING REINFORCED, REPAIRED, OR REPLACED IN ACCORDANCE WITH THE STRUCTURAL REQUIREMENTS OF THE CODE.
- FIELD INSTALLED (ON-SITE) PIPING SHALL BE APPROVED BY THE LOCAL BUILDING CODE ENFORCEMENT OFFICER. PIPING SHALL BE FIELD TESTED FOR LEAKS.
- 17. BATH TUBS, INCLUDING GARDEN TUBS, HYDRO-MASSAGE, AND HOT TUBS SHALL HAVE A 1 ½" MIN OVERFLOW.
- 18. JOINTS AROUND PLUMBING FIXTURES SHALL BE MADE WATERPROOF AT FLOORS, WALLS, & COUNTERTOPS.
- 19. EACH FIXTURE SHALL BE INDIVIDUALLY DIRECT OR WET VENTED.
- 20. EACH DWELLING UNIT SHALL HAVE ONE MAIN 3" STACK FROM BUILDING DRAIN.
- 21. ALL VENTS THROUGH ROOF TO BE 3" MIN DIAMETER AND SHALL TERMINATE 18'-24" ABOVE THE ROOF.
- 22. BASEMENT MODELS SHALL BE PROVIDED IN FACTORY WITH A 2" VENT TO BASEMENT STUBBED BELOW THE FIRST FLOOR, THEN CAPPED AND LABELED. BASEMENT VENT MAY BE DELETED WHEN CLOTHES WASHER IS ON THE FIRST OR SECOND FLOOR.

- 23. ALL TRAP ARMS MUST BE SUPPORTED WITH 3" MINIMUM BEARING. (MA ONLY)
- 24. ALL PLASTIC PIPE MUST BE SUPPORTED AT INTERVALS IN ACCORDANCE WITH APPLICABLE PLUMBING CODES.
- 25. TRAPS SHALL BE PLACED AS CLOSE AS POSSIBLE TO FIXTURE OUTLET. MAXIMUM VERTICAL DROP FROM FIXTURE OUTLET TO TRAP WEIR IS 24".
- 26. INACCESSIBLE TRAPS SHALL NOT HAVE UNIONS, CLEANOUTS OR SLIPJOINTS. ACCESSIBLE TRAPS SHALL BE REMOVABLE WITH UNION IN TRAP SEAL OR HAVE CLEANOUT OPENING SIZED THE SAME AS THE TRAP.
- 27. MAXIMUM DISTANCE OF FIXTURE TRAP WEIR TO VENT SHALL BE IN ACCORDANCE WITH ALL APPLICABLE PLUMBING CODES.
- 28. PLASTIC PIPING SHALL BE PROTECTED WITH  $\frac{1}{18}$ " STEEL PLATE WHEN PIPE PASSES THROUGH WOOD MEMBERS LESS THAN 1  $\frac{1}{4}$ " FROM EDGE OF MEMBER.
- 29. FIRST FLOOR FIXTURES SHALL CONNECT INTO HORIZONTAL BUILDING DRAIN MORE THAN 10 PIPE DIAMETERS DOWNSTREAM OF STACK BASE AND NOT CONNECT INTO SECOND FLOOR DRAIN STACK,
- 30. POTABLE WATER SYSTEM SHALL BE DISINFECTED ON SITE BY BUILDER IN ACCORDANCE WITH APPLICABLE STATE PLUMBING CODES.
- 31. ISLAND FIXTURE VENTING SHALL NOT BE PERMITTED FOR FIXTURES OTHER THAN SINKS AND LAVATURES.. (SEE ISLAND DETAILS).
- 12. ANTI-SIPHONING DEVICE, VACUUM BREAKDERS, AND AIR GAPS: FOR WATER DISTRICTUION SYSTEMS "PROTECTION OF POTABLE WATER SUPPLY".
- 32.1. WATER HEATER LOCATED AT OR ON LIVING SPACE LEVEL MUST HAVE AN ANTI-SIPHONING DEVICE INSTALLED.
- 32.2. CLOTHES WASHER MUST HAVE AN ANTI-SIPHONING DEVICE INSTALLED (IF NOT BUILT INTO THE APPLIANCE).
- 33. WATER HAMMER ARRESTORS SHALL BE INSTALLED WHERE QUICK CLOSING VALVES ARE UTLIZED. (I.E. WASHING MACHINES AND DISHWASHERS).
- PIPE INSTALLED DOWNSTREAM OF THE POINT OF POINT OF DELIVERY SHALL NOT EXTEND THROUGH ANY
  TOWNHOUSE UNIT OTHER THAN THE UNIT SERVED BY SUCH PIPING.









Project ELIZABETH GILLIS

Energy Code: 2015 IECC

Location: Pocasset, Massachusetts

Construction Type: Single-family
Project Type: New Construction

Conditioned Floor Area: **1,898 ft2** Glazing Area **25%** 

Climate Zone: **5 (6297 HDD)** 

Permit Date: Permit Number:

Construction Site: 10 HAROR WAY POCESSET, MA 02559 Owner/Agent: PLEASANT BAY HOMES 256 PLEASANT BAY ROAD HARWICH, MA 02615 PFS Corporation
Northeast Region
APPROVED
H Raup – 3
7/20/17
Approval limited to
Factory Built Portion

Designer/Contractor: ICON LEGACY CMH 246 SAND HILL ROAD SELINSGROVE, PA 17870

#### Compliance: Passes using UA trade-off

Compliance: 5.0% Better Than Code Maximum UA: 299 Your UA: 284

The % Better or Worse Than Code Index reflects how close to compliance the house is based on code trade-off rules. It DOES NOT provide an estimate of energy use or cost relative to a minimum-code home.

### **Envelope Assemblies**

Data filename: Untitled.rck

Assembly	Gross Area or Perimeter	Cavity R-Value	Cont. R-Value	U-Factor	UA
ABOVE COLLAR TIE: Flat Ceiling or Scissor Truss	824	38.0	0.0	0.030	25
BEHIND KNEE WALL: Flat Ceiling or Scissor Truss	107	38.0	0.0	0.030	3
SLOPED CEILING: Cathedral Ceiling	49	19.0	0.0	0.052	3
KNEE WALLS: Wood Frame, 16" o.c.	73	13.0	5.0	0.057	4
HOUSE WALLS: Wood Frame, 16" o.c.	1,811	21.0	0.0	0.057	75
Window 1: Vinyl/Fiberglass Frame:Double Pane with Low-E	314			0.310	97
Door 1: Glass	160			0.250	40
Door 2: Solid	22			0.170	4
Floor 1: All-Wood Joist/Truss:Over Unconditioned Space	990	30.0	0.0	0.033	33

Compliance Statement: The proposed building design described here is consistent with the building plans, specifications, and other calculations submitted with the permit application. The proposed building has been designed to meet the 2015 IECC requirements in REScheck Version 4.6.4 and to comply with the mandatory requirements listed in the REScheck Inspection Checklist.

Project Title: ELIZABETH GILLIS Report date: 07/12/17

Page 1 of 9

# REScheck Software Version 4.6.4 Inspection Checklist

Energy Code: 2015 IECC

Requirements: 0.0% were addressed directly in the REScheck software

Text in the "Comments/Assumptions" column is provided by the user in the REScheck Requirements screen. For each requirement, the user certifies that a code requirement will be met and how that is documented, or that an exception is being claimed. Where compliance is itemized in a separate table, a reference to that table is provided.

Section # & Req.ID	Pre-Inspection/Plan Review	Plans Verified Value	Field Verified Value	Complies?	Comments/Assumptions
103.1, 103.2 [PR1] <sup>1</sup>	Construction drawings and documentation demonstrate energy code compliance for the building envelope. Thermal envelope represented on construction documents.			☐Complies ☐Does Not ☐Not Observable ☐Not Applicable	
103.1, 103.2, 403.7 [PR3] <sup>1</sup>	Construction drawings and documentation demonstrate energy code compliance for lighting and mechanical systems. Systems serving multiple dwelling units must demonstrate compliance with the IECC Commercial Provisions.			□Complies □Does Not □Not Observable □Not Applicable	
302.1, 403.7 [PR2] <sup>2</sup>	Heating and cooling equipment is sized per ACCA Manual S based on loads calculated per ACCA Manual J or other methods approved by the code official.	Heating: Btu/hr Cooling: Btu/hr	Heating: Btu/hr Cooling: Btu/hr	□Complies □Does Not □Not Observable □Not Applicable	

Additional Comments/Assumptions:

PFS Corporation
Northeast Region
APPROVED
H Raup – 3
7/20/17
Approval limited to
Factory Built Portion

1 High Impact (Tier 1) 2 Medium Impact (Tier 2) 3 Low Impact (Tier 3)

Project Title: ELIZABETH GILLIS

Report date: 07/12/17

Data filename: Untitled.rck

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Section # & Req.ID	Foundation Inspection	Complies?	Comments/Assumptions
303.2.1 [FO11] <sup>2</sup>	A protective covering is installed to protect exposed exterior insulation and extends a minimum of 6 in. below	□Complies □Does Not	
•	grade.	□Not Observable □Not Applicable	
403.9 [FO12] <sup>2</sup>	Snow- and ice-melting system controls installed.	$\square$ Complies $\square$ Does Not	
•		□Not Observable □Not Applicable	

**Additional Comments/Assumptions:** 

PFS Corporation
Northeast Region
APPROVED
H Raup – 3
7/20/17
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1 High Impact (Tier 1) 2 Medium Impact (Tier 2) 3 Low Impact (Tier 3)

Project Title: ELIZABETH GILLIS

Report date: 07/12/17

Data filename: Untitled.rck

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Section # & Req.ID	Framing / Rough-In Inspection	Plans Verified Value	Field Verified Value	Complies?	Comments/Assumptions
402.1.1, 402.3.4 [FR1] <sup>1</sup>	Door U-factor.	U	U	□Complies □Does Not □Not Observable □Not Applicable	See the Envelope Assemblies table for values.
402.1.1, 402.3.1, 402.3.3, 402.3.6, 402.5 [FR2] <sup>1</sup>	Glazing U-factor (area-weighted average).	U	U	□Complies □Does Not □Not Observable □Not Applicable	See the Envelope Assemblies table for values.
303.1.3 [FR4] <sup>1</sup>	U-factors of fenestration products are determined in accordance with the NFRC test procedure or taken from the default table.			□Complies □Does Not □Not Observable □Not Applicable	
402.4.1.1 [FR23] <sup>1</sup>	Air barrier and thermal barrier installed per manufacturer's instructions.			□Complies □Does Not □Not Observable □Not Applicable	
402.4.3 [FR20] <sup>1</sup>	Fenestration that is not site built is listed and labeled as meeting AAMA /WDMA/CSA 101/I.S.2/A440 or has infiltration rates per NFRC 400 that do not exceed code limits.			□Complies □Does Not □Not Observable □Not Applicable	
402.4.5 [FR16] <sup>2</sup>	IC-rated recessed lighting fixtures sealed at housing/interior finish and labeled to indicate ≤2.0 cfm leakage at 75 Pa.	PFS Corp	oration	☐Complies ☐Does Not ☐Not Observable ☐Not Applicable	
403.2.1 [FR12] <sup>1</sup>	Supply and return ducts in attics insulated >= R-8 where duct is >= 3 inches in diameter and >= R-6 where < 3 inches. Supply and return ducts in other portions of the building insulated >= R-6 for diameter >= 3 inches and R-4.2 for < 3 inches in diameter.	Northeast APPRO H Rau 7/20/ Approval li	DVED p - 3 <b>17</b>	□Complies □Does Not □Not Observable □Not Applicable	
403.3.3.5 [FR15] <sup>3</sup>	Building cavities are not used as ducts or plenums.	Factory Bui		☐Complies ☐Does Not ☐Not Observable ☐Not Applicable	
403.4 [FR17] <sup>2</sup>	HVAC piping conveying fluids above 105 °F or chilled fluids below 55 °F are insulated to ≥R-3.	R	R	□Complies □Does Not □Not Observable □Not Applicable	
403.4.1 [FR24] <sup>1</sup>	Protection of insulation on HVAC piping.			☐Complies ☐Does Not ☐Not Observable ☐Not Applicable	
403.5.3 [FR18] <sup>2</sup>	Hot water pipes are insulated to ≥R-3.	R	R	□Complies □Does Not □Not Observable □Not Applicable	
403.6 [FR19] <sup>2</sup>	Automatic or gravity dampers are installed on all outdoor air intakes and exhausts.			☐Complies ☐Does Not ☐Not Observable ☐Not Applicable	
	1 High Impact (Tier	1) 2 Medium	Impact (Tier 2)	3 Low Impact (Ti	er 3)

Project Title: ELIZABETH GILLIS Report date: 07/12/17 Data filename: Untitled.rck

#### **Additional Comments/Assumptions:**

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Factory Built Portion

1 High Impact (Tier 1) 2 Medium Impact (Tier 2) 3 Low Impact (Tier 3)

Project Title: ELIZABETH GILLIS

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Section # & Req.ID	Insulation Inspection	Plans Verified Value	Field Verified Value	Complies?	Comments/Assumptions
303.1 [IN13] <sup>2</sup>	All installed insulation is labeled or the installed R-values provided.			☐Complies ☐Does Not ☐Not Observable	
				□Not Applicable	 
402.1.1, 402.2.6 [IN1] <sup>1</sup>	Floor insulation R-value.	R Wood     Steel	R Wood Steel	□Complies □Does Not □Not Observable □Not Applicable	See the Envelope Assemblies table for values.
303.2, 402.2.7 [IN2] <sup>1</sup>	Floor insulation installed per manufacturer's instructions and in substantial contact with the underside of the subfloor, or floor framing cavity insulation is in contact with the top side of sheathing, or continuous insulation is installed on the underside of floor framing and extends from the bottom to the top of all perimeter floor framing members.			□Complies □Does Not □Not Observable □Not Applicable	
402.1.1, 402.2.5, 402.2.6 [IN3] <sup>1</sup>	Wall insulation R-value. If this is a mass wall with at least ½ of the wall insulation on the wall exterior, the exterior insulation requirement applies (FR10).	R Wood Mass Steel	R Wood Mass Steel	□Complies □Does Not □Not Observable □Not Applicable	See the Envelope Assemblies table for values.
303.2 [IN4] <sup>1</sup>	Wall insulation is installed per manufacturer's instructions.			□Complies □Does Not □Not Observable □Not Applicable	

**Additional Comments/Assumptions:** 

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Section # & Req.ID	Final Inspection Provisions	Plans Verified Value	Field Verified Value	Complies?	Comments/Assumptions
402.1.1, 402.2.1, 402.2.2, 402.2.6 [FI1] <sup>1</sup>	Ceiling insulation R-value.	R	R Wood Steel	□Complies □Does Not □Not Observable □Not Applicable	See the Envelope Assemblies table for values.
303.1.1.1, 303.2 [FI2] <sup>1</sup>	Ceiling insulation installed per manufacturer's instructions. Blown insulation marked every 300 ft <sup>2</sup> .			□Complies □Does Not □Not Observable □Not Applicable	
402.2.3 [FI22] <sup>2</sup>	Vented attics with air permeable insulation include baffle adjacent to soffit and eave vents that extends over insulation.			☐Complies ☐Does Not ☐Not Observable ☐Not Applicable	
402.2.4 [FI3] <sup>1</sup>	Attic access hatch and door insulation ≥R-value of the adjacent assembly.	R	R	□Complies □Does Not □Not Observable □Not Applicable	
402.4.1.2 [FI17] <sup>1</sup>	Blower door test @ 50 Pa. <=5 ach in Climate Zones 1-2, and <=3 ach in Climate Zones 3-8.	ACH 50 =	ACH 50 =	□Complies □Does Not □Not Observable □Not Applicable	
403.2.3 [FI4] <sup>1</sup>	Duct tightness test result of <=4 cfm/100 ft2 across the system or <=3 cfm/100 ft2 without air handler @ 25 Pa. For rough-in tests, verification may need to occur during Framing Inspection.	cfm/100 ft <sup>2</sup>	cfm/100 ft²	□Complies □Does Not □Not Observable □Not Applicable	
403.3.2 [FI27] <sup>1</sup>	Ducts are pressure tested to determine air leakage with either: Rough-in test: Total leakage measured with a pressure differential of 0.1 inch w.g. across the system including the manufacturer's air handler enclosure if installed at time of test. Postconstruction test: Total leakage measured with a pressure differential of 0.1 inch w.g. across the entire system including the manufacturer's air handler enclosure.	cfm/100	cfm/100 ft <sup>2</sup>	□Complies □Does Not □Not Observable □Not Applicable	
403.3.2.1 [FI24] <sup>1</sup>	Air handler leakage designated by manufacturer at <=2% of design air flow.			☐Complies ☐Does Not ☐Not Observable ☐Not Applicable	
403.1.1 [FI9] <sup>2</sup>	Programmable thermostats installed for control of primary heating and cooling systems and initially set by manufacturer to code specifications.	PFS Corpo Northeast F	Region	□Complies □Does Not □Not Observable □Not Applicable	
403.1.2 [FI10] <sup>2</sup>	Heat pump thermostat installed on heat pumps.	APPROV H Raup 7/20/17	- 3 '	☐Complies ☐Does Not ☐Not Observable ☐Not Applicable	
403.5.1 [FI11] <sup>2</sup>	Circulating service hot water systems have automatic or accessible manual controls.	Approval lim Factory Built		□Complies □Does Not □Not Observable □Not Applicable	
	1 High Impact (Tier	1) 2 Medium	Impact (Tier 2)	3 Low Impact (Ti	ier 3)

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Final Inspection Provisions	Plans Verified Value	Field Verified Value	Complies?	Comments/Assumptions
All mechanical ventilation system fans not part of tested and listed HVAC equipment meet efficacy and air flow limits.			□Complies □Does Not □Not Observable □Not Applicable	
Hot water boilers supplying heat through one- or two-pipe heating systems have outdoor setback control to lower boiler water temperature based on outdoor temperature.			☐Complies ☐Does Not ☐Not Observable ☐Not Applicable	
Heated water circulation systems have a circulation pump. The system return pipe is a dedicated return pipe or a cold water supply pipe. Gravity and thermossyphon circulation systems are not present. Controls for circulating hot water system pumps start the pump with signal for hot water demand within the occupancy. Controls automatically turn off the pump when water is in circulation loop is at set-point temperature and no demand for hot water exists.			□Complies □Does Not □Not Observable □Not Applicable	
Electric heat trace systems comply with IEEE 515.1 or UL 515. Controls automatically adjust the energy input to the heat tracing to maintain the desired water temperature in the piping.	Northeast	Region	□Complies □Does Not □Not Observable □Not Applicable	
Water distribution systems that have recirculation pumps that pump water from a heated water supply pipe back to the heated water source through a cold water supply pipe have a demand recirculation water system. Pumps have controls that manage operation of the pump and limit the temperature of the water entering the cold water piping to $104^{\circ}F$ .	H Raup 7/20/1 Approval lin	- 3 7 nited to	□Complies □Does Not □Not Observable □Not Applicable	
Drain water heat recovery units tested in accordance with CSA B55.1. Potable water-side pressure loss of drain water heat recovery units < 3 psi for individual units connected to one or two showers. Potable waterside pressure loss of drain water heat recovery units < 2 psi for individual units connected to three or more showers.			□Complies □Does Not □Not Observable □Not Applicable	
75% of lamps in permanent fixtures or 75% of permanent fixtures have high efficacy lamps. Does not apply to low-voltage lighting.			□Complies □Does Not □Not Observable □Not Applicable	
Fuel gas lighting systems have no continuous pilot light.			□Complies □Does Not	
	All mechanical ventilation system fans not part of tested and listed HVAC equipment meet efficacy and air flow limits.  Hot water boilers supplying heat through one- or two-pipe heating systems have outdoor setback control to lower boiler water temperature based on outdoor temperature.  Heated water circulation systems have a circulation pump. The system return pipe is a dedicated return pipe or a cold water supply pipe. Gravity and thermossyphon circulation systems are not present. Controls for circulating hot water system pumps start the pump with signal for hot water demand within the occupancy. Controls automatically turn off the pump when water is in circulation loop is at set-point temperature and no demand for hot water exists.  Electric heat trace systems comply with IEEE 515.1 or UL 515. Controls automatically adjust the energy input to the heat tracing to maintain the desired water temperature in the piping.  Water distribution systems that have recirculation pumps that pump water from a heated water supply pipe back to the heated water source through a cold water source through a cold water supply pipe have a demand recirculation water system. Pumps have controls that manage operation of the pump and limit the temperature of the water entering the cold water piping to 104°F.  Drain water heat recovery units tested in accordance with CSA B55.1. Potable water-side pressure loss of drain water heat recovery units < 3 psi for individual units connected to one or two showers. Potable water-side pressure loss of drain water heat recovery units < 2 psi for individual units connected to one or two showers. Potable water-side pressure loss of drain water heat recovery units < 2 psi for individual units connected to three or more showers.  75% of lamps in permanent fixtures or 75% of permanent fixtures have high efficacy lamps. Does not apply to low-voltage lighting.  Fuel gas lighting systems have	All mechanical ventilation system fans not part of tested and listed HVAC equipment meet efficacy and air flow limits.  Hot water boilers supplying heat through one- or two-pipe heating systems have outdoor setback control to lower boiler water temperature based on outdoor temperature. Heated water circulation systems have a circulation pump. The system return pipe is a dedicated return pipe or a cold water supply pipe. Gravity and thermossyphon circulation systems are not present. Controls for circulating hot water system pumps start the pump with signal for hot water demand within the occupancy. Controls automatically turn off the pump when water is in circulation loop is at set-point temperature and no demand for hot water exists.  Electric heat trace systems comply with IEEE 515.1 or UL 515. Controls automatically adjust the energy input to the heat tracing to maintain the desired water temperature in the piping.  Water distribution systems that have recirculation water supply pipe have a demand recirculation water system. Pumps have controls that manage operation of the pump and limit the temperature of the water entering the cold water surply pipe have a demand recirculation water system. Pumps have controls that manage operation of the pump and limit the temperature of the water entering the cold water piping to 104°F.  Drain water heat recovery units tested in accordance with CSA B55.1. Potable water-side pressure loss of drain water heat recovery units < 2 psi for individual units connected to one or two showers. Potable water-side pressure loss of drain water heat recovery units < 2 psi for individual units connected to three or more showers.  75% of lamps in permanent fixtures or 75% of permanent fixtures have high efficacy lamps. Does not apply to low-voltage lighting.  Fuel gas lighting systems have	All mechanical ventilation system fans not part of tested and listed HVAC equipment meet efficacy and air flow limits.  Hot water boilers supplying heat through one- or two-pipe heating systems have outdoor setback control to lower boiler water temperature based on outdoor temperature. Heated water circulation pump. The system return pipe is a dedicated return pipe or a cold water supply pipe. Gravity and thermossyphon circulation systems are not present. Controls for circulating hot water system pumps start the pump with signal for hot water system pumps start the pump with signal for hot water is in circulation loop is at set-point temperature and no demand for hot water exists.  Electric heat trace systems comply with IEEE 515.1 or U. 515. Controls automatically turn off the pump when water is in circulation loop is at set-point temperature and no demand for hot water exists.  Electric heat trace systems comply with IEEE 515.1 or U. 515. Controls automatically adjust the energy input to the heat tracing to maintain the desired water temperature in the piping.  PFS Corporation Northeast Region APPROVED  H Raup - 3 7/20/17  Approval limited to Factory Built Portion  PFS Corporation Northeast Region APPROVED  H Raup - 3 7/20/17  Approval limited to Factory Built Portion  Proval Immited to Factory Built Portion	All mechanical ventilation system fans not part of tested and listed HVAC equipment meet efficacy and air flow limits.  Hot water boilers supplying heat through one- or two-pipe heating systems have outdoor setback control to lower boiler water temperature based on outdoor temperature. Heated water circulation systems have a circulation pump. The system return pipe is a dedicated return pipe or a cold water supply pipe. Gravity and thermosysyphm circulation systems are not present. Controls for circulating hot water system pumps start the pump with signal for hot water demand within the occupancy. Controls automatically adjust the energy input to the heat tracing to maintain the desired water temperature in the desired water temperature in the desired water supply pipe back to the heated water supply pipe have a demand recirculation water system. Pumps have controls that manage operation of the pump and limit the temperature of the water entering the cold water supply pipe have a demand recirculation water system. Pumps have controls that manage operation of the pump and limit the temperature of the water entering the cold water supply pipe have a demand recirculation water system. Pumps have controls that manage operation of the pump and limit the temperature of the water entering the cold water supply pipe sos of drain water heat recovery units <a href="mailto:special-water-side">special-water-side</a> possor of the pump and limit the temperature of the water entering the cold water supply pipe have a demand recirculation water system. Pumps have controls that manage operation of the pump and limit the semperature of the water supply pipe sos of drain water heat recovery units <a href="mailto:special-water-side">special-water-side</a> possor of special wa

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Section # & Req.ID	Final Inspection Provisions	Plans Verified Value	Field Verified Value	Complies?	Comments/Assumptions
401.3 [FI7] <sup>2</sup>	Compliance certificate posted.			□Complies □Does Not	
				□Not Observable □Not Applicable	
303.3 [FI18] <sup>3</sup>	Manufacturer manuals for mechanical and water heating systems have been provided.			☐Complies ☐Does Not ☐Not Observable ☐Not Applicable	

**Additional Comments/Assumptions:** 

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Insulation Rating	R-Value	
Above-Grade Wall	21.00	
Below-Grade Wall	0.00	
Floor	30.00	
Ceiling / Roof	38.00	
Ductwork (unconditioned spaces):		
Glass & Door Rating	U-Factor	SHGC
Window	0.31	
Door	0.25	
Heating & Cooling Equipment	Efficiency	
Heating System:		
Cooling System:		
Water Heater:		
Name:	Date:	
Comments		

Comments

**PFS** Corporation Northeast Region **APPROVED** H Raup - 3 7/20/17 **Approval limited to Factory Built Portion** 



# HIGH WIND CALCULATIONS FOR

# ICON - LEGACY CUSTOM MODULAR HOMES, LLC

SELINSGROVE, PA

O#6861

ASCE 7-05, RISK CATEGORY II,  $V_{asd}$  110 MPH, VELOCITY PRESSURE q=25.81~psf WIND EXPOSURE: C

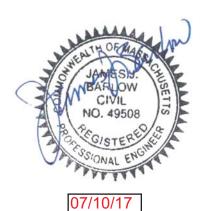


07/10/17

PREPARED BY:
BARLOW ENGINEERING, P.C.
6512 SIX FORKS RD, SUITE 203B
RALEIGH, NC 27615

#### **INDEX**

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SECTION 4 ALTERNATE CALCULATIONS	P48-49





#### **NARRATIVE**

170394 0278nec2017 Legacy O#6861 Two-Story 27.5' x 39'

Roof Slope: 4.71:12 Wind Speed: 110 mph V<sub>asd</sub>

Risk Category II
Exposure C
MA
Ethan Loewenthal
7/6/17



It is assumed that the structure will be placed over a basement foundation system. The mean roof height (MRH) of the structure is adjusted per manufacturer drawings.

Ensure that the foundation is structurally adequate for the shear, uplift and downward point loads imposed at corner connections and similar locations.

The structure was analyzed using ASCE 7-05 basic wind speed ( $V_{asd}$  – nominal design 3 sec. gust mph) = 110 mph.

The house was modeled as a 5/12.

Where 2<sup>nd</sup> story overturning uplifts occur above 1<sup>st</sup> story openings, the 2<sup>nd</sup> floor band was designed to transfer the point loads to the edges of the openings on the 1<sup>st</sup> story.

A 1<sup>st</sup> story offset shearwall was designed. Because of the offset, tributary lengths were used to calculate the load on this offset wall, as well as the 1<sup>st</sup> story endwalls.

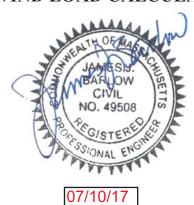
Where the 2<sup>nd</sup> story Endwall #2 does not align with the 1<sup>st</sup> story Endwall #2 below, the 2<sup>nd</sup> floor diaphragm was designed to transfer the shear load.

Tension connections were designed at ceiling and floor levels to carry shearwall loads across the matelines.



# **Section 1**

# **ASCE 7-05 WIND LOAD CALCULATIONS**





FIRST FLOOR WIDTH: DESIGN INPUTS: 27.50 ft 27.50 ft SECOND FLOOR WIDTH: THIRD FLOOR WIDTH: 0.00 ft FOURTH FLOOR WIDTH: 0.00 ft FIRST FLOOR LENGTH: 39.00 ft SECOND FLOOR LENGTH: 33.00 ft THIRD FLOOR LENGTH: 0.00 ft FOURTH FLOOR LENGTH: 0.00 ft ROOF SPAN (RS): 27.50 ft STUD SPACING: 16 in TRUSS SPACING: 16 in 5 / 12 22.62 ° ROOF PITCH: ROOF ANGLE (  $\Theta$  ): RAFTER LENGTH (L) = 14.90 ft 30.00 ft hr = 5.73 ft 2 87 ft hr / 2 = h= **30.00** ft WALL EFFECTIVE WIND AREA = h<sub>s</sub> x STUD SPACING = 21.33 74.00 ft<sup>2</sup> ROOF EFFECTIVE WIND AREA = L x TRUSS SPACING = 0.17 ft<sup>2</sup> MIN. WALL & ROOF EFFECTIVE AREA FOR FASTENERS =

NO. OF STORIES: 1st FLOOR WALL HEIGHT: 8.00 ft 2nd FLOOR WALL HEIGHT: 8.00 ft 3rd FLOOR WALL HEIGHT: 0.00 4th FLOOR WALL HEIGHT: 0.00 ft WIND SPEED: 110 WIND EXPOSURE CASE: С

> ( WIND BORNE DEBRIS PROTECTION IS REQUIRED FOR HURRICANE PRONE REGIONS )

(IF ROOF SLOPE <= 10 DEGREES, USE EAVE HEIGHT)
(EFFECTIVE WIDTH NEED NOT BE LESS THAN 8t/3 = 2.66 ft)
(EFFECTIVE WIDTH NEED NOT BE LESS THAN 14.9ft/3 = 4.96 ft)
(WORST CASE: 2" o.c. FASTENERS WITH 12" o.c. FRAMING)

 $a=10\%\ \text{OF LEAST HORIZONTAL DIMENSION OR }0.4\text{h, WHICHEVER IS SMALLER, BUT NOT LESS THAN EITHER }4\%$  OF LEAST HORIZONTAL DIMENSION OR 3 ft. (p. 54, FIG. 6-10, NOTATION 9.a)

a: 0.1W = 0.1 \* 27.5 ft = 2.75 ft

OR

0.4h = 0.4 \* 30 ft = 12 ft

LESSER =

2.75 ft

AND NOT LESS THAN EITHER:

0.04W = 0.04 \* 27.5 ft = 1.1 ft

OR 3 ft:

a = 3 ft

0.85

25.81

25.81

0.85

0.18

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Bloomsburg, PA

#### DETERMINE WIND LOADS PER ASCE 7-05:

#### MAIN WIND FORCE RESISTING SYSTEM:

#### CONSTANTS:

WIND VELOCITY (V):	110 mph
VEL. PRESS. EXP. COEF. (Kh):	0.98
VEL. PRESS. EXP. COEF. (Kz):	0.98
MULT. for TOPO. FACTOR (K <sub>1</sub> ):	0.09
MULT. for TOPO. FACTOR (K2):	0
MULT. for TOPO. FACTOR (K <sub>3</sub> ):	0
$K_{Zi}$ : = $(1 + K_1 x K_2 x K_3)^2$ =	1

PER TABLE 6-6, ASCE 7-05, pp 49, "EXTERNAL PRESSURE COEFFICIENTS, Cp"

#### WALL PRESSURE COEFICIENTS

WALL FRESSORE COEFICIENTS			
SURFACE		Ср	USE WITH
WINDWARD WALL	ALL	0.8	qz
LEEWARD WALL	SIDE	-0.5	qh
LEEWARD WALL	END	-0.4	qh
SIDE WALL	ALL	-0.7	qh

#### ROOF PRESSURE COEFICIENTS FOR USE WITH qh NORMAL TO RIDGE (WIND FROM SIDEWALL)

DIRECTIONALITY FACTOR (K<sub>r</sub>):

 $q_h$ : = .00256 x  $K_h$  x  $K_{2t}$  x Kd x  $V^2$  =

 $q_z$ : = .00256 x  $K_z$  x  $K_{z1}$  x Kd x  $V^2$  =

GUST EFFECT FACTOR (G):

INTERNAL PRESS. COEF. (GCpi1):

Cp - WINDWARD WALL	-0.60
	-0.10
Cp - LEEWARD WALL	0.60

#### PARALLEL TO RIDGE (WIND FROM ENDWALL)

Cp - 0 TO h/2	-1.17
Cp - h/2 TO h	-1.17
Cp - h TO 2h	-1.17
Cp - > 2h	-1.17
Ср	-0.18

#### LATERAL LOADS:

EXTERNAL PRESSURE COEFFICIENTS: 22.62 ° ROOF

#### CASE A - WIND FROM SIDE WALL:

SIDE WALL:	$GC_{pf1} =$	0.54	$GC_{pf1E} =$	0.77
SIDF WALL:	GC =	-0.41	GC-m =	-0.60

#### LOAD CALCULATIONS (WIND FROM SIDE WALL):

P = q GCp - qi (GCpi)

EXAMPLE:

 $P = qh \ GCp - qi \ (GCpi)$  = (25.81 psf x 0.85 x 0.8) - (25.81 x 0.18) = 12.9 psf  $P = qh \ GCp - qi \ (GCpi)$  = (25.81 psf x 0.85 x 0.8) - (25.81 x -0.18) = 22.2 psf

WINDWARD	P = 12.90 psf
WINDWARD	P = 22.20 psf
LEEWARD	P = -15.60 psf
LEEWARD	P = -6.30 psf

WINDWARD	P=	-6.84	psf	
WINDWARD	P =	2.45	psf	
LEEWARD	P =	8.52	psf	
LEEWARD	P =	17.81	nef	

WINDWARD SIDE: ROOF SIDE:

-						
ı	USE	28.50	psf WIND LOAD	USE	-5.91	psf WIND LOAD

#### CASE B - WIND FROM END WALL:

ENDWALL:	$GC_{pf1} =$	0.4	$GC_{pf1E} =$	0.61
ENDWALL:	GC <sub>pf4</sub> =	-0.29	GC <sub>pf4E</sub> =	-0.43

#### LOAD CALCULATIONS (WIND FROM END WALL):

P = q GCp - qi (GCpi)

EXAMPLE:

 $P = qz \ GCp - qi \ (GCpi)$  =  $(25.81 \ psf \times 0.85 \times 0.8) - (25.81 \times 0.18) = 12.9 \ psf$  $P = qz \ GCp - qi \ (GCpi)$  =  $(25.81 \ psf \times 0.85 \times 0.8) - (25.81 \times -0.18) = 22.2 \ psf$ 

_					
ſ	WINDWARD	P=	12.90	psf	
Γ	WINDWARD	P=	22.20	psf	
E	LEEWARD	P=	-13.40	psf	
Г	LEEWARD	P =	-4.10	psf	

#### WINDWARD SIDE:

USE	26.30	psf WIND LOAD	

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#### **UPLIFT LOADS:**

EXTERNAL PRESSURE COEFFICIENTS:

22.62 ° ROOF

CASE A - WIND FROM SIDE WALL:

#### LOAD CALCULATIONS (WIND FROM SIDE WALL):

P = q GCp - qi (GCpi)

EXAMPLE:

P = qh GCp - qi (GCpi) = (25.81 psf x 0.85 x -0.6) - (25.81 x 0.18) = -17.8 psf

P = qh GCp - qi (GCpi) = (25.81 psf x 0.85 x -0.6) - (25.81 x -0.18) = -8.5 psf

WINDWARD	P =	-17.80 psf	
WINDWARD	P =	-8.50 psf	
WINDWARD	P =	-6.80 psf	
WINDWARD	P =	2.50 psf	

LEEWARD	P =	8.50 psf	
LEEWARD	P =	17.80 psf	

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WINDWARD SIDE:

USE	-17.80	psf WIND LOAD
USE	2.50	psf WIND LOAD

USE 8.50 psf WIND LOAD

THE MAXIMUM UPLIFT LOAD FOR 110 mph CASE A - WIND FROM SIDE WALL (MWFRS) IS -17.80 psf.

#### CASE B - WIND FROM END WALL:

#### LOAD CALCULATIONS (WIND FROM END WALL):

P = q GCp - qi (GCpi)

EXAMPLE:

P = qh GCp - qi (GCpi) = (25.81 psf x 0.85 x -1.17) - (25.81 x 0.18) = -30.3 psf

P = qh GCp - qi (GCpi) = (25.81 psf x 0.85 x -0.18) - (25.81 x -0.18) = -21 psf

٧	VINDWARD	P =	-30.30 psf	
٧	VINDWARD	P =	-21.00 psf	
	LEEWARD	P =	-8.60 psf	
	LEEWARD	P=	0.70 psf	



LEEWARD SIDE:

USE -30.30 psf WIND LOAD

USE -8.60 psf WIND LOAD

# CALCULATE LOADING ON BUILDING

#### LATERAL LOADS FROM WIND:

#### WIND PERPENDICULAR TO RIDGE:

WINDWARD SIDE:

WINDWARD SIDE:

LICE	28.50	psf WIND LOAD
USE	28.50	pst wind LOAD

WIND PRESSURE (w) = 28.5 psf

MAX. WALL HEIGHT (H) = 8.00 ft

LAT = w \* H / 2 = 28.5 psf \* 8 ft / 2 = LAT = 114 plf

THE MAXIMUM UPLIFT LOAD FOR 110 mph CASE B - WIND FROM END WALL (MWFRS) IS -30.30 psf.

#### WIND PARALLEL TO RIDGE:

WINDWARD SIDE:

USE 26.30 psf WIND LOAD

WIND PRESSURE (w) = 26.3 psf

MAX. WALL HEIGHT (H) = 13.730 ft (INCLUDES GABLE)

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#### **UPLIFT LOADS FROM WIND:**

#### WIND PERPENDICULAR TO RIDGE:

USE

WINDWARD SIDE:

LEEWARD SIDE:

USE 8.50 psf WIND LOAD

USE -8.60 psf WIND LOAD

USE -17.80 psf WIND LOAD 2.50 psf WIND LOAD

> 17.8 psf WIND PRESSURE (w) =

MAX. RAFTER LENGTH (L) = 14.90 ft

> LAT = w \* H / 2 =17.8 psf \* 14.9 ft / 2 = LAT = 133 plf

#### WIND PARALLEL TO RIDGE:

WINDWARD SIDE:

LEEWARD SIDE:

WIND PRESSURE (w) = 30.3 psf

MAX. ROOF LENGTH (L) = 14.900 ft

> LAT = w \* H / 2 = 30.3 psf \* 14.9 ft / 2 =

> > ft

ft

LAT = 226 plf

**UPLIFT LOADING:** 

ROOF SPAN (RS) = 27.50 ROOF PITCH: 5 / 12 WIND PRESSURE =

ESSURE = 30.3 psf
UPLIFT = WIND PRESSURE \* COS()\*ROOF SPAN/2 ft 384.609 / 12

THIS IS THE UPLIFT IN THE SIDEWALL FROM TRUSS/ROOF psf

USE -30.30 psf WIND LOAD

FROM TRUSS/ROOF

DATE 7/20/17 PFS CORPORATION Bloomsburg, PA



LATERAL LOADING:

ft ft MAX. FLOOR WIDTH (W) = MAX. FLOOR LENGTH (L) = 39.00 ROOF SPAN (RS) = 27.50 ROOF PITCH: 5 ROOF ANGLE (θ)= 22.62 MAX. WALL HEIGHT (H) = 8.00 psf RIDGE ROOF HEIGHT (hr)= 5.73 2.5 28.5 psf \* 8 ft= EDGE ROOF HEIGHT (he)= plf (w/ 0.6 FACTOR)

CALCULATE LATERAL PRESSURE AT FLOOR: (PERPENDICULAR TO RIDGE)

 $W_{LAT}$  = 28.5 psf  $w_{FL}$  =  $W_{LAT}$  \* H =  $w_{FL}$  = 228 26.3 psf \* 8 ft=

CALCULATE LATERAL PRESSURE AT FLOOR: (PARALLEL TO RIDGE)

 $W_{LAT} = 26.3$   $W_{FL} = W_{LAT} * H = W_{FL} = 210$  114 plf ) (ASCE 7-10 FIGURE 27.4-1 NOTE 6)

 ${\bf CALCULATE\ LATERAL\ PRESSURE\ @\ ROOF:\ (PERPENDICULAR\ TO\ RIDGE)}$ 

Sin () = 0.38443063  $\begin{aligned} w_{R,PER} &= & Wmax(roof) * hr*SIN() + w_{FL} / 2 = \\ w_{R,PER} &= & 30.3 \text{ psf} * 2.20279997301131 \text{ ft} + 228 \text{ plf} / 2 = \end{aligned}$ 

(BUT NO LESS THAN: 228 plf / 2 = 114 plf ) (ASCE 7-10 FIGURE 27.4-1 NOTE 6)

w<sub>R-PER</sub> = 180.75 **plf** 

CALCULATE LATERAL PRESSURE @ ROOF: (PARALLEL TO RIDGE)

GABLE AREA ( $A_T$ ) = RS \* hr / 2 =  $A_T$  = 27.5 ft \* 5.73 ft / 2 =  $A_T$  = 78.79 lbs



TOTAL WIND LOAD (P<sub>w</sub>) =  $(A_T - A_e)^* w_{rf} + A_e^* w_{re} = P_w = (78.79 \text{ ft}^2)^* 26.3 \text{ psf} = P_w = 2072$ 

 $W_{R-PAR} = P_w / R + W_f / 2 = mph$ W<sub>R-PAR</sub> = 2072 lbs / 27.5 ft + 210 plf / 2 = W<sub>R-PAR</sub> = 180 **plf** 

#### DETERMINE WIND LOADS PER ASCE 7-05 FOR ALL-HEIGHT BUILDINGS:

#### COMPONENTS AND CLADDING:

CONSTANTS:	WIND VELOCITY (V):	110
	VEL. PRESS. EXP. COEF. (Kz):	0.98
	MULT. for TOPO. FACTOR (K <sub>1</sub> ):	0.09
	MULT. for TOPO. FACTOR (K2):	0.00
	MULT. for TOPO. FACTOR (K <sub>3</sub> ):	0.00
	$K_{2i}$ : = $(1 + K_1 x K_2 x K_3)^2$ =	1.00

#### LATERAL LOADS (COMPONENTS AND CLADDING):

EXTERNAL PRESSURE COEFFICIENTS:

SIDE WALL: FIELD: GC<sub>pf4</sub> = -1.00 EDGE: GC<sub>pf5</sub> = -1.16

#### LOAD CALCULATIONS:

 $P = q_h x (GC_{pf} - GC_{pi})$ 

EXAMPLE:

 $P_{4i} = q_h x (GC_{pf4} - GC_{pi4})$ = 25.81 psf \* [ ( -1 - 0.18 ) ] = -30.46 psf

 $P_{4i} = q_h x (GC_{pt4} - GC_{pi4})$ = 25.81 psf \* [ ( -1 - -0.18 ) ] = -21.17 psf

FIELD:	P <sub>4i</sub> =	-30.46	psf
FIELD:	P <sub>4i</sub> =	-21.17	psf
EDGE:	P <sub>5i</sub> =	-34.59	psf
EDGE:	P <sub>5i</sub> =	-25.30	psf

#### UPLIFT LOADS (COMPONENTS AND CLADDING):

EXTERNAL PRESSURE COEFFICIENTS:

FIELD: GC<sub>pf1</sub> = EDGE: GC<sub>pf2</sub> = -1.27 OVERHANG:  $GC_{pf3} = DOWNWARD$ :  $GC_{pf1-3} = C_{pf1-3} = C_{pf1-3} = C_{pf1-3} = C_{pf1-3}$ -2.20 0.37

#### LOAD CALCULATIONS:

 $P_h = q_h x (GC_p - GC_{pi})$ 

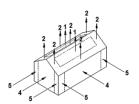
EXAMPLE:

 $P_h = q_h x (GC_{pf1} - GC_{pi1})$ = 25.81 psf \* [ ( -0.81 - 0.18 ) ] = -25.56 psf

= 25.81 psf \* [ ( -0.81 - -0.18 ) ] = -16.27 psf  $P_{1i} = q_h x (GC_{pf1} - GC_{pi1})$ 

FIELD:	P <sub>1i</sub> =	-25.56	psf
FIELD:	P <sub>1i</sub> =	-16.27	psf

DIRECTIONALITY FACTOR ( $K_d$ ):	0.85
$q_z$ : = .00256 x $K_z$ x $K_{zt}$ x $Kd$ x $V^2$ = $q_t$ = $q_h$ = $q_z$ =	25.81 25.81
GUST EFFECT FACTOR (G):	0.85
INTERNAL PRESS. COEF. (GCpi):	0.18
	-0.18



USE -18.28 psf WIND LOAD FOR FIELD.
USE -20.75 psf WIND LOAD FOR EDGE.

\*(W/ 0.6 FACTOR)

USE	-15.34	psf WIND LOAD FOR FIELD.
USE	-22.46	psf WIND LOAD FOR EDGE.
USE	-36.86	psf WIND LOAD FOR OVERHANG.
USE	8.52	psf DOWNWARD WIND LOAD.

\*\*(W/ 0.6 FACTOR)



EDGE:	P <sub>2i</sub> =	-37.43	psf
EDGE:	P <sub>2i</sub> =	-28.14	psf
OVERHANG:	P <sub>3i</sub> =	-61.43	psf
OVERHANG:	P <sub>3i</sub> =	-52.14	psf
DOWNWARD:	P <sub>1-3i</sub> =	4.91	psf
DOWNWARD:	P <sub>1-3i</sub> =	14.20	psf

DIRECTIONALITY FACTOR (K<sub>d</sub>): 0.85 mph

$q_z$ : = .00256 x $K_z$ x $K_{z1}$ x Kd x	$V^2 = 25.81$
$q_i = q_h$ :	$= q_z = 25.81$
DETERMINE WIND LOADS PER ASCE 7-05 FOR ALL-HEIGHT BUILDINGS:  GUST EFFECT FACTOR	R (G): 0.85
INTERNAL PRESS. COEF. (0	GC <sub>pi</sub> ): 0.18
COMPONENTS AND CLADDING: FOR FASTENERS ONLY (EFFECTIVE AREA SHALL BE NO GREATER THAN FASTENER TRIBUTAR	-0.18

#### DETERMINE WIND LOADS PER ASCE 7-05 FOR ALL-HEIGHT BUILDINGS:

CONSTANTS:	WIND VELOCITY (V):	110
	VEL. PRESS. EXP. COEF. (Kz):	0.98
	MULT. for TOPO. FACTOR (K <sub>1</sub> ):	0.09
	MULT. for TOPO. FACTOR (K2):	0.00
	MULT. for TOPO. FACTOR (K <sub>3</sub> ):	0.00

 $K_{21}$ : =  $(1 + K_1 \times K_2 \times K_3)^2$  =

LATERAL LOADS (COMPONENTS AND CLADDING):

EXTERNAL PRESSURE COEFFICIENTS:

SIDE WALL: ) (ZONE 4): GC<sub>pf4</sub> = EDGE (ZONE 5): GC<sub>pf5</sub> = -1.40

LOAD CALCULATIONS:

 $P = q_h x (GC_{pf} - GC_{pi})$ 

EXAMPLE:

 $P_{4i} = q_h x (GC_{pf4} - GC_{pi4})$ = 25.81 psf \* [ ( -1.1 - 0.18 ) ] = -33.04 psf = 25.81 psf \* [ ( -1.1 - -0.18 ) ] = -23.75 psf  $P_{4i} = q_h x (GC_{pf4} - GC_{pi4})$ 

FIELD (ZONE 4):	P <sub>4i</sub> =	-33.04	psf
FIELD (ZONE 4):	P <sub>4i</sub> =	-23.75	psf
EDGE (ZONE 5):	P <sub>5i</sub> =	-40.78	psf
FDGE (ZONE 5):	Pc: =	-31.49	psf

#### UPLIFT LOADS (COMPONENTS AND CLADDING):

EXTERNAL PRESSURE COEFFICIENTS:

ROOF: ) (ZONE 1):	GC <sub>pf1</sub> =	-0.90
EDGE (ZONE 2):	GC <sub>pf2</sub> =	-1.70
CORNER (ZONE 3):	$GC_{pf3} =$	-2.60
CORNER OH (ZONE 3):	GC =	-3.70

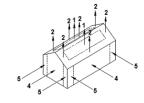
#### LOAD CALCULATIONS:

 $P_h = q_h x (GC_p - GC_{pi})$ 

EXAMPLE:

 $P_h = q_h x (GC_{pf1} - GC_{pi1})$ = 25.81 psf \* [ ( -0.9 - 0.18 ) ] = -27.88 psf  $P_{1i} = q_h x (GC_{pf1} - GC_{pi1})$ = 25.81 psf \* [ ( -0.9 - -0.18 ) ] = -18.59 psf

FIELD (ZONE 1): P<sub>1i</sub> = -27.88 psf



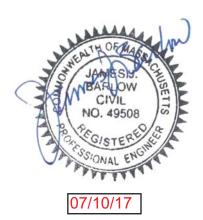
USE 19.82 psf WIND LOAD FOR FIELD. 24.47 psf WIND LOAD FOR EDGE.

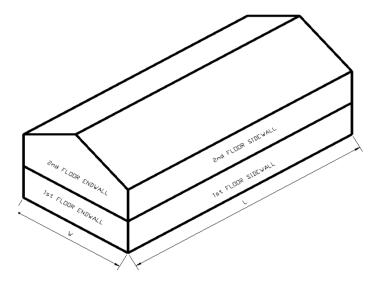
16.73 psf WIND LOAD FOR FIELD (ZONE 1). USE 29.12 psf WIND LOAD FOR EDGE (ZONE 2). 43.06 psf WIND LOAD FOR CORNER (ZONE 3). USE 60.09 psf WIND LOAD FOR CORNER OH (ZONE 3).

\*\*(W/ 0.6 FACTOR)



# **Section 2** SHEAR WALL CALCULATIONS







#### BUILDING INFORMATION:

JOB NUMBER =	170394	
PLAN NAME / NUMBER = 0#6861		
FIRST FLOOR WIDTH (W1) =	27.5	ft
SECOND FLOOR WIDTH (W2) =	27.5	ft
FIRST FLOOR LENGTH $(L_1)$ =	39	ft
SECOND FLOOR LENGTH (L2) =	33	ft
ROOF SPAN =	27.5	ft
TRUSS SPACING (TOC)=	16	in
STUD SPACING (SOC) =	16	in
WIND SPEED (V3S) =	110	mph
EXPOSURE FACTOR =	С	

#### SHEARWALL SUMMARY:

SHEATHING FASTENING MUST USE THE MORE RESTRICTIVE FASTENING OF THAT SPECIFIED FOR SHEARWALL SHEATHING FASTENING AND SHEATHING SUCTION FASTENING

FIRST FLOOR ENDWALL #1: 7/16" OSB EXTERIOR (BLOCKED) w/ 7/16" OSB INTERIOR (BLOCKED)

FAMILY / DINING WITH 8d COMMON NAILS SPACED AT 2" EDGE \*\*\* SEGMENTED SHEARWALL - HOLDDOWNS REQUIRED AT EACH SEGMENT END \*\*\*

\*\*\* DOUBLE FRAMING MEMBERS AND DOUBLE BOTTOM PLATE REQUIRED AT PANEL EDGES, STAGGERED NAILING AT ALL PANEL EDGES ARE REQUIRED.

FIRST FLOOR ENDWALL #2: 7/16" OSB EXTERIOR (BLOCKED) w/ 7/16" OSB INTERIOR (BLOCKED) FOYER / MECH. ROOM WITH 8d COMMON NAILS SPACED AT 3" EDGE

\*\*\* SEGMENTED SHEARWALL - HOLDDOWNS REQUIRED AT EACH SEGMENT END \*\*\*

FIRST FLOOR OFFSET SHEARWALL: 7/16" OSB EXTERIOR (BLOCKED) w/ 7/16" OSB INTERIOR (BLOCKED)

BEDROOM #1 WITH 8d COMMON NAILS SPACED AT 6" EDGE

FIRST FLOOR SIDEWALL #1: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR FAMILY / BEDROOM #1 WITH 8d COMMON NAILS SPACED AT 6" EDGE

FIRST FLOOR SIDEWALL #2: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR DINING / MECH. ROOM WITH 8d COMMON NAILS SPACED AT 6" EDGE

SECOND FLOOR ENDWALL #1: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR

SECOND FLOOR ENDWALL #2: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR BEDROOMS #2 & #3 WITH 8d COMMON NAILS SPACED AT 4" EDGE

SECOND FLOOR SIDEWALL #1: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR BEDROOM #2 WITH 8d COMMON NAILS SPACED AT 6" EDGE

SECOND FLOOR SIDEWALL #2: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR

SITTING / BEDROOM #3 WITH 8d COMMON NAILS SPACED AT 6" EDGE

ROOF SHEATHING: 7/16" OSB (UN-BLOCKED) w/ 8d NAILING @ 6"/12"

CEILING SHEATHING: 1/2" GWB (UN-BLOCKED) w/ FASTENERS @ 7"/7"
FLOOR SHEATHING: 19/32" MIN. OSB (UN-BLOCKED) w/ 10d NAILING @ 6"/12"

PREPARED BY: BARLOW ENGINEERING. P.C. 6512 SIX FORKS RD, SUITE 203B RALEIGH, NC 27615



FOR ROOF ZONE 1: USE 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 12 in o.c. SHEATHING SUCTION FASTENING:

FOR ROOF ZONE 2: USE 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 12 in o.c. FOR ROOF ZONE 3 (CORNER): USE 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 12 in o.c.

FOR ROOF ZONE 30H (CORNER OVERHANG): USE 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 10 in o.c.

FOR WALL ZONE 4: USE 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 12 in o.c. FOR WALL ZONE 5: USE 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 12 in o.c.

EDGE DIMENSION, a =

#### CONNECTION SUMMARY: CONNECTIONS TO BE AS SPECIFIED OR EQUIVALENT

#### UPLIFT CONNECTIONS

REQUIRED TRUSS TIE DOWN: USE (4) 0.131" x 2.5" COMMON NAIL (ENDNAILED) CEILING BAND TO TRUSS

AND USE (1) SIMPSON H2.5A EACH TRUSS
OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 431 lbs

2nd FLOOR STUD TO TOP PLATE / CEILING BAND: USE A 1.5" x 26 ga. STRAP EACH STUD WITH (6) 8d NAIL(S) EACH END OR WITH (9) 16 ga. STAPLE(S) EACH END

OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 430 lbs

2nd FLOOR STUD TO FLOOR BAND: USE A 1.5" x 26 ga. STRAP EACH STUD WITH (6) 8d NAIL(S) EACH END OR WITH (9) 16 ga. STAPLE(S) EACH END

OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 354 lbs

2nd FLOOR BAND TO 1st CEILING BAND: USE A 1.5" x 26 ga. STRAP EACH STUD WITH (6) 8d NAIL(S) EACH END

OR WITH (9) 16 ga, STAPLE(S) EACH END

OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 354 lbs

1st FLOOR STUD TO CEILING BAND: USE A 1.5" x 26 ga. STRAP EACH STUD WITH (6) 8d NAIL(S) EACH END

OR WITH (9) 16 ga. STAPLE(S) EACH END
OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 299 lbs

1st FLOOR STUD TO FLOOR BAND: USE A 1.5" x 26 ga. STRAP EACH STUD WITH (6) 8d NAIL(S) EACH END

OR WITH (9) 16 ga. STAPLE(S) EACH END
OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 223 lbs

FLOOR BAND TO SILL PLATE CONNECTION: USE (2) SIMPSON RSP4(1) PLATE AT EACH ANCHOR BOLT LOCATION

TO CONNECT FLOOR BAND TO SILL PLATE

OR CONNECTION TO WITHSTAND AN UPLIET FORCE OF 557 lbs

#### LATERAL CONNECTIONS

TRUSS TO TOP PLATE CONNECTION: USE (1) 0.131" x 2.5" COMMON NAIL (TOENAILED) PER TRUSS

PLATE TO PLATE CONNECTION: ATTACH WITH 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 14" ON CENTER

PLATE TO STUD CONNECTION: USE (2) 0.162" x 3.5" COMMON NAIL (ENDNAILED) PER STUD

BOTTOM PLATE TO FLOOR CONNECTION: ATTACH WITH 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 14" ON CENTER

#### TOP PLATE SPLICES

TOP PLATE SPLICES SHALL BE A MINIMUM OF 2 ft w/ (2) ROWS 16d (0.162" x 3.5" COMMON NAIL (FACE NAILED)) 3" o.c OR A MINIMUM OF 5 ft w/ (2) ROWS 16d (0.162" x 3.5" COMMON NAIL (FACE NAILED)) 12" o.c

#### HORIZONTAL FLOOR DIAPHRAGM CONTINUITY

#### SECOND FLOOR

MODULE TO MODULE CONNECTION AT FLOOR RIMBAND: (ALONG MATE LINE) USE A MIN. OF (5) 1/2" DIA.THRU BOLTS OR USE A MIN. OF (14) 3/8" DIA. X 12" LAG TOE SCREWS (SPACED A MAX. OF 28" o.c.)

MODULE TO MODULE CONNECTION AT FLOOR RIMBAND: (AT ENDWALLS) USE A 1.5" x 22 ga. STRAP WITH (5) 8d NAIL(S) EACH END OR WITH (13) 16 ga. STAPLE(S) EACH END TO ATTACH MODULE TO MODULE AT EACH ENDWALL

OR CONNECTION TO WITHSTAND A TENSILE FORCE OF 602 lbs

MODULE TO MODULE CONNECTION AT FLOOR RIMBAND: (ALONG MATE LINE) USE A MIN. OF (6) 1/2" DIA.THRU BOLTS OR USE A MIN. OF (17) 3/8" DIA. X 12" LAG TOE SCREWS (SPACED A MAX. OF 27" o.c.)

MODULE TO MODULE CONNECTION AT FLOOR RIMBAND: (AT ENDWALLS) USE A 1.5" x 26 ga. STRAP WITH (5) 8d NAIL(S) EACH END OR WITH (8) 16 ga. STAPLE(S) EACH END TO ATTACH MODULE TO MODULE AT EACH ENDWALL OR CONNECTION TO WITHSTAND A TENSILE FORCE OF 382 lbs



#### SHEAR CONNECTIONS

#### SECOND FLOOR ENDWALL

UNIT SHEAR SHEATHING TO FLOOR BAND: USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 2" O.C. (AND SHEATHING TO TRUSS BOTTOM CHORD) OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 560 plf

UNIT UPLIFT SHEATHING TO FLOOR BAND: USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 2" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 560 plf ALTERNATE: FASTEN SHEATHING TO BAND WITH 1" WIDE STRIP OF 200 psi MINIMUM CONSTRUCTION ADHESIVE

TRUSS BOTTOM CHORD TO TOP PLATE CONNECTION: USE 0.162" x 3.5" COMMON NAIL (TOENAILED) @ 16" ON CENTER

OR USE (1) SIMPSON LTP4 PLATE @ 63" ON CENTER OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 2987 lbs

BANDS TO BANDS & BOTTOM / TOP PLATE CONNECTION: USE 0.162" x 3.5" COMMON NAIL (TOENAILED) AT 7" ON CENTER OR USE (1) SIMPSON LTP4 PLATE @ 28" ON CENTER OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 6749 lbs

#### SECOND FLOOR SIDEWALL

UNIT SHEAR SHEATHING TO FLOOR BAND: USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 3" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 335 plf

UNIT UPLIFT SHEATHING TO FLOOR BAND: USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 3" O.C.

OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 335 plf

ALTERNATE: FASTEN SHEATHING TO BAND WITH 1" WIDE STRIP OF 200 psi MINIMUM CONSTRUCTION ADHESIVE

BANDS TO BANDS & BOTTOM / TOP PLATE CONNECTION: USE 0.162" x 3.5" COMMON NAIL (TOENAILED) @ 5" ON CENTER OR USE (1) SIMPSON LTP4 PLATE @ 20" ON CENTER OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 5377 lbs

#### FIRST FLOOR ENDWALL

UNIT SHEAR SHEATHING TO FLOOR BAND: USE SHEATHING CONNECTION WITH 3 ROW(S) OF 8d NAILS AT 2" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 1306 plf

UNIT UPLIFT SHEATHING TO FLOOR BAND: USE SHEATHING CONNECTION WITH 3 ROW(S) OF 8d NAILS AT 2" O.C.

OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 1306 plf ALTERNATE: FASTEN SHEATHING TO BAND WITH 1" WIDE STRIP OF 200 psi MINIMUM CONSTRUCTION ADHESIVE

RIMBAND TO SILL PLATE CONNECTION: USE 0.162" x 3.5" COMMON NAIL (TOENAILED) @ 2" ON CENTER

OR USE (1) SIMPSON LTP4 PLATE @ 8" ON CENTER OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 10768 lbs

SILL PLATE TO FOUNDATION CONNECTION: USE 1/2" ANCHOR BOLTS @ 14" O.C

OR USE 5/8" ANCHOR BOLTS @ 20" O.C

OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 10768 lbs (784 plf)

#### FIRST FLOOR SIDEWALL

UNIT SHEAR SHEATHING TO FLOOR BAND: USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 2" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 404 plf

UNIT UPLIFT SHEATHING TO FLOOR BAND: USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 2" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 404 plf

ALTERNATE: FASTEN SHEATHING TO BAND WITH 1" WIDE STRIP OF 200 psi MINIMUM CONSTRUCTION ADHESIVE

RIMBAND TO SILL PLATE CONNECTION: USE 0.162" x 3.5" COMMON NAIL (TOENAILED) @ 8" ON CENTER OR USE (1) SIMPSON LTP4 PLATE @ 30" ON CENTER OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 7543 lbs

SILL PLATE TO FOUNDATION CONNECTION: USE 1/2" ANCHOR BOLTS @ 53" O.C

OR USE 5/8" ANCHOR BOLTS @ 72" O.C OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 7543 lbs (229 plf)

#### **DESIGN PARAMETERS**

MEAN ROOF HEIGHT (MRH) =	30.00 ft
NUMBER OF STORIES =	2
FIRST FLOOR WIDTH (W <sub>1</sub> ) =	27.5 ft
SECOND FLOOR WIDTH (W2) =	27.5 ft
FIRST FLOOR LENGTH $(L_1)$ =	39 ft
SECOND FLOOR LENGTH $(L_2)$ =	33 ft
BUILDING ASPECT RATIO (L/W) =	1.20
FLOOR JOIST DEPTH =	9.25 in
MAX. VERTICAL FLOOR OFFSET =	0 in
FLOOR ASPECT RATIO (L/W) =	1.20
MAX. FLOOR DIAPHRAGM OPENING WIDTH =	13.56 ft
MAX. FLOOR DIAPHRAGM OPENING LENGTH =	3.33 ft
FIRST FLOOR HEIGHT (H <sub>1</sub> ) =	8 ft
SECOND FLOOR HEIGHT (H <sub>2</sub> ) =	8 ft
CEILING ASPECT RATIO (L/W) =	1.20
MIN. SHEARWALL SEGMENT (H / 3.5) =	2.29 ft
ROOF PITCH =	5 /12



#### SEE ADDITIONAL CALCULATIONS

#### CONNECTION INFORMATION:

#### TRUSS TO PLATE CONNECTORS

	UPLIFT STRENGTH:		SHEAR STRENGTH:		
(1) SIMPSON H2.5A	U =	535 lbs	F <sub>2</sub> =	110 lbs	
(2) SIMPSON H2.5A	U =	1070 lbs	F <sub>2</sub> =	220 lbs	
(2) SIMPSON LS50	U =	0 lbs	F <sub>2</sub> =	1260 lbs	
	200 psi MINIMUM CON	ISTRUCTION ADHESIVE	Z =	100 psi (I	END-GRAIN)
	200 psi MINIMUM CON	STRUCTION ADHESIVE	Z =	200 psi (FACE)	
FLAT STRAPS			FASTENERS: 8d NAIL	16 ga. STAPLE	
1.5" x 26 ga. STRAP	Z =	485 lbs	Z =	76.7	49.9 lbs
1.5" x 22 ga. STRAP	Z =	810 lbs	Z =	127.2	48.6 lbs
1.5" x 20 ga. STRAP	Z =	973 lbs	Z =	127.3	48.3 lbs
(2) 1.5" x 22 ga. STRAP	Z =	1620 lbs	Z =	129.4	46.4 lbs
(2) 1.5 x 20 ga STRAP	Z =	1946 lbs	Z =	131.4	46 lbs
	HOLDDOWNS w/	1 1/2" EDGE DISTANCE			
	N	IINIMUM 8" STEM WALL			
	ASSUME	3000 psi Fc CONCRETE			
	SIN	MPSON HHDQ11-SDS2.5	Z =	8505 lbs	
	SIN	MPSON HHDQ14-SDS2.5	Z =	10745 lbs	
		SIMPSON STHD14RJ	Z =	4430 lbs	
	SIMPSON	HD12 W/(3) 2X6 STUDS	Z =	11055 lbs	
		1/2" DIA. THRU BOLT	Z =	623 lbs	
		1/2" ANCHOR BOLT	Z =	1056 lbs	
		5/8" ANCHOR BOLT	Z =	1488 lbs	
	3/8" DIA.	X 12" LAG TOE SCREW	Z =	208 lbs	
	0.131" x 2.5" COMM	ON NAIL (FACE NAILED)	Z =	100 lbs	
	0.131" x 2.5" COM	MON NAIL (TOENAILED)	Z =	83 lbs	
	0.131" x 2.5" COM	MON NAIL (ENDNAILED)	Z =	67 lbs	
	0.162" x 3.5" COM	MON NAIL (TOENAILED)	Z =	158 lbs	
	0.162" x 3.5" COMM	ON NAIL (FACE NAILED)	Z =	191 lbs	
	0.162" x 3.5" COM	MON NAIL (ENDNAILED)	Z =	128 lbs	
8d COM	MON NAIL (FACE NAILE	D), 7/16" SIDE MEMBER	Z =	95 lbs	
	0.131" x 2.5" COMM	ON NAIL (FACE NAILED)	Z =	69 lbs (7	7/16" SIDE; WITHDRAWAL)
	(1	) SIMPSON LTP4 PLATE	Z =	575 lbs	
	SI	MPSON RSP4(1) PLATE	Z =	285 lbs	
1/2	" GWB (UN-BLOCKED)	w/ FASTENERS @ 7"/7"	Z =	70 plf	
7/1	6" OSB (UN-BLOCKED)	) w/ 8d NAILING @ 6"/12"	Z =	296 plf	
	7/16" OSB (BLOCKED	) w/ 8d NAILING @ 6"/12"	Z =	328 plf	
19/32" MIN	I. OSB (UN-BLOCKED)	w/ 10d NAILING @ 6"/12"	Z =	368 plf	
19/32"	MIN. OSB (BLOCKED)	w/ 10d NAILING @ 6"/12"	Z =	412 plf	
7/16" OSB (BLOCKED)	w/ 8d NAILING @ 6"/12"	& 4" o.c. @ PERIMETER	Z =	437 plf	
19/32" OSB (BLOCKED) w	/ 10d NAILING @ 6"/12"	& 4" o.c. @ PERIMETER	Z =	548 plf	
19/32" OSB (BLOCKED) w/ 10d NA	NLING @ 4"/12" & 2 1/2" o.c. @ I	PERIMETER, DOUBLE FRAMING	Z =	824 plf	

NOTE: USP CONNECTORS & FASTEN VALUES ASSUME SPF FRAMING MATERIAL ANCHOR BOLT VALUES ASSUME DF/SP VALUES



#### **DESIGN UPLIFT LOADS**

#### UPLIFT CONNECTION LOAD:

PER ASCE 7-05: wup' = 385 plf wup = wup' - 0.6 \* RDL \* RS / 4 = wup = 385 plf - 0.6 \* 15 psf \* 27.5 ft / 4 =

323 pl

#### STANDARD TRUSS TO CEILING BAND CONNECTION:

(4) 0.131" x 2.5" COMMON NAIL (ENDNAILED) Z = 4 NAILS x 67 lbs / NAIL Z = 268 lbs

USE (4) 0.131" x 2.5" COMMON NAIL (ENDNAILED) CEILING BAND TO TRUSS

#### ADDITIONAL TIE(S) REQUIRED FOR TRUSS TIE DOWN:

 $P_{up}$  = wup \* TOC - 268 lbs  $P_{up}$  = 323 plf \* 16 in / 12 - 268 lbs =  $P_{up}$  = 163 lbs

# AND USE (1) SIMPSON H2.5A EACH TRUSS OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 431 lbs

#### REQUIRED SIDEWALL STUD TIE DOWN LOADING:

2nd FLOOR STUD TO TOP PLATE / CEILING BAND:  $P_{2tp} = w_{up} * SOC = 323 * 16 / 12 = 430 \; lbs$ 

2nd FLOOR STUD TO FLOOR BAND:  $P_{2tb} = P_{2tp} - 0.6 * WDL * H<sub>2</sub> * SOC =$ 

 $P_{2fb} = 430 \text{ lbs} - 0.6 * 12 \text{ psf} * 8 \text{ ft} * 16 \text{ in} / 12 = 354 \text{ lbs}$ 

2nd FLOOR BAND TO 1st CEILING BAND:  $P_{2f1c} = P_{2fb} = 354$  lbs

1st FLOOR STUD TO CEILING BAND:  $P_{1ab} = P_{2b} - 0.6 * FDL * W_2 / 4 * SOC = \\ P_{1ab} = 354 \; lbs - 0.6 * 10 \; psf * 27.5 \; ft / 4 * 16 \; in / 12 = \\ P_{1ab} = 100 \; rac{1}{100} \;$ 

P<sub>1cb</sub> = 299 lbs

1st FLOOR STUD TO FLOOR BAND:  $P_{1tb} = P_{1cb} - 0.6 \text{ *WDL * H}_1 \text{ * SOC = } \\ P_{1tb} = 299 \text{ lbs - } 0.6 \text{ * 12 psf * 8 ft * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 12 psf * 8 ft * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 12 psf * 8 ft * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 12 psf * 8 ft * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 12 psf * 8 ft * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 12 psf * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 10 psf * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 10 psf * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 10 psf * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 10 psf * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 10 psf * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 10 psf * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 10 psf * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 10 psf * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 10 psf * 16 in / 12 = } \\ 223 \text{ lbs - } 0.6 \text{ * 10 psf * 10$ 

F<sub>1fb</sub> = 299 lbs - 0.0 12 psi | 0 it | 10 iii / 12 = 223 lb

CHECK FASTENERS: 8d NAIL Z = 76.7 lbs

430 lbs / 76.7 lbs / FASTENER = 5.61 FASTENERS
USE (6) 8d NAIL(S) EACH END

16 ga. STAPLE Z = 49.9 lbs

USE A 1.5" x 26 ga. STRAP EACH STUD WITH (6) 8d NAIL(S) EACH END OR WITH (9) 16 ga. STAPLE(S) EACH END OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 430 lbs



#### SIDEWALL 1st FLOOR BAND TO SILL PLATE CONNECTION:

SIDEWALL UPLIFT AT SILL PLATE:  $W_{sp} = P_{1fb} / SOC - 0.6 * FDL * W_1 / 4 =$ 

w<sub>sp</sub> = 223 lbs \* 12 / 16 in - 0.6 \* 10 psf \* 27.5 ft / 4 =

w<sub>sp</sub> = 126 plf

#### CHECK STRAP AT ANCHOR BOLT LOCATIONS:

1/2" ANCHOR BOLT SPACING (BOC) = 53 in

 $P_{sp} = W_{sp} * BOC = 126 plf * 53 = 557 lbs$ 

SIMPSON RSP4(1) PLATE Z = 285 lbs

557 lbs = 2 PLATES

# USE (2) SIMPSON RSP4(1) PLATE AT EACH ANCHOR BOLT LOCATION TO CONNECT FLOOR BAND TO SILL PLATE OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 557 lbs

#### CHECK BENDING IN RIMBAND:

DBL. 2x10 SPF #2 RIMBAND DESIGN VALUES:

SECTION MODULUS (S) =  $42.78 \text{ in}^3$ ALLOWABLE BENDING (fb) = 875 psi

 $M_{MAX} = \underline{w_{sp} * BOC}^2 =$ 

 $M_{MAX} = 126 \text{ plf} * (53 / 12)^2 = 3687 \text{ in-lbs}$ 

APPLIED fb =  $\frac{M_{MAX}}{S} = \frac{3687 \text{ in-lbs}}{42.78 \text{ in}^3}$  86 ps

ALLOWABLE BENDING (fb) = 875 psi > APPLIED fb = 86 psi

DBL. 2x10 SPF #2 RIMBAND IS OK



# LATERAL LOAD AT ROOF/CEILING DIAPHRAGM ROOF SPAN = 27.5 ft ROOF PITCH = 5 /12 WIND PERPENDICULAR TO RIDGE: WIND PARALLEL TO RIDGE: LATERAL LOAD AT FLOOR DIAPHRAGM WIND PERPENDICULAR TO RIDGE: 228 off WIND PARALLEL TO RIDGE:

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#### LATERAL FRAMING CONNECTION LOADS FROM WIND:

(FOR ROOF-TO-PLATE, PLATE-TO-PLATE, PLATE-TO-STUD, AND PLATE-TO-FLOOR)

PER ASCE 7-10 WIND PRESSURE (w) =

wl-wall' = w \* H / 2 =

TRUSS MULTIPLIER = 1.33

STUD MULTIPLIER = 1.33

#### TRUSS TO TOP PLATE CONNECTION:

P<sub>C</sub> = w<sub>I-wall</sub> \* M<sub>24</sub> = 84 plf \* 1.33 =

TRUSS CONNECTION: (1) SIMPSON H2.5A

112 lbs

P<sub>C</sub> = P - F<sub>2</sub> = P<sub>C</sub> = 112 lbs - 110 lbs =

# OF 0.131" x 2.5" COMMON NAIL (TOENAILED) REQUIRED =

1 NAILS

#### USE (1) 0.131" x 2.5" COMMON NAIL (TOENAILED) PER TRUSS

#### PLATE TO PLATE CONNECTION:

SPACING OF 0.131" x 2.5" COMMON NAIL (FACE NAILED) =

<u>Z \* 12</u> = 100 lbs \* 12 = 84 plf

14 in O.C. (16" max)

#### ATTACH WITH 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 14" ON CENTER

#### PLATE TO STUD CONNECTION:

P<sub>C</sub> = w<sub>i-wall</sub> \* M<sub>16</sub> = 84 plf \* 1.33 =

# OF 0.162" x 3.5" COMMON NAIL (ENDNAILED) REQUIRED =

Pc = 112 lbs =

2 NAILS

#### USE (2) 0.162" x 3.5" COMMON NAIL (ENDNAILED) PER STUD

#### BOTTOM PLATE TO FLOOR CONNECTION:

SPACING OF 0.131" x 2.5" COMMON NAIL (FACE NAILED) =  $\underline{Z * 12}$  =  $\underline{100 \text{ lbs * } 12 \text{ = }}$ 

W<sub>I-wall</sub> 84 plf 14 in O.C. (16" max)

#### ATTACH WITH 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 14" ON CENTER

#### TOP PLATE SPLICE LENGTH

DIAPHRAGM CHORD FORCE =

STRUCTURE WIDTH (W) =

27.5 ft 39 ft

STRUCTURE LENGTH (L) = 0.162" x 3.5" COMMON NAIL (FACE NAILED) Z =

191 lbs

ROOF DIAPHRAGM LOADING (wi-per) =

181 plf

FLOOR DIAPHRAGM LOADING (FLI-per) = 228 plf

#### FLOOR DIAPHRAGM LOADING CONTROLS

CONTROLLING LOADING: 228 plf

 $T = \underline{\text{wl-per} * L^2} =$ 

228 plf \* 39 ft ^ 2 = 8 \* 27.5 ft

5 ft

REQUIRED SPLICE LENGTH (w/ (2) 16d 3" o.c.): T \* 3" / 12" / ft =

1577 lbs \* 3" / 12" / ft = 2 \* 191 lbs / NAIL

REQUIRED SPLICE LENGTH (w/ (2) 16d 12" o.c.):  $\underline{T * 12" / 12" / ft} =$ 

1577 lbs \* 12" / 12" / ft = 2 \* 191 lbs / NAIL

TOP PLATE SPLICES SHALL BE A MINIMUM OF 2 ft w/ (2) ROWS 16d (0.162" x 3.5" COMMON NAIL (FACE NAILED)) 3" o.c OR A MINIMUM OF 5 ft w/ (2) ROWS 16d (0.162" x 3.5" COMMON NAIL (FACE NAILED)) 12" o.c

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#### ROOF DIAPHRAGM SHEATHING REQUIREMENTS

 $\begin{aligned} & \text{ROOF SPAN (RS) =} & 27.5 \text{ ft} \\ & \text{ROOF LENGTH (RL) =} & 33 \text{ ft} \\ & \text{ROOF PITCH =} & 5 \ /12 \\ & \text{ROOF ANGLE (RA) =} & 22.6 \ ^{\circ} \\ & w_{\text{l-per}} = & 181 \text{ plf} \end{aligned}$ 

STANDARD ROOF SHEATHING = 7/16" OSB (UN-BLOCKED) w/ 8d NAILING @ 6"/12"

ROOF SHEATHING SHEAR CAPACITY (v,') = 296 plf

STANDARD CEILING SHEATHING = 1/2" GWB (UN-BLOCKED) w/ FASTENERS @ 7"/7"

CEILING SHEATHING SHEAR CAPACITY ( $v_c$ ) = 70 plf

MAX DIAPHRAGM SHEAR (v) =  $\frac{L * wl_{opt} / 2 =}{RS}$  =  $\frac{33 \text{ ft} * 181 \text{ plf} / 2 =}{27.5 \text{ ft}}$  = 109 plf

NET DIAPHRAGM SHEAR CAPACITY ( $v_n$ ) =  $v_r$  +  $v_c$  = 296 plf + 70 plf = 366 plf

DIAPHRAGM SHEAR CAPACITY
REQUIRED = 109 plf

STANDARD ROOF/CEILING DIAPHRAGM
CAPACITY = 366 plf

STANDARD ROOF/CEILING DIAPHRAGM OK

#### FLOOR DIAPHRAGM SHEATHING REQUIREMENTS

BUILDING WIDTH (W) = 27.5 ft
BUILDING LENGTH (L) = 33 ft

 $FL_{lpgr} = 228 \ plf$   $STANDARD \ FLOOR \ SHEATHING = 19/32" \ MIN. \ OSB \ (UN-BLOCKED) \ w/\ 10d \ NAILING \ @ 6"/12"$ 

FLOOR DIAPHRAGM SHEAR CAPACITY (v<sub>f</sub>) = 368 plf

MAX FLOOR DIAPHRAGM SHEAR (v) =  $\frac{L * FLL_{per} / 2 =}{W}$   $\frac{33 \text{ ft * 228 pif } / 2 =}{27.5 \text{ ft}}$  137 plf

DIAPHRAGM SHEAR CAPACITY REQUIRED = 137 plf STANDARD ROOF/CEILING DIAPHRAGM CAPACITY = 368 plf

STANDARD FLOOR DIAPHRAGM OK



#### SHEATHING SUCTION CONNECTION (PER ASCE 7-05 C-C PRESSURES, pp. 355-358) TRUSS SPACING (TOC) = 16 in O.C. STUD SPACING (SOC) = 16 in O.C. 0.131" x 2.5" COMMON NAIL (FACE NAILED) 69 lbs (7/16" SIDE MEMBER; WITHDRAWAL) a = 3 ft FOR ROOF ZONE 1 (FIELD): 16.728 psf TRUSS LOADING = 16.728 psf x 16" o.c. / 12" / ft = 0.4 FASTENERS / ft = 22 plf 30 in O.C. MAX ALLOWABLE SPACING: 69 lbs / FASTENER 12 in O.C. USE 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 12 in o.c. FOR ROOF ZONE 2 (EDGE): 29.118 psf TRUSS LOADING = 29.118 psf x 16" o.c. / 12" / ft = 39 plf 0.6 FASTENERS / ft = 39 plf 20 in O.C. 69 lbs / FASTENER MAX ALLOWABLE SPACING: 12 in O.C. USE 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 12 in o.c. FOR ROOF ZONE 3 (CORNER): 43.056 psf TRUSS LOADING = 43.056 psf x 16" o.c. / 12" / ft = 57 plf 0.9 FASTENERS / ft = 57 plf 13 in O.C. 69 lbs / FASTENER MAX ALLOWABLE SPACING: 12 in O.C.

USE 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 12 in o.c.



FOR ROOF ZONE 30H (CORNI	ER OVERHANG):				
		p =	60.09 psf		
	TRUSS L	OADING = 60.09 ps	sf x 16" o.c. / 12" / ft =	80 plf	
	80 plf 69 lbs / FASTENER	=	1.2 FASTENERS / ft = MAX ALLOWABLE	E SPACING:	10 in O.C. 12 in O.C.
		USE 0.131" x 2	:.5" COMMON NAIL (FACE NAIL	ED) AT 10 in o.c.	
FOR WALL ZONE 4 (FIELD):					
		p =	19.824 psf		
	STUD L	OADING = 19.824	psf x 16" o.c. / 12" / ft =	26 plf	
	26 plf	=	0.4 FASTENERS / ft =		30 in O.C.
	69 lbs / FASTENER		MAX ALLOWABLE	E SPACING:	12 in O.C.
		USE 0.131" x 2	.5" COMMON NAIL (FACE NAIL	ED) AT 12 in o.c.	
FOR WALL ZONE 5 (EDGE):					
		p =	24.468 psf		
	STUD L	OADING = 24.468	psf x 16" o.c. / 12" / ft =	33 plf	
	33 plf	=	0.5 FASTENERS / ft =		24 in O.C.
	69 lbs / FASTENER		MAX ALLOWABLE	- SPACING:	12 in O.C.

USE 0.131" x 2.5" COMMON NAIL (FACE NAILED) AT 12 in o.c.

PREPARED BY: BARLOW ENGINEERING. P.C. 6512 SIX FORKS RD, SUITE 203B RALEIGH, NC 27615

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7/20/17

### SECOND FLOOR ENDWALL #1 SHEATHING LENGTH REQUIREMENTS

FIRST FLOOR LENGTH (W<sub>1</sub>) = SECOND FLOOR LENGTH (W2) = FIRST FLOOR LENGTH (L1) = 39 ft SECOND FLOOR LENGTH (L2) = 33 ft

SHEARWALL TYPE: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR SHEATHING EDGE 8d NAIL SPACING = 6 in O.C. (8d NAILS OR EQUIVALENT)

SHEARWALL STRENGTH (V) = 436 plf MIN. SHEARWALL SEGMENT LENGTH = 2.3 ft FULL HEIGHT SHEATHING PROVIDED ( $\Sigma L_i$ ) = 7.83 ft 2nd FL. PERCENT FULL HEIGHT SHEATHING= 100 % 2nd FL. MAX. UNRESTRAINED OPENING HEIGHT =

SHEAR ADJUSTMENT FACTOR (Co) = 1 (TABLE 2305.3.7.2, IBC)

2nd FL. NUMBER OF SHEARWALLS (N<sub>end</sub>) = 2 ADDITIONAL WALL LOAD =

SHEARWALL REACTION (R<sub>end2</sub>) =  $L_2 * w_{l-per} / N_{end} + ADDITIONAL=$ 

R<sub>end2</sub> = 33 ft \* 181 plf / 2 + 0 lbs =

MIN. LENGTH SEGMENTED SHEARWALLS ( $L_{sw}$ ) =  $R_{end2}/V$  = 2987 lbs / 436 plf = 6.85 ft

PERFORATED FULL HEIGHT SHEATHING LENGTH REQUIRED (ENDWALL) =  $L_{sw}/C_0$  = 6.85 ft / 1 = 6.86 ft

> PERFORATED FULL HEIGHT SHEATHING PERFORATED FULL HEIGHT SHEATHING

REQUIRED = 6.86 ft PROVIDED = 7.83 ft

ENDWALL SHEARWALLS OK ALL EXTERIOR SHEATHING TO BE BLOCKED UNO

#### SECOND FLOOR HORIZONTAL FLOOR DIAPHRAGM CONTINUITY:

#### MODULE TO MODULE CONNECTION AT FLOOR RIMBAND: (ALONG MATE LINE)

(DEEP BEAM HORIZONTAL SHEAR)

2987 lbs

3/4 \* 228 plf \* 33 ft = 2822 lbs V<sub>f</sub> = (3 \* F<sub>i-per</sub> / 4) \* L =

# 1/2" DIA. THRU BOLT =  $\underline{V_f}$  = 2822 lbs = 5 BOLTS  $Z_{1/2\;BOLT}$ 623 lbs

# 3/8" DIA. X 12" LAG TOF SCREW = <u>V<sub>f</sub></u> = 2822 lbs = 14 SCREWS Z<sub>3/8 LAG</sub> 208 lbs

> SPACING = L2 / # = 33 ft / 14 SCRE 28 in

#### USE A MIN. OF (5) 1/2" DIA.THRU BOLTS

OR USE A MIN. OF (14) 3/8" DIA. X 12" LAG TOE SCREWS (SPACED A MAX. OF 28" o.c.) TO ATTACH MODULE TO MODULE ALONG MATE LINE

#### MODULE TO MODULE CONNECTION AT FLOOR RIMBAND: (AT ENDWALLS)

(CHORD FORCE CONTINUITY)

 $T = \frac{F_{l-para} * W_2^2}{} =$ 210 plf \* 27.5 ft ^ 2 = 602 lbs 8 \* L<sub>2</sub> 8 \* 33 ft

Z = CHECK FASTENERS: 8d NAIL 127.2 lbs

602 lbs / 127.2 lbs / FASTENER =

USE (5) 8d NAIL(S) EACH END

16 ga. STAPLE 7 = 48.6 lbs

> 602 lbs / 48.6 lbs / FASTENER = 12.39 FASTENERS USE (13) 16 ga. STAPLE(S) EACH END

USE A 1.5" x 22 ga. STRAP WITH (5) 8d NAIL(S) EACH END OR WITH (13) 16 ga. STAPLE(S) EACH END TO ATTACH MODULE TO MODULE AT EACH ENDWALL OR CONNECTION TO WITHSTAND A TENSILE FORCE OF 602 lbs

#### SECOND FLOOR ENDWALL #1: UPLIFT DUE TO OVERTURNING

FULL HEIGHT SHEATHING PROVIDED (ΣL) = SHEARWALL ADJUSTMENT FACTOR ( $C_0$ ) = 1 SHEARWALL REACTION (Rend2) = 2987 lbs WALL HEIGHT (H) = 8 ft

> UPLIFT FORCE (U<sub>E2</sub>) = R<sub>end1</sub> x H =

> > 3052 lbs U<sub>E2</sub> = 2987 lbs x 8 ft

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#### SECOND FLOOR ENDWALL #2 SHEATHING LENGTH REQUIREMENTS BEDROOMS #2 & #3

FIRST FLOOR WIDTH (W1) = 27.5 ft SECOND FLOOR WIDTH  $(W_2)$  = 27.5 ft FIRST FLOOR LENGTH  $(L_1)$  = 39 ft SECOND FLOOR LENGTH (L2) = 33 ft

SHEARWALL TYPE: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR

SHEATHING EDGE 8d NAIL SPACING = 4 in O.C. (8d NAILS OR EQUIVALENT)

SHEARWALL STRENGTH (V) = 590 plf MIN. SHEARWALL SEGMENT LENGTH = 2.3 ft FULL HEIGHT SHEATHING PROVIDED ( $\Sigma L_i$ ) = 11.58 ft 2nd FL. PERCENT FULL HEIGHT SHEATHING= 42 % 2nd FL. MAX. UNRESTRAINED OPENING HEIGHT =

SHEAR ADJUSTMENT FACTOR ( $C_o$ ) = 0.461 (TABLE 2305.3.7.2, IBC) 2

2nd FL. NUMBER OF SHEARWALLS (Nend) = ADDITIONAL WALL LOAD = 0 lbs

SHEARWALL REACTION (R<sub>end2</sub>) =  $L_2$  \*  $w_{i-per}$  /  $N_{end}$  + ADDITIONAL=  $R_{end2}$  = 33 ft \* 181 plf / 2 + 0 lbs =

2987 lbs

MIN. LENGTH SEGMENTED SHEARWALLS ( $L_{sw}$ ) =  $R_{end2}/V$  = 2987 lbs / 590 lbs = 5.06 ft

PERFORATED FULL HEIGHT SHEATHING LENGTH REQUIRED (ENDWALL) = L<sub>SW</sub> / C<sub>O</sub> = 5.06 ft / 0.461 = 10.99 ft

> PERFORATED FULL HEIGHT SHEATHING REQUIRED = 10.99 ft

PERFORATED FULL HEIGHT SHEATHING PROVIDED = 11.58 ft

ENDWALL SHEARWALLS OK ALL EXTERIOR SHEATHING TO BE BLOCKED UNO

#### SECOND FLOOR ENDWALL #2: UPLIFT DUE TO OVERTURNING

FULL HEIGHT SHEATHING PROVIDED ( $\Sigma L_i$ ) = SHEARWALL ADJUSTMENT FACTOR (Co) = SHEARWALL REACTION  $(R_{end2})$  = 2987 lbs WALL HEIGHT (H) = 8 ft

> UPLIFT FORCE (U<sub>E2</sub>) = R<sub>end1</sub> x H =  $\Sigma L_i \times C_o$

> > U<sub>E2</sub> = 2987 lbs x 8 ft 4477 lbs 11.58 ft x 0.461



#### SECOND FLOOR ENDWALL: SHEAR CONNECTIONS

	27.5 ft	SECOND FLOOR WIDTH (W2) =
	33 ft	SECOND FLOOR LENGTH $(L_2)$ =
	228 plf	FL <sub>I-per</sub> =
1056 lbs	Z =	1/2" ANCHOR BOLT
1488 lbs	Z =	5/8" ANCHOR BOLT
158 lbs	Z =	0.162" x 3.5" COMMON NAIL (TOENAILED)
191 lbs	Z =	0.162" x 3.5" COMMON NAIL (FACE NAILED)
575 lbs	Z =	(1) SIMPSON LTP4 PLATE

MAXIMUM SECOND FLOOR ENDWALL SHEAR LOAD = 2987 lbs

#### TRUSS BOTTOM CHORD TO TOP PLATE CONNECTION:

# TOENAILS PER FOOT = V / Z / W = 2987 lbs / 158 lbs / 27.5 ft = 0.7 NAILS / ft TOENAIL SPACING = 12 / # = 12 / 0.7 = 16 " O.C. (16" MAX) # MP4F PLATES PER FOOT = V / Z / W = 2987 lbs / 575 lbs / 27.5 ft = 0.2 PLATES / ft

(72" MAX) MP4F PLATE SPACING = 12 / # = 12 / 0.2 = 63 " O.C.

USE 0.162" x 3.5" COMMON NAIL (TOENAILED) @ 16" ON CENTER OR USE (1) SIMPSON LTP4 PLATE @ 63" ON CENTER OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 2987 lbs

#### BANDS TO BANDS & BOTTOM / TOP PLATE CONNECTION:

V = MAX ENDWALL SHEAR +  $L_2$  x FL<sub>I-per</sub> / 2 = V = 2987 lbs + 33 ft x 228 plf / 2 6749 lbs

# TOENAILS PER FOOT = V / Z / W = 6749 lbs / 158 lbs / 27.5 ft = 1.6 NAILS / ft

(16" MAX) TOENAIL SPACING = 12 / # = 12 / 1.6 = 7 " O.C.

# MP4F PLATES PER FOOT = V / Z / W = 6749 lbs / 575 lbs / 27.5 ft = 0.4 PLATES / ft

MP4F PLATE SPACING = 12 / # = 12 / 0.4 = 28 " O.C. (72" MAX)

USE 0.162" x 3.5" COMMON NAIL (TOENAILED) AT 7" ON CENTER OR USE (1) SIMPSON LTP4 PLATE @ 28" ON CENTER OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 6749 lbs



#### CHECK SHEATHING TO RIMBAND CONNECTION:

#### UNIT SHEAR CHECK:

SHEAR FORCE (V) = 
$$\frac{R_{end2}}{\sum L_i X C_O}$$
 =

SECOND FLOOR ENDWALL #1: V = \_\_\_\_2987 lbs \_\_\_ = 382 plf

SECOND FLOOR ENDWALL #2: V = 2987 lbs = 560 plf 11.58 ft \* 0.461

MAXIMUM SECOND FLOOR ENDWALL UNIT SHEAR = 560 plf

CHECK # 8d NAILS REQUIRED FOR SHEATHING CONNECTION:

8d COMMON NAIL (FACE NAILED), 7/16" SIDE MEMBER Z = 95 lbs

# OF 8d NAILS PER FOOT = V = 560 plf
Z 95 lbs / NAIL

# OF 8d NAILS PER FOOT = 5.9 NAILS PER FOOT

OVERALL 8d NAIL SPACING = 12 / # = 12 / 5.9 = 2.03 " O.C.

# OF ROWS : 1 ROW(S)

8d NAIL SPACING WITHIN EACH ROW = 1 \* SPACING 1 \* 2.03 o.c. 2 " O.C.

# USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 2" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 560 plf

#### UNIT UPLIFT CHECK: (EQUAL TO UNIT SHEAR)

CHECK # 8d NAILS REQUIRED FOR SHEATHING CONNECTION:

8d COMMON NAIL (FACE NAILED), 7/16" SIDE MEMBER Z = 95 lbs

# OF 8d NAILS PER FOOT = V = 560 plf
Z 95 lbs / NAIL

# OF 8d NAILS PER FOOT = 5.9 NAILS PER FOOT

OVERALL 8d NAIL SPACING = 12 / # = 12 / 5.9 = 2.03 "O.C.

# OF ROWS : 1 ROW(S)

8d NAIL SPACING WITHIN EACH ROW = 1 \* SPACING 1 \* 2.03 o.c. 2 " O.C.

# USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 2" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 560 plf

#### ALTERNATE SHEATHING CONNECTION FOR UNIT UPLIFT (GLUE):

V = 560 plf

200 psi MINIMUM CONSTRUCTION ADHESIVE Z = 200 psi (FACE)

WIDTH OF GLUE REQUIRED FOR SHEATHING CONNECTION ALONG FLOOR BAND:

WIDTH OF GLUE STRIP REQUIRED = V = 560 plf = 1 
Z 200 psi \* 12" / ft

FASTEN SHEATHING TO BAND WITH 1" WIDE STRIP OF 200 psi MINIMUM CONSTRUCTION ADHESIVE PLUS (1) ROW OF 8d NAILS AT 6" o.c.

#### FIRST FLOOR ENDWALL #1 SHEATHING LENGTH REQUIREMENTS

FAMILY / DINING

FIRST FLOOR WIDTH (W<sub>1</sub>) = SECOND FLOOR WIDTH (W2) = 27.5 ft FIRST FLOOR LENGTH (L1) = 39 ft SECOND FLOOR LENGTH (L2) = 33 ft

SHEARWALL TYPE: 7/16" OSB EXTERIOR (BLOCKED) w/ 7/16" OSB INTERIOR (BLOCKED)

SHEATHING EDGE 8d NAIL SPACING = 2 in O.C. (8d NAILS OR EQUIVALENT)

SHEARWALL STRENGTH (V) = 1648 plf MIN. SHEARWALL SEGMENT LENGTH = 2.3 ft SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma$  L<sub>i</sub>) = 5.17 ft 1st FL. PERCENT FULL HEIGHT SHEATHING= 1st FL. MAX. UNRESTRAINED OPENING HEIGHT = 0 ft

SHEAR ADJUSTMENT FACTOR (Co) = 1 (TABLE 2305.3.7.2, IBC)

TRIBUTARY LENGTH (TL) = 16.5 ft ADDITIONAL WALL LOAD = 0 lbs

SHEARWALL REACTION (R $_{\rm end1}$ ) = TL \* FL $_{\rm l-per}$  + R $_{\rm end2}$  + ADDITIONAL=

Rend1 = 16.5 ft \* 228 plf + 2987 lbs + 0 lbs = 6749 lbs

MIN. LENGTH SEGMENTED SHEARWALLS (Lsw) = Rend1 / V = 6749 lbs / 1648 plf = 4.10 ft

PERFORATED FULL HEIGHT SHEATHING LENGTH REQUIRED (ENDWALL) = L<sub>SW</sub> / C<sub>O</sub> = 4.1 ft / 1 = 4.10 ft

PERFORATED FULL HEIGHT SHEATHING

PERFORATED FULL HEIGHT SHEATHING

REQUIRED = 4.1 ft PROVIDED = 5.17 ft

**ENDWALL SHEARWALLS OK** ALL EXTERIOR SHEATHING TO BE BLOCKED UNO

#### FIRST FLOOR HORIZONTAL FLOOR DIAPHRAGM CONTINUITY:

#### MODULE TO MODULE CONNECTION AT FLOOR RIMBAND: (ALONG MATE LINE)

(DEEP BEAM HORIZONTAL SHEAR)

 $V_f = (3 * F_{i-per} / 4) * L =$ 3335 lbs 3 / 4 \* 228 plf \* 39 ft = # 1/2" DIA. THRU BOLT =  $\frac{V_t}{}$  =  $\frac{3335 \text{ lbs}}{}$  = 6 BOLTS  $Z_{1/2\;BOLT}$ 623 lbs # 3/8" DIA. X 12" LAG TOF SCREW = <u>V<sub>f</sub></u> = <u>3335 lbs =</u> 17 SCREWS

 $Z_{3/8 \, LAG}$ 208 lbs SPACING = L2 / # = 39 ft / 17 SCRE

USE A MIN. OF (6) 1/2" DIA.THRU BOLTS

OR USE A MIN. OF (17) 3/8" DIA. X 12" LAG TOE SCREWS (SPACED A MAX. OF 27" o.c.) TO ATTACH MODULE TO MODULE ALONG MATE LINE

MODULE TO MODULE CONNECTION AT FLOOR RIMBAND: (AT ENDWALLS)

(CHORD FORCE CONTINUITY)

 $T = 3/4 * F_{1-para} * W_1^2 =$ 3/4 \* 210 plf \* 27.5 ft ^ 2 = 8 \* 39 ft 8 \* L<sub>1</sub>

CHECK FASTENERS: 8d NAIL Z = 76.7 lbs

382 lbs / 76.7 lbs / FASTENER = 4.98 FASTENERS USE (5) 8d NAIL(S) EACH END

16 ga. STAPLE 7 = 49.9 lbs

7.66 FASTENERS 382 lbs / 49.9 lbs / FASTENER = USE (8) 16 ga. STAPLE(S) EACH END

USE A 1.5" x 26 ga. STRAP WITH (5) 8d NAIL(S) EACH END OR WITH (8) 16 ga. STAPLE(S) EACH END TO ATTACH MODULE TO MODULE AT EACH ENDWALL OR CONNECTION TO WITHSTAND A TENSILE FORCE OF 382 lbs

#### FIRST FLOOR ENDWALL #1: UPLIFT DUE TO OVERTURNING

SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma L_i$ ) = SHEARWALL ADJUSTMENT FACTOR (C<sub>O</sub>) = SHEARWALL REACTION (Rend1) = 6749 lbs WALL HEIGHT (H) =

> UPLIFT FORCE (U<sub>E1</sub>) = R<sub>end1</sub> x H =  $\Sigma L_i \times C_O$

> > 10444 lbs U<sub>E1</sub> = 6749 lbs x 8 ft

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APPROVED

PFS CORPORATION

Bloomsburg, PA



### FIRST FLOOR ENDWALL #2 SHEATHING LENGTH REQUIREMENTS FOYER / MECH. ROOM

FIRST FLOOR WIDTH (W1) = 27.5 ft SECOND FLOOR WIDTH (W<sub>2</sub>) = 27.5 ft FIRST FLOOR LENGTH  $(L_1)$  = 39 ft SECOND FLOOR LENGTH (L<sub>2</sub>) = 33 ft

SHEARWALL TYPE: 7/16" OSB EXTERIOR (BLOCKED) w/ 7/16" OSB INTERIOR (BLOCKED)

SHEATHING EDGE 8d NAIL SPACING = 3 in O.C. (8d NAILS OR EQUIVALENT)

SHEARWALL STRENGTH (V) = 1260 plf MIN. SHEARWALL SEGMENT LENGTH = 2.3 ft SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma$  L<sub>i</sub>) = 6.42 ft 1st FL. PERCENT FULL HEIGHT SHEATHING= 100 % 1st FL. MAX. UNRESTRAINED OPENING HEIGHT = 0 ft

SHEAR ADJUSTMENT FACTOR ( $C_o$ ) = 1 (TABLE 2305.3.7.2, IBC)

TRIBUTARY LENGTH (TL) = 19.5 ft ADDITIONAL WALL LOAD = 0 lbs

SHEARWALL REACTION (R<sub>end1</sub>) = TL \* FL<sub>hoer</sub> + R<sub>end2</sub> + ADDITIONAL=

R<sub>end1</sub> = 19.5 ft \* 228 plf + 2987 lbs + 0 lbs = 7433 lbs

MIN. LENGTH SEGMENTED SHEARWALLS (Lsw) = Rend1 / V = 7433 lbs / 1260 plf = 5.90 ft

PERFORATED FULL HEIGHT SHEATHING LENGTH REQUIRED (ENDWALL) = L<sub>SW</sub> / C<sub>O</sub> = 5.9 ft / 1 = 5.90 ft

> PERFORATED FULL HEIGHT SHEATHING REQUIRED = 5.9 ft

PERFORATED FULL HEIGHT SHEATHING PROVIDED = 6.42 ft

ENDWALL SHEARWALLS OK ALL EXTERIOR SHEATHING TO BE BLOCKED UNO

### FIRST FLOOR ENDWALL #2: UPLIFT DUE TO OVERTURNING

SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma$  L<sub>i</sub>) = SHEARWALL ADJUSTMENT FACTOR (Co) = SHEARWALL REACTION ( $R_{end1}$ ) = 7433 lbs WALL HEIGHT (H) = 8 ft

> UPLIFT FORCE (U<sub>E1</sub>) = R<sub>end1</sub> x H =  $\Sigma L_i \times C_o$

> > U<sub>E1</sub> = 7433 lbs x 8 ft 9263 lbs 6.42 x 1



# FIRST FLOOR OFFSET SHEARWALL SHEATHING LENGTH REQUIREMENTS BEDROOM #1

$$\begin{split} & \text{FIRST FLOOR WIDTH (W}_1) = & 27.5 \text{ ft} \\ & \text{SECOND FLOOR WIDTH (W}_2) = & 27.5 \text{ ft} \\ & \text{FIRST FLOOR LENGTH (L}_1) = & 39 \text{ ft} \\ & \text{SECOND FLOOR LENGTH (L}_2) = & 33 \text{ ft} \end{split}$$

SHEARWALL TYPE: 7/16" OSB EXTERIOR (BLOCKED) w/ 7/16" OSB INTERIOR (BLOCKED)

SHEATHING EDGE 8d NAIL SPACING = 6 in O.C. (8d NAILS OR EQUIVALENT)

SHEARWALL STRENGTH (V) = 436 plf
MIN. SHEARWALL SEGMENT LENGTH = 2.3 ft
SUM OF FULL HEIGHT SHEATHING PROVIDED (2 L) = 7.42 ft
1st FL. PERCENT FULL HEIGHT SHEATHING= 54 %
1st FL. MAX. UNRESTRAINED OPENING HEIGHT = 5.35 ft

SHEAR ADJUSTMENT FACTOR ( $C_o$ ) = 0.684 (TABLE 2305.3.7.2, IBC)

TRIBUTARY LENGTH (TL) = 3 ft
ADDITIONAL WALL LOAD = 0 lbs

SHEARWALL REACTION ( $R_{end1}$ ) = TL \* FL<sub>i-per</sub> + ADDITIONAL=

R<sub>end1</sub> = 3 ft \* 228 plf + 0 lbs = 684 lbs

MIN. LENGTH SEGMENTED SHEARWALLS ( $L_{sw}$ ) =  $R_{end1}$  / V = 684 lbs / 436 plf = 1.57 ft

PERFORATED FULL HEIGHT SHEATHING LENGTH REQUIRED (ENDWALL) = L<sub>SW</sub> / C<sub>O</sub> = 1.57 ft / 0.684 = 2.30 ft

PERFORATED FULL HEIGHT SHEATHING

PERFORATED FULL HEIGHT SHEATHING

REQUIRED = 2.3 ft PROVIDED = 7.42 ft

### OFFSET SHEARWALL OK ALL EXTERIOR SHEATHING TO BE BLOCKED UNO

### FIRST FLOOR OFFSET SHEARWALL: UPLIFT DUE TO OVERTURNING

SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma$  L<sub>i</sub>) = 7.42 ft SHEARWALL ADJUSTMENT FACTOR ( $C_0$ ) = 0.684 SHEARWALL REACTION ( $R_{end1}$ ) = 684 lbs WALL HEIGHT (H) = 8 ft

UPLIFT FORCE ( $U_{E1}$ ) =  $\frac{R_{end1} \times H}{\sum L_i \times C_O}$  =

 $U_{E1} = \frac{684 \text{ lbs } \times 8 \text{ ft}}{7.42 \times 0.684}$  = 1079 lbs



### FIRST FLOOR ENDWALL: SHEAR CONNECTIONS

EFFECTIVE FIRST FLOOR WIDTH (W<sub>1</sub>) = 13.75 ft FIRST FLOOR LENGTH  $(L_1)$  = 39 ft 228 plf 1/2" ANCHOR BOLT Z= 1056 lbs 5/8" ANCHOR BOLT 1488 lbs Z = 0.162" x 3.5" COMMON NAIL (TOENAILED) Z = 158 lbs (1) SIMPSON LTP4 PLATE Z= 575 lbs

MAXIMUM FIRST FLOOR ENDWALL SHEAR LOAD = 7433 lbs

### RIMBAND TO SILL PLATE CONNECTION:

V = MAX ENDWALL SHEAR +  $L_1 x (3/4 * FL_{i-per}) / 2 =$ 

V = 7433 lbs + 39 ft x (3/4 \* 228 plf) / 2 10768 lbs

# TOENAILS PER FOOT = V / Z / W = 10768 lbs / 158 lbs / 13.75 ft = 5.0 NAILS / ft

TOENAIL SPACING = 12 / # = 12 / 5 = 2 " O.C. (16" MAX)

# LTP4 PLATES PER FOOT = V / Z / W = 10768 lbs / 575 lbs / 13.75 ft = 1.4 PLATES / ft

LTP4 PLATE SPACING = 12 / # = 12 / 1.4 = 8 " O.C. (72" MAX)

USE 0.162"  $\times$  3.5" COMMON NAIL (TOENAILED) @ 2" ON CENTER OR USE (1) SIMPSON LTP4 PLATE @ 8" ON CENTER OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 10768 lbs

### SILL PLATE TO FOUNDATION CONNECTION:

# 1/2" ANCHOR BOLTS = V / Z = 10768 lbs / 1056 lbs = 11 BOLTS

BOLT SPACING = (W - 2) / (N - 1) = (13.75 ft - 2) / (11 - 1) = 14 in

USE 1/2" ANCHOR BOLTS @ 14" O.C
ANCHOR BOLTS TO BE A MIN. OF 4" AND A MAX. OF 1'-0" FROM CORNERS
OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 10768 lbs (784 pif)

# 5/8" ANCHOR BOLTS = V / Z = 10768 lbs / 1488 lbs = 8 BOLTS

BOLT SPACING = (W - 2) / (N - 1) = (13.75 ft - 2) / (8 - 1) = 20 in

USE 5/8" ANCHOR BOLTS @ 20" O.C

ANCHOR BOLTS TO BE A MIN. OF 4" AND A MAX. OF 1'-0" FROM CORNERS OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 10768 lbs (784 pif)

APPROVED

DATE 7/20/17

PFS CORPORATION

Bloomsburg, PA

1306 plf

1158 plf

135 plf

### CHECK SHEATHING TO RIMBAND CONNECTION:

UNIT SHEAR CHECK:

SHEAR FORCE (V) =  $\frac{R_{end1}}{\sum L_i X C_O}$  =

FIRST FLOOR ENDWALL #1: V = 6749 lbs 5.17 ft \* 1

FIRST FLOOR ENDWALL #2:  $V = \frac{7433 \text{ lbs}}{6.42 \text{ ft} * 1}$ 

FIRST FLOOR OFFSET SHEARWALL:  $V = \frac{684 \text{ lbs}}{7.42 \text{ft} * 0.684}$ 

MAXIMUM FIRST FLOOR ENDWALL UNIT SHEAR = 1306 plf

CHECK # 8d NAILS REQUIRED FOR SHEATHING CONNECTION:

8d COMMON NAIL (FACE NAILED), 7/16" SIDE MEMBER Z = 95 lbs

# OF 8d NAILS PER FOOT = V = 1306 plf
Z 95 lbs / NAIL

# OF 8d NAILS PER FOOT = 13.75 NAILS PER FOOT

OVERALL 8d NAIL SPACING = 12 / # = 12 / 13.75 = 0.87 " O.C.

# OF ROWS: 3 ROW(S)

8d NAIL SPACING WITHIN EACH ROW = 3 \* SPACING 3 \* 0.87 o.c. 2 " O.C.

USE SHEATHING CONNECTION WITH 3 ROW(S) OF 8d NAILS AT 2" O.C.
OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 1306 plf

UNIT UPLIFT CHECK: (EQUAL TO UNIT SHEAR)

CHECK # 8d NAILS REQUIRED FOR SHEATHING CONNECTION:

8d COMMON NAIL (FACE NAILED), 7/16" SIDE MEMBER Z = 95 lbs

# OF 8d NAILS PER FOOT = V = 1306 plf
Z 95 lbs / NAIL

# OF 8d NAILS PER FOOT = 13.75 NAILS PER FOOT

OVERALL 8d NAIL SPACING = 12 / # = 12 / 13.75 = 0.87 " O.C.

# OF ROWS : 3 ROW(S)

8d NAIL SPACING WITHIN EACH ROW = 3 \* SPACING 3 \* 0.87 o.c. 2 " O.C.

USE SHEATHING CONNECTION WITH 3 ROW(S) OF 8d NAILS AT 2" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 1306 plf

ALTERNATE SHEATHING CONNECTION FOR UNIT UPLIFT (GLUE):

V = 1306 plf

200 psi MINIMUM CONSTRUCTION ADHESIVE Z = 200 psi (FACE)

WIDTH OF GLUE REQUIRED FOR SHEATHING CONNECTION ALONG FLOOR BAND:

WIDTH OF GLUE STRIP REQUIRED = V = 1306 plf = 1 

Z 200 psi \* 12" / ft

FASTEN SHEATHING TO BAND WITH 1" WIDE STRIP OF 200 psi MINIMUM CONSTRUCTION ADHESIVE PLUS (1) ROW OF 8d NAILS AT 6" o.c.



### SECOND FLOOR SIDEWALL #1 SHEATHING LENGTH REQUIREMENTS BEDROOM #2

FIRST FLOOR WIDTH (W1) = 27 5 ft SECOND FLOOR WIDTH (W<sub>2</sub>) = 27.5 ft FIRST FLOOR LENGTH (L<sub>1</sub>) = 39 ft SECOND FLOOR LENGTH (L<sub>2</sub>) = 33 ft

SHEARWALL TYPE: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR

SHEATHING EDGE 8d NAIL SPACING = 6 in O.C. (8d NAILS OR EQUIVALENT) SHEARWALL STRENGTH (V) = 436 plf

MIN. SHEARWALL SEGMENT LENGTH = 2.3 ft SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma$  L<sub>i</sub>) = 7.43 ft 2nd FL. PERCENT FULL HEIGHT SHEATHING= 100 % 2nd FL. MAX. UNRESTRAINED OPENING HEIGHT = 0 ft

SHEAR ADJUSTMENT FACTOR ( $C_o$ ) = 1 (TABLE 2305.3.7.2, IBC) 2nd FL. NUMBER OF SHEARWALLS (N<sub>siria</sub>) = 2

ADDITIONAL WALL LOAD = 0 lbs

SHEARWALL REACTION (Rside2) =  $W_2* w_{l-para} / N_{side} + ADDITIONAL = R_{side2} = 27.5 ft* 181 plf / 2 + 0 lbs =$ 

2489 lbs

MIN. LENGTH SEGMENTED SHEARWALLS ( $L_{sw}$ ) =  $R_{side2}$  / V = 2489 lbs / 436 plf = 5.71 ft

PERFORATED FULL HEIGHT SHEATHING LENGTH REQUIRED (SIDEWALL) =  $L_{SW}/C_0$  = 5.71 ft / 1 = 5.71 ft

PERFORATED FULL HEIGHT SHEATHING

PERFORATED FULL HEIGHT SHEATHING

REQUIRED = 5.71 ft PROVIDED = 7.43 ft

### SIDEWALL SHEARWALLS OK ALL EXTERIOR SHEATHING TO BE BLOCKED UNO

### SECOND FLOOR SIDEWALL #1: UPLIFT DUE TO OVERTURNING

SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma$  L<sub>i</sub>) = SHEARWALL ADJUSTMENT FACTOR (Co) = SHEARWALL REACTION (Rend1) = 2489 lbs WALL HEIGHT (H) = 8 ft

> UPLIFT FORCE (U<sub>E1</sub>) = R<sub>side1</sub> x H =  $\Sigma L_i \times C_O$

> > U<sub>E1</sub> = 2489 lbs x 8 ft 2680 lbs 7.43 ft x 1



### SECOND FLOOR SIDEWALL #2 SHEATHING LENGTH REQUIREMENTS SITTING / BEDROOM #3

FIRST FLOOR WIDTH (W<sub>1</sub>) = 27 5 ft SECOND FLOOR WIDTH (W<sub>2</sub>) = 27.5 ft FIRST FLOOR LENGTH (L<sub>1</sub>) = 39 ft SECOND FLOOR LENGTH (L<sub>2</sub>) = 33 ft

SHEARWALL TYPE: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR

SHEATHING EDGE 8d NAIL SPACING = 6 in O.C. (8d NAILS OR EQUIVALENT)

SHEARWALL STRENGTH (V) = 436 plf MIN. SHEARWALL SEGMENT LENGTH = 2.3 ft SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma$  L<sub>i</sub>) = 12 ft 82 %

2nd FL. PERCENT FULL HEIGHT SHEATHING= 2nd FL. MAX. UNRESTRAINED OPENING HEIGHT = 3.02 ft

SHEAR ADJUSTMENT FACTOR ( $C_o$ ) = 0.979 (TABLE 2305.3.7.2, IBC) 2nd FL. NUMBER OF SHEARWALLS (N<sub>siria</sub>) =

2 ADDITIONAL WALL LOAD = 0 lbs

SHEARWALL REACTION ( $R_{side2}$ ) =  $W_2$  \*  $w_{i-para}$  /  $N_{side}$  + ADDITIONAL=  $R_{side2}$  = 27.5 ft \* 181 plf / 2 + 0 lbs =

2489 lbs

MIN. LENGTH SEGMENTED SHEARWALLS ( $L_{sw}$ ) =  $R_{side2}$  / V = 2489 lbs / 436 plf = 5.71 ft

PERFORATED FULL HEIGHT SHEATHING LENGTH REQUIRED (SIDEWALL) =  $L_{SW}/C_{O}$  = 5.71 ft / 0.979 = 5.84 ft

PERFORATED FULL HEIGHT SHEATHING

PERFORATED FULL HEIGHT SHEATHING

REQUIRED = 5.84 ft PROVIDED = 12 ft

### SIDEWALL SHEARWALLS OK ALL EXTERIOR SHEATHING TO BE BLOCKED UNO

### SECOND FLOOR SIDEWALL #2: UPLIFT DUE TO OVERTURNING

SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma$  L<sub>i</sub>) = 12 ft SHEARWALL ADJUSTMENT FACTOR (Co) = SHEARWALL REACTION (Rend1) = WALL HEIGHT (H) = 8 ft

> UPLIFT FORCE (U<sub>E1</sub>) = R<sub>side1</sub> x H =  $\Sigma L_i \times C_O$

> > U<sub>E1</sub> = 2489 lbs x 8 ft 1695 lbs 12 ft x 0.979



### SECOND FLOOR SIDEWALL: SHEAR CONNECTIONS

SECOND FLOOR WIDTH (W2) =	27.5 ft	
EFFECTIVE SECOND FLOOR LENGTH (L2) =	15.83 ft	
FL <sub>I-para</sub> =	210 plf	
1/2" ANCHOR BOLT	Z =	1056 lbs
5/8" ANCHOR BOLT	Z =	1488 lbs
0.162" x 3.5" COMMON NAIL (TOENAILED)	Z =	158 lbs
0.162" x 3.5" COMMON NAIL (FACE NAILED)	Z =	191 lbs
(1) SIMPSON LTP4 PLATE	Z =	575 lbs

MAXIMUM SECOND FLOOR SIDEWALL SHEAR LOAD = 2489 plf

### BANDS TO BANDS & BOTTOM / TOP PLATE CONNECTION:

V = MAX SIDEWALL SHEAR +  $W_2$  x FL<sub>i-para</sub> / 2 =

V = 2489 lbs + 27.5 ft x 210 plf / 2 5377 plf

# TOENAILS PER FOOT = V / Z / L = 5377 lbs / 158 lbs / 15.83 ft = 2.1 NAILS / ft

TOENAIL SPACING = 12 / # = 12 / 2.1 = 5 " O.C. (16" MAX)

#MP4F PLATES PER FOOT = V / Z / W = 5377 lbs / 575 lbs / 15.83 ft = 0.6 PLATES / ft

MP4F PLATE SPACING = 12 / # = 12 / 0.6 = 20 "O.C. (72" MAX)

USE 0.162" x 3.5" COMMON NAIL (TOENAILED) @ 5" ON CENTER
OR USE (1) SIMPSON LTP4 PLATE @ 20" ON CENTER
OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 5377 lbs



### CHECK SHEATHING TO RIMBAND CONNECTION:

UNIT SHEAR CHECK:

SHEAR FORCE (V) =  $\frac{R_{side2}}{\Sigma L_i X C_O} =$ 

V = 2489 lbs 7.43 ft \* 1 SECOND FLOOR SIDEWALL #1: 335 plf

V = 2489 lbs 12 ft \* 0.979 SECOND FLOOR SIDEWALL #2: 212 plf

> MAXIMUM SECOND FLOOR SIDEWALL UNIT SHEAR = 335 plf

CHECK # 8d NAILS REQUIRED FOR SHEATHING CONNECTION:

8d COMMON NAIL (FACE NAILED), 7/16" SIDE MEMBER

# OF 8d NAILS PER FOOT =

# OF 8d NAILS PER FOOT = 3.53 NAILS PER FOOT

12 / # = 12 / 3.53 = OVERALL 8d NAIL SPACING = 3.39 " O.C.

> # OF ROWS : 1 ROW(S)

8d NAIL SPACING WITHIN EACH ROW = 1 \* SPACING 1 \* 3.39 o.c. 3 " O.C.

> USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 3" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 335 plf

UNIT UPLIFT CHECK: (EQUAL TO UNIT SHEAR)

CHECK # 8d NAILS REQUIRED FOR SHEATHING CONNECTION:

8d COMMON NAIL (FACE NAILED), 7/16" SIDE MEMBER

# OF 8d NAILS PER FOOT = V = 335 plf
Z 95 lbs / NAIL

# OF 8d NAILS PER FOOT = 3.53 NAILS PER FOOT

OVERALL 8d NAIL SPACING = 12 / # = 12 / 3.53 = 3.39 " O.C.

> 1 ROW(S) # OF ROWS :

8d NAIL SPACING WITHIN EACH ROW = 1 \* SPACING 1 \* 3.39 o.c. 3 " O.C.

> USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 3" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 335 plf

ALTERNATE SHEATHING CONNECTION FOR UNIT UPLIFT (GLUE):

V = 335 plf

200 psi MINIMUM CONSTRUCTION ADHESIVE Z = 200 psi (FACE)

WIDTH OF GLUE REQUIRED FOR SHEATHING CONNECTION ALONG FLOOR BAND:

WIDTH OF GLUE STRIP REQUIRED =  $\frac{V}{Z} = \frac{335 \text{ pif}}{200 \text{ psi}^* 12^* / \text{ft}}$ 

FASTEN SHEATHING TO BAND WITH 1" WIDE STRIP OF 200 psi MINIMUM CONSTRUCTION ADHESIVE PLUS (1) ROW OF 8d NAILS AT 6" o.c.



### FIRST FLOOR SIDEWALL #1 SHEATHING LENGTH REQUIREMENTS

FAMILY / BEDROOM #1

FIRST FLOOR WIDTH (W<sub>1</sub>) = SECOND FLOOR WIDTH (W2) = 27.5 ft FIRST FLOOR LENGTH (L1) = 39 ft SECOND FLOOR LENGTH  $(L_2)$  = 33 ft

SHEARWALL TYPE: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR

SHEATHING EDGE 8d NAIL SPACING = 6 in O.C. (8d NAILS OR EQUIVALENT) SHEARWALL STRENGTH (V) = 436 plf

MIN. SHEARWALL SEGMENT LENGTH = 2.3 ft FULL HEIGHT SHEATHING PROVIDED = 21.17 ft 1st FL. PERCENT FULL HEIGHT SHEATHING= 77 % 1st FL. MAX. UNRESTRAINED OPENING HEIGHT = 5.35 ft

SHEAR ADJUSTMENT FACTOR ( $C_o$ ) = 0.81 (TABLE 2305.3.7.2, IBC)

1st FL. NUMBER OF SHEARWALLS  $(N_{side})$  = ADDITIONAL WALL LOAD = 0 lbs

 $\begin{aligned} \text{SHEARWALL REACTION } (R_{\text{sidet}}) = & W_1 * FL_{\text{patra}} / N_{\text{side}} + R_{\text{sidez}} + \text{ADDITIONAL} = \\ R_{\text{sidet}} = & 27.5 \text{ ft * 210 plf} / 2 + 2489 \text{ lbs } + 0 \text{ lbs} = \end{aligned}$ 

5377 lbs

MIN. LENGTH SEGMENTED SHEARWALLS ( $L_{sw}$ ) =  $R_{side1}$  / V = 5377 lbs / 436 plf = 12.33 ft

PERFORATED FULL HEIGHT SHEATHING LENGTH REQUIRED (SIDEWALL) =  $L_{SW}/C_{O}$  = 12.33 ft/0.81 = 15.23 ft

PERFORATED FULL HEIGHT SHEATHING

PERFORATED FULL HEIGHT SHEATHING

REQUIRED = 15.23 ft PROVIDED = 21.17 ft

### SIDEWALL SHEARWALLS OK ALL EXTERIOR SHEATHING TO BE BLOCKED UNO

### FIRST FLOOR SIDEWALL #1: UPLIFT DUE TO OVERTURNING

SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma$  L<sub>i</sub>) = SHEARWALL ADJUSTMENT FACTOR (Co) = SHEARWALL REACTION (Rend1) = 5377 lbs WALL HEIGHT (H) =

> UPLIFT FORCE (U<sub>E1</sub>) = R<sub>side1</sub> x H =  $\Sigma \; L_i \; x \; C_O$

> > U<sub>E1</sub> = 5377 lbs x 8 ft 2509 lbs 21.17 x 0.81



### FIRST FLOOR SIDEWALL #2 SHEATHING LENGTH REQUIREMENTS DINING / MECH. ROOM

FIRST FLOOR WIDTH (W<sub>1</sub>) = SECOND FLOOR WIDTH (W2) = 27.5 ft FIRST FLOOR LENGTH (L1) = 39 ft SECOND FLOOR LENGTH  $(L_2)$  = 33 ft

SHEARWALL TYPE: 7/16" OSB EXTERIOR (BLOCKED) w/ 1/2" GWB INTERIOR

SHEATHING EDGE 8d NAIL SPACING = 6 in O.C. (8d NAILS OR EQUIVALENT) SHEARWALL STRENGTH (V) = 436 plf

MIN. SHEARWALL SEGMENT LENGTH = 2.3 ft FULL HEIGHT SHEATHING PROVIDED = 17.25 ft 1st FL. PERCENT FULL HEIGHT SHEATHING= 1st FL. MAX. UNRESTRAINED OPENING HEIGHT = 5.35 ft

SHEAR ADJUSTMENT FACTOR (Co) = 0.772 (TABLE 2305.3.7.2, IBC)

1st FL. NUMBER OF SHEARWALLS  $(N_{side})$  = ADDITIONAL WALL LOAD = 0 lbs

 $\begin{aligned} \text{SHEARWALL REACTION } (R_{aldet}) &= W_1 * FL_{l-patrs} / N_{alde} * R_{aldez} * \text{ADDITIONAL} = \\ R_{aldet} &= 27.5 \text{ ft * 210 plf} / 2 * + 2489 \text{ lbs * 0 lbs} = \end{aligned}$ 

5377 lbs

MIN. LENGTH SEGMENTED SHEARWALLS ( $L_{sw}$ ) =  $R_{side1}$  / V = 5377 lbs / 436 plf = 12.33 ft

PERFORATED FULL HEIGHT SHEATHING LENGTH REQUIRED (SIDEWALL) =  $L_{SW}/C_{O}$  = 12.33 ft / 0.772 = 15.98 ft

PERFORATED FULL HEIGHT SHEATHING

PERFORATED FULL HEIGHT SHEATHING

REQUIRED = 15.98 ft PROVIDED = 17.25 ft

### SIDEWALL SHEARWALLS OK ALL EXTERIOR SHEATHING TO BE BLOCKED UNO

### FIRST FLOOR SIDEWALL #2: UPLIFT DUE TO OVERTURNING

SUM OF FULL HEIGHT SHEATHING PROVIDED ( $\Sigma$  L<sub>i</sub>) = SHEARWALL ADJUSTMENT FACTOR (Co) = SHEARWALL REACTION (Rend1) = 5377 lbs WALL HEIGHT (H) =

> UPLIFT FORCE (U<sub>E1</sub>) = R<sub>side1</sub> x H =  $\Sigma L_i \times C_O$

> > U<sub>E1</sub> = 5377 lbs x 8 ft 17.25 x 0.772 3231 lbs



### FIRST FLOOR SIDEWALL: SHEAR CONNECTIONS

FIRST FLOOR WIDTH (W<sub>1</sub>) = 27.5 ft EFFECTIVE FIRST FLOOR LENGTH  $(L_1)$  = 33 ft FL<sub>I-para</sub> = 210 plf 1/2" ANCHOR BOLT 1056 lbs 7 = 5/8" ANCHOR BOLT 1488 lbs Z = 0.162" x 3.5" COMMON NAIL (TOENAILED) Z = 158 lbs (1) SIMPSON LTP4 PLATE Z= 575 lbs

MAXIMUM FIRST FLOOR SIDEWALL SHEAR LOAD = 5377 lbs

RIMBAND TO SILL PLATE CONNECTION:

V = MAX SIDEWALL SHEAR +  $W_1 \times (3/4 * FL_{i-para}) / 2 =$ 

V = 5377 lbs + 27.5 ft x (3/4 \* 210 plf) / 2 7543 lbs

# TOENAILS PER FOOT = V/Z/L<sub>1</sub> = 7543 lbs / 158 lbs / 33 ft = 1.4 NAILS / ft

TOENAIL SPACING = 12 / # = 12 / 1.4 = 8 "O.C. (16" MAX)

,

# MP4F PLATES PER FOOT = V / Z / W = 7543 lbs / 575 lbs / 33 ft = 0.4 PLATES / ft

MP4F PLATE SPACING = 12 / # = 12 / 0.4 = 30 " O.C. (72" MAX)

USE 0.162" x 3.5" COMMON NAIL (TOENAILED) @ 8" ON CENTER OR USE (1) SIMPSON LTP4 PLATE @ 30" ON CENTER OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 7543 lbs

SILL PLATE TO FOUNDATION CONNECTION:

# 1/2" ANCHOR BOLTS = V / Z = 7543 lbs / 1056 lbs = 8 BOLTS

BOLT SPACING = (L-2)/(N-1) = (33 ft-2)/(8-1) = 53 in

USE 1/2" ANCHOR BOLTS @ 53" O.C ANCHOR BOLTS TO BE A MIN. OF 4" AND A MAX. OF 1'-0" FROM CORNERS OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 7543 lbs (229 pif)

# 5/8" ANCHOR BOLTS = V / Z = 7543 lbs / 1488 lbs = 6 BOLTS

BOLT SPACING = (L - 2) / (N - 1) = (33 ft - 2) / (6 - 1) = 72 in

USE 5/8" ANCHOR BOLTS @ 72" O.C ANCHOR BOLTS TO BE A MIN. OF 4" AND A MAX. OF 1'-0" FROM CORNERS OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 7543 lbs (229 pif)



### CHECK SHEATHING TO RIMBAND CONNECTION:

### UNIT SHEAR CHECK:

SHEAR FORCE (V) =  $\frac{R_{side1}}{\sum L_i X C_O}$  =

FIRST FLOOR SIDEWALL #1:  $V = \frac{5377 \text{ lbs}}{21.17 \text{ ft} * 0.81}$  = 314 plf

FIRST FLOOR SIDEWALL #2: V = 5377 lbs = 404 plf 17.25 \* 0.772

MAXIMUM FIRST FLOOR SIDEWALL UNIT SHEAR = 404 plf

CHECK # 8d NAILS REQUIRED FOR SHEATHING CONNECTION:

8d COMMON NAIL (FACE NAILED), 7/16" SIDE MEMBER Z = 95 lbs

# OF 8d NAILS PER FOOT = V = 404 plf
Z 95 lbs / NAIL

# OF 8d NAILS PER FOOT = 4.26 NAILS PER FOOT

OVERALL 8d NAIL SPACING = 12 / # = 12 / 4.26 = 2.81 " O.C.

# OF ROWS : 1 ROW(S)

8d NAIL SPACING WITHIN EACH ROW = 1 \* SPACING 1 \* 2.81 o.c. 2 " O.C.

# USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 2" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 404 plf

### UNIT UPLIFT CHECK: (EQUAL TO UNIT SHEAR)

CHECK # 8d NAILS REQUIRED FOR SHEATHING CONNECTION:

8d COMMON NAIL (FACE NAILED), 7/16" SIDE MEMBER Z = 95 lbs

# OF 8d NAILS PER FOOT = V = 404 plf
Z 95 lbs / NAIL

# OF 8d NAILS PER FOOT = 4.26 NAILS PER FOOT

OVERALL 8d NAIL SPACING = 12 / # = 12 / 4.26 = 2.81 " O.C.

# OF ROWS : 1 ROW(S)

8d NAIL SPACING WITHIN EACH ROW = 1 \* SPACING 1 \* 2.81 o.c. 2 " O.C.

# USE SHEATHING CONNECTION WITH 1 ROW(S) OF 8d NAILS AT 2" O.C. OR CONNECTION TO WITHSTAND A SHEAR FORCE OF 404 plf

### ALTERNATE SHEATHING CONNECTION FOR UNIT UPLIFT (GLUE):

V = 404 plf

200 psi MINIMUM CONSTRUCTION ADHESIVE Z = 200 psi (FACE)

WIDTH OF GLUE REQUIRED FOR SHEATHING CONNECTION ALONG FLOOR BAND:

WIDTH OF GLUE STRIP REQUIRED =  $\frac{V}{Z} = \frac{404 \text{ pif}}{200 \text{ psi}^* 12" / \text{ft}} = 1$ 

FASTEN SHEATHING TO BAND WITH 1" WIDE STRIP OF 200 psi MINIMUM CONSTRUCTION ADHESIVE PLUS (1) ROW OF 8d NAILS AT 6" o.c.

### SHEARWALL HOLDOWN DESIGN

SHEARWALL UPLIFT FROM EACH FLOORS			
2nd FLOOR SIDEWALL #1	2680	lbs	
2nd FLOOR SIDEWALL #2	1695	lbs	
2nd FLOOR ENDWALL #1	3052	lbs	
2nd FLOOR ENDWALL #2	4477	lbs	
1st FLOOR SIDEWALL #1	2509	lbs	
1st FLOOR SIDEWALL #2	3231	lbs	
1st FLOOR ENDWALL #1	10444	lbs	
1st FLOOR ENDWALL #2	9263	lbs	
1st FLOOR OFFSET SHEARWALL	1079	lbs	

DEAD LOAD	UNIT WEIGHT (PSF)
TRUSS DEAD	15
FLOOR DEAD	10
WALL DEAD	12

# | STORY HEIGHT | HEIGHT (ft) | 1ST FLOOR | 8 | 2nd FLOOR | 8 | 2nd FLOOR | 0 |



13.75

16d COMMON NAILS



	COMPRESSION	COMPRESSION		TENSION CAPACITY (lbs) (Cd
	CAPACITY (lbs) (Cd =	CAPACITY (lbs)	COMPRESSION CAPACITY (lbs) (Cd = 1.6)	= 1.6)
SPF #2 VALUE	1.0)	(Cd = 1.15)		- 1.0)
2X4 (8 FT)	2603	2660	2745	5670
2X4 (9 FT)	2115	2153	2203	5670
2X4 (10 FT)	1744	1771	1802	5670
2X6 (8 FT)	7494	8058	9141	7722
2X6 (9 FT)	6629	7005	7668	7722
2X6 (10 FT)	5792	6041	6453	7722

SIMPSON STRAP	CAPACITY		<u>FASTENERS</u>
SIMPSON CS16 COILED STRAP	1705	22	10d NAILS
SIMPSON CS14 COILED STRAP	2490	30	10d NAILS
SIMPSON CMSTC16 COILED STRAP	4585	58	16d SINKER NAILS
SIMPSON CMST14 COILED STRAP	6490	66	16d NAILS
SIMPSON CMST12 COILED STRAP	9215	84	16d NAILS
*** CADACITY ORTAINED EDOM SIMPSON STRONG TIE 2015 16 WOOD CONSTRUCTION CONNECTIONS CATALOG			

 1/4" LAG SCREWS
 225 lbs

 3/8" LAG SCREWS
 295 lbs

 1/2" LAG SCREWS
 555 lbs

 5/8" LAG SCREWS
 789 lbs

\*\* ALL WITH Cd = 1.6 FACTOR

191 lbs

HOLDOWN	CAPACITY (lbs)
SIMPSON PA51	2025
SIMPSON HD5B W/(2) STUDS	3785
SIMPSON STHD14RJ	4210
SIMPSON HDU8-SDS2.5 W/ (2) STUDS	4870
SIMPSON HD7B W/(3) STUDS	6245
SIMPSON HD9B W/(4) STUDS	8430
SIMPSON HD12 W/(4) STUDS W/ 1-1/8" ANCHOR BOLT	12690
SIMPSON HD19 W/(4) STUDS W/ 1-1/4" ANCHOR BOLT	16210

<sup>\*\*\*</sup> CAPACITY OBTAINED FROM SIMPSON STRONG-TIE 2015-16 WOOD CONSTRUCTION CONNECTIONS CATALOG

### NET UPLIFT CALCULATIONS (UPLFIT - DEAD LOAD)

DEVVALL#1	
7.43	ft
443.849625	lbs
2236	lbs
1	2X6 STUDS
	7.43 443.849625 <b>2236</b>

SHEARWALL LENGTH	27.53 ft	
DEAD LOAD	1360.67025 lbs	
NET UPLIFT	1148 lbs	
STUDS REQUIRED	2 2X6 STUD	S

1st FLOOR SIDEWALL #1

2nd FLOOR SI	DEWALL #2	
SHEARWALL LENGTH	14.56	ft
DEAD LOAD	869.778	lbs
NET UPLIFT	825	lbs
STUDS REQUIRED	1	2X6 STUDS

	1st FLOOR SIDEWAL	L #2
SHEARWALL LENGTH	24.47	ft
DEAD LOAD	1209.42975	lbs
NET UPLIFT	2847	lbs
STUDS REQUIRED	2	2X6 STUDS

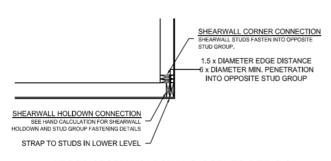
2nd FLOOR E	NDWALL #1	
SHEARWALL LENGTH	7.83	ft
DEAD LOAD	225.504	lbs
NET UPLIFT	2826	lbs
STUDS REQUIRED	1	2X6 STUDS

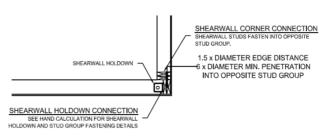
	1st FLOOR ENDWAL	L #1
SHEARWALL LENGTH	5.17	ft
DEAD LOAD	148.896	lbs
NET UPLIFT	13122	lbs
STUDS REQUIRED	3	2X6 STUDS

2nd FLOOR E	NDWALL #2	
SHEARWALL LENGTH	27.5	ft
DEAD LOAD	792	lbs
NET UPLIFT	3685	lbs
STUDS REQUIRED	1	2X6 STUDS

	1st FLOOR ENDWAL	L #2
SHEARWALL LENGTH	2.42	ft
DEAD LOAD	69.696	lbs
NET UPLIFT	12878	lbs
STUDS REQUIRED	2	2X6 STUDS

1	st FLOOR OFFSET SHE	ARWALL
SHEARWALL LENGTH	13.75	ft
DEAD LOAD	396	lbs
NET UPLIFT	683	lbs
STUDS REQUIRED	2	2X6 STUDS





### UPPER STORY HOLDOWN @ CORNER DETAILS

### 1ST STORY HOLDOWN @ CORNER DETAILS

### SECOND FLOOR SHEAR WALL HOLDOWN CONNECTION #1

USE (1) SIMPSON CMSTC16 COILED STRAP W/(47) 16d SINKER NAILS TOTAL @ EACH STRAP STUDS ATTACHED TOGETHER W/ 2 ROWS OF 16d COMMON NAILS @ 9" ON CENTER OR CONNECTION TO WITHSTAND 3685 lbs TENSION

### FIRST FLOOR SHEAR WALL HOLDOWN CONNECTION #1

NET UPLIFT =	3685	lbs	
HOLDOWN =	SIMPSON STHD14RJ		
HOLDOWN CAPACITY =	4210	lbs	O.K.
STUDS REQUIRED =	2	2X6 STUDS	
ROWS OF FASTENERS =	2	ROWS	
16d NAIL SPACING =	9	"O.C.	

#### USE A SIMPSON STHD14RJ

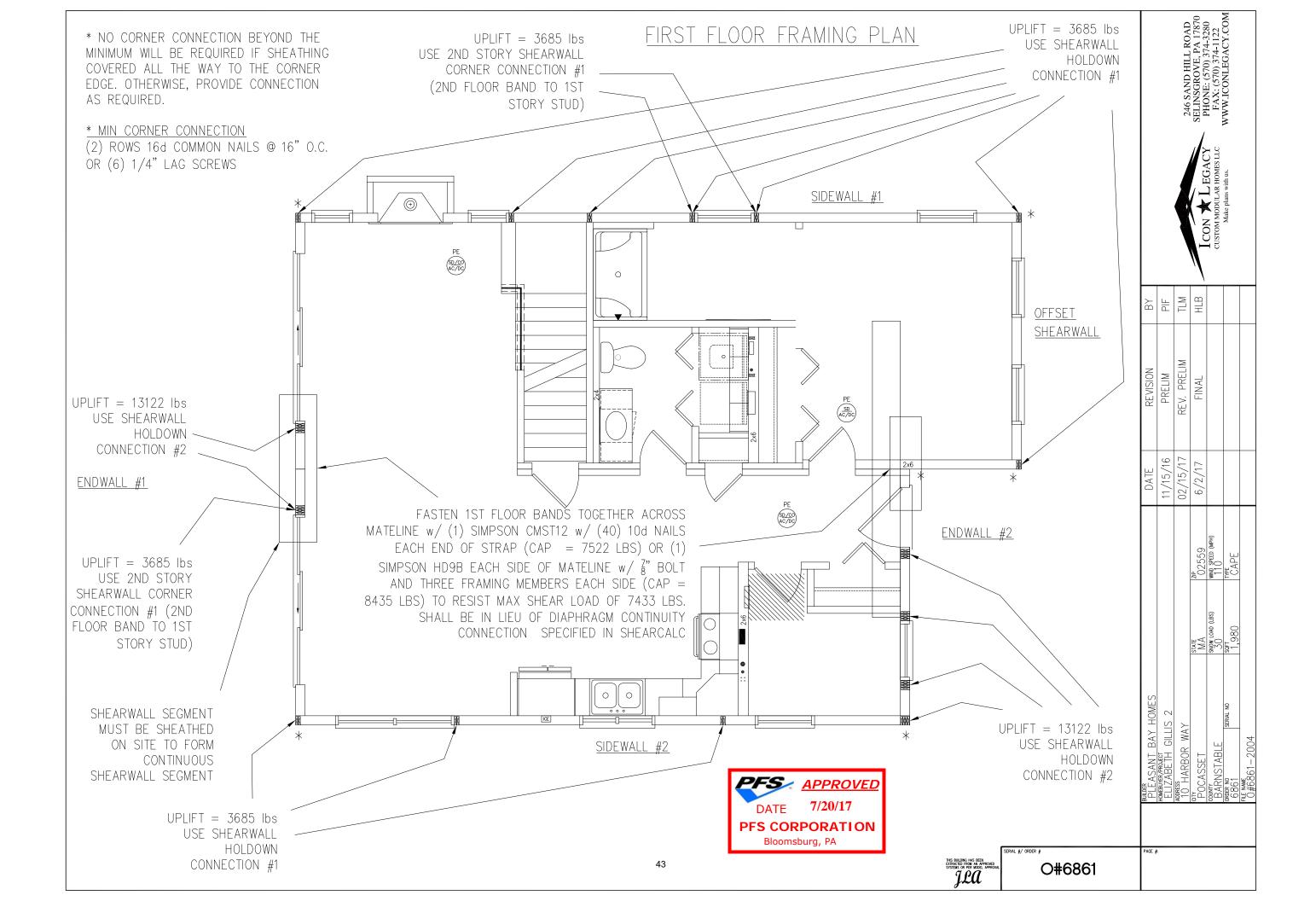
SHEARWALL EDGE STUDS ATTACHED TOGETHER W/ 2 ROWS OF 16d COMMON NAILS @ 9" ON CENTER OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 3685 lbs

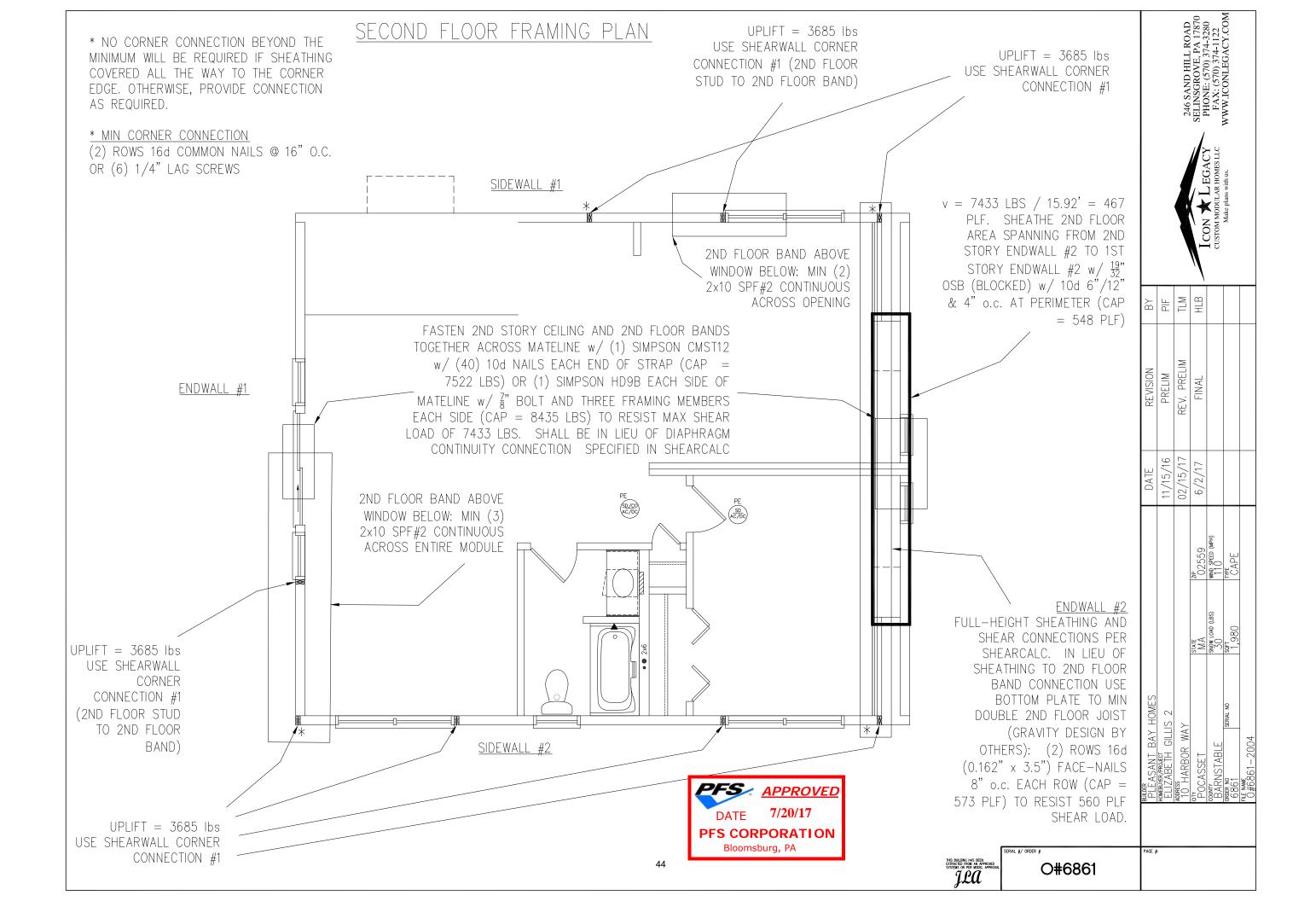
### FIRST FLOOR SHEAR WALL HOLDOWN CONNECTION #2

NET UPLIFT =	13122	lbs		
HOLDOWN =	SIMPSON HD19 W/(4) S	STUDS W/ 1-1/4"	ANCHOR BOLT	
HOLDOWN CAPACITY =	16210	lbs	O.K.	
STUDS REQUIRED =	4	2X6 STUDS		
ROWS OF FASTENERS =	2	ROWS		
16d NAIL SPACING =	2	"O.C.		

USE A SIMPSON HD19 W/(4) STUDS W/ 1-1/4" ANCHOR BOLT SHEARWALL EDGE STUDS ATTACHED TOGETHER W/ 2 ROWS OF 16d COMMON NAILS @ 2" ON CENTER OR CONNECTION TO WITHSTAND AN UPLIFT FORCE OF 13122 lbs

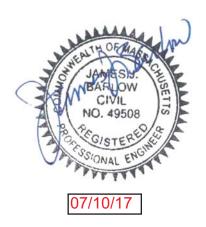








# **Section 3** HAND CALCULATIONS



Project: BEAM CALCS

Location: 2ND FLOOR BAND-1 Multi-Loaded Multi-Span Beam

[2015 International Building Code(2012 NDS)]

(3) 1.5 IN x 9.25 IN x 11.29 FT #2 - Spruce-Pine-Fir - Dry Use

Ethan Loewenthal **Barlow Engineering** 6512 Six Forks Rd. Suite 203B Raleigh, NC 27615

StruCalc Version 10.0.1.5

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Section Adequate By: 27.8% Controlling Factor: Deflection

### **CAUTIONS**

\* Laminations are to be fully connected to provide uniform transfer of loads to all members

DEFLECTIONS	C	enter	
DEI LEGINORIO		<del></del>	
Live Load	-0.29	IN L/460	
Dead Load	0.01	in	
Total Load	-0.29	IN L/471	
Live Load Deflection Criteria: L/360			Total Load Deflection Criteria: L/240

<u>REACTIONS</u>	<u>A</u>		<u>B</u>	
Live Load	-1925	lb	-901	lb
Dead Load	43	lb	43	lb
Total Load	-1882	lb	-858	lb
Uplift (1.5 F.S)	-1896	lb	-873	lb
Bearing Length	0.02	in	0.02	in

BEAM DATA	<u>Ce</u>	nter			
Span Length	11.29	ft			
Unbraced Length-Top	0	ft			
Unbraced Length-Bottom	11.29	ft			
Live Load Duration Factor	1.60				
Notch Depth	0.00				

### **MATERIAL PROPERTIES**

#2 - Spruce-Pine-Fir

Shear Stress:

Base Values **Adjusted** 875 psi Fb' = Bending Stress: Fb = 1730 psi

Cd=1.60 CI=0.98 CF=1.10 Cr=1.15 Fv = 135 psi Fv' = 216 psi

Cd=1.60

Modulus of Elasticity: E = 1400 ksi E' = 1400 ksi Comp. <sup>⊥</sup> to Grain: Fc - <sup>⊥</sup> = 425 psi  $Fc - \bot' = 425 \text{ psi}$ 

-6813 ft-lb **Controlling Moment:** 

3.61 Ft from left support of span 2 (Center Span)

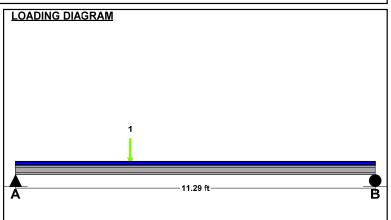
Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: -1909 lb

3.0 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Comparisons with required sections:	Req'd	<u>Provided</u>
Section Modulus:	47.26 in3	64.17 in3
Area (Shear):	13.25 in2	41.63 in2
Moment of Inertia (deflection):	232.26 in4	296.79 in4
Moment:	-6813 ft-lb	9251 ft-lb
Shear:	-1909 lb	5994 lb



UNIFORM LOADS	<u>Center</u>
Uniform Live Load	0 plf
Uniform Dead Load	0 plf
Beam Self Weight	8 plf
Total Uniform Load	8 plf

### **POINT LOADS - CENTER SPAN**

Load Number One Page 1 Live Load -2826 lb Dead Load 0 lb Location 3.6 ft

**NOTES** 



Project: BEAM CALCS

Location: 2ND FLOOR BAND-2 Multi-Loaded Multi-Span Beam

[2015 International Building Code(2012 NDS)]

(2) 1.5 IN x 9.25 IN x 3.2 FT #2 - Spruce-Pine-Fir - Dry Use Section Adequate By: 204.2% Controlling Factor: Moment Ethan Loewenthal Barlow Engineering 6512 Six Forks Rd. Suite 203B Raleigh, NC 27615

StruCalc Version 10.0.1.5

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### **CAUTIONS**

\* Laminations are to be fully connected to provide uniform transfer of loads to all members

DEFLECTION	<u>s</u>	<u>enter</u>	
Live Load	-0.01	IN L/4033	
Dead Load	0.00	in	
Total Load	-0.01	IN L/4051	
Live Load Deflection Criteria: L/360			Total Load Deflection Criteria: L/240

<u>REACTIONS</u>	<u>A</u>	<u>B</u>	
Live Load	-1118 lb	-1118	lb
Dead Load	8 lb	8	lb
Total Load	-1110 lb	-1110	lb
Uplift (1.5 F.S)	-1113 lb	-1113	lb
Bearing Length	0.01 in	0.01	in

BEAM DATA	<u>Center</u>
Span Length	3.2 ft
Unbraced Length-Top	0 ft
Unbraced Length-Bottom	3.2 ft
Live Load Duration Factor	1.60
Notch Depth	0.00

### **MATERIAL PROPERTIES**

#2 - Spruce-Pine-Fir

	<u>Base</u>	: values	<u>A0</u>	<u>justea</u>
Bending Stress:	Fb =	875 psi	Fb' =	1521 psi

Cd=1.60 Cl=0.99 CF=1.10

Shear Stress: Fv = 135 psi Fv' = 216 psi

Cd=1.60

Modulus of Elasticity: E = 1400 ksi E' = 1400 ksi Comp.  $^{\perp}$  to Grain: Fc -  $^{\perp}$  = 425 psi Fc -  $^{\perp}$  = 425 psi

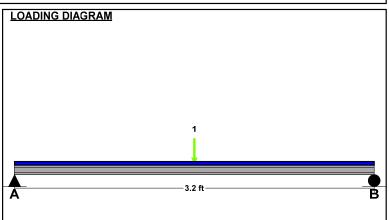
# Controlling Moment: -1782 ft-lb 1.6 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: -1118 lb 2.0 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Comparisons with required sections:	Reg'd	<u>Provided</u>
Section Modulus:	14.06 in3	42.78 in3
Area (Shear):	7.76 in2	27.75 in2
Moment of Inertia (deflection):	17.66 in4	197.86 in4
Moment:	-1782 ft-lb	5422 ft-lb
Shear:	-1118 lb	3996 lb



UNIFORM LOADS	<u>Center</u>
Uniform Live Load	0 plf
Uniform Dead Load	0 plf
Beam Self Weight	5 plf
Total Uniform Load	5 plf

### **POINT LOADS - CENTER SPAN**

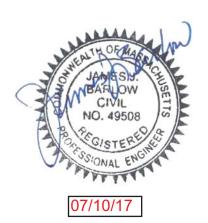
Load Number One
Live Load -2236 lb
Dead Load 0 lb
Location 1.6 ft

**NOTES** 





# **Section 4 ALTERNATE CALCULATIONS**



### **ALTERNATE CONNECTIONS**

PROJECT NUMBER: 0278nec2017

### PER ESR-1539 (JULY 2016)

### TABLE 8

	ALLOWABLE SHEAR VALUE (PLF)
7/16" O.S.B. Sheathing w/ 16, 15 & 14 GA. Staples @ 2" O. C.	324

- \* Staple must have a 7-16 -inch minimum crown width and must be installed with their crown parallel to the long direction of the framing member.
- \*\* Framing adjoining panel edge must be 3-inch nominal or wider
- \*\*\* Shear value assumed fasteners attached along the total length of the framing member specified.

### Required Sidewall Stud Tie Down

STUD SPACING 16 inch

1. 2<sup>nd</sup> Floor Stud to Top Plate

 Load =
 430 lbs

 UNIFORM LOAD
 323 plf

7/16" O.S.B. Sheathing w/ 16 GA. Staples @ 2" O. C.

2. 2<sup>nd</sup> Floor Stud to Floor Band - 2<sup>nd</sup> Floor Band to 1<sup>st</sup> Floor Ceiling Band

Load = 354 lbs UNIFORM LOAD 266 plf

7/16" O.S.B. Sheathing w/ 16 GA. Staples @ 2" O. C.

3. 1st Floor Stud to Ceiling Band

Load = 299 lb UNIFORM LOAD 225 pl

7/16" O.S.B. Sheathing w/ 16 GA. Staples @ 2" O. C.

4. 1st Floor Stud to Floor Band

 Load =
 223 lbs

 UNIFORM LOAD
 168 plf

7/16" O.S.B. Sheathing w/ 16 GA. Staples @ 2" O. C.

5. Second Floor Horizontal Floor Diaphragm Continuity

 Module to Module (Along Mate Line)

 Load =
 2822 lbs

 3/8" LAG SCREWS =
 288 lbs

 NUMBER OF SCREWS REQUIRED
 10 SCREWS

Use (10) 3/8" lag screws to attach module to module along mate line. (Minimum 1" penetration in last band)

6. First Floor Horizontal Floor Diaphragm Continuity

 Module to Module (Along Mate Line)

 Load =
 3335 lbs

 3/8" LAG SCREWS =
 288 lbs

 NUMBER OF SCREWS REQUIRED
 12 SCREWS

Use (12) 3/8" lag screws to attach module to module along mate line. (Minimum 1" penetration in last band)

STAPLES PROPERTIES:

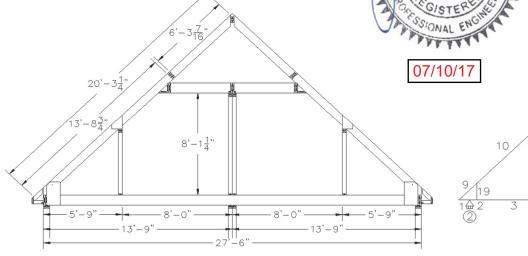
SPECIES GROUP III

LOAD DURATION FACTOR CD 1.6 WIND DESIGN)

SPECIFIC GRAVITY 0.42

STAPLES	MIN CROWN (INCH)	WIRE DIA. (INCH)	MIN. PENETR (INCH)	ATION LAT	ERAL CAPA	CITY WIT	HDRAWN CAPAC S / IN PENETRAT	
16, 15 & 14 GAGE	7/16	0.063	1		67	,	20	,





13 14

12 25 26 15

11 16

20 21 22 23 17

24 18

3 4 5 5 6 88

TRUSS NO.: 4BOX-CAPE-27-6

JOB NO.: 170367 PITCH: 12/12

SPAN: 27'-6"

TRUSS CENTERS: 16 in O.C.

 GROUND SNOW LOAD:
 30 psf
 TC DL:

 \* BALANCED SNOW LOAD:
 17.76 psf
 BC DL:

UNBALANCED SNOW LOAD: 47.51 psf BC LL: 10 psf WHERE h < 42" OPPOSITE SIDE UNB. SNOW LOAD: 5.328 psf BC LL: 20 psf WHERE h  $\geq$  42"

UNBALANCED SNOW LOAD LENGTH: 4.432 ft BC LL: 40 psf BETWEEN KNEEWALLS

**APPLIED MWFRS UPLIFT:** 33.61 psf WINDWARD AT 110 mph

19.09 psf LEEWARD AT 110 mph

10 psf

10 psf

APPLIED C & C UPLIFT: 33.61 psf AT 110 mph

### **MEMBER INFORMATION:**

	SIZE &
MEMBER	SPECIES
1 - 8	2 x 10 SPF #2
9 - 12 & 15 - 18	2 x 10 SPF #2
13-14	2 x 8 SPF #2
19 - 24	2 x 4 SPF #2
25 - 26	2 x 6 SPF #2

### NOTES:

- 1. MATING WALL REACTIONS ARE TOTAL FOR BOTH SIDES.
- 2. WIND PER ASCE 7-05, 110 mph (Vasd), EXP. C.
- 3. SNOW PER ASCE 7-05 30 psf GSL, Ct = 1.1, Ce = 1.0
  DRIFTING LENGTH IS LATERAL DISTANCE FROM RIDGE.
- 4. COMPONENT DESIGN IS BASED ON C & C PRESSURES



MAXIMUM SUPPORT REAC	TIONS (lbs):		MWFRS	C & C	
		DL + LL +	0.6 DL +	0.6 DL +	
	DEAD	30 psf	110 mph	110 mph	
	LOAD	GSL	UPLIFT	UPLIFT	
EXTERIOR WALL (2 & 8)	476	1299	-314	-357	
MATING WALL (5)	154	648	-99	0	

### **MAXIMUM INTERACTION & DEFLECTION:**

		MAXIMUM	
	MAXIMUM	DEFLECTION	
	CSI	(in)	<i>l 1</i>
BOTTOM CHORD	0.903	0.54	318
TOP CHORD	0.925	1.331	182
WEB	0.415	0.00	****

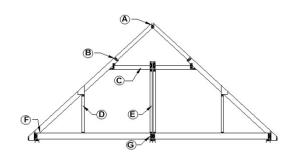


### **TRUSS CONNECTIONS**

PROJECT NUMBER: 170367

TRUSS NUMBER: 4BOX-CAPE-27-6

TRUSS PITCH: 12/12
TRUSS SPAN: 27'-6"



### UPLIFT CONNECTIONS (MWFRS LOADS):

110 mph										
EXTERIOR WALL			CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END
UPLIFT (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
314	WIND	1.6	OK	4	6	OK	3	6	OK	3
,	ALTERNATE:	(4) 16 d NAILS	TOENAILED THROUGH	BC INTO BA	ND PLUS (3) 16	d NAILS THROUGH SHI	EATHING INT	O BAND AND S	TUD	
MATING WALL			CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END
UPLIFT (lbs / PER SIDE)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
50	WIND	1.6	OK	2	2	OK	2	2	OK	2
,	ALTERNATE: (2) 16 d NAILS TOENAILED THROUGH BC INTO BAND PLUS (2) 16 d NAILS THROUGH SHEATHING INTO BAND AND STUD									

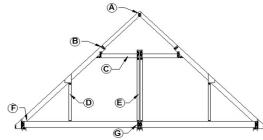


### TRUSS CONNECTIONS

PROJECT NUMBER: 170367

TRUSS NUMBER: 4BOX-CAPE-27-6

TRUSS PITCH: 12/12
TRUSS SPAN: 27'-6"



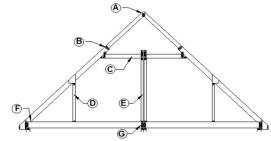
MAXIMUM OF DULL I	20 == £ CCL 8	0 C DL + 440	- WIND							
MAXIMUM OF DL + LL +	SU PST GSL &	0.6 DL + 110 Mp	טאואט חכ							
CONDITION "A" - RIDGE			CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
122	WIND	1.6	ОК	2	3	ОК	2	3	OK	2
		ALTERNATE:	USE (2) 8 d NAILS EAC	H END OF 1	x 4		•			•
SHEAR (lbs)	CASE	CD								
173	SNOW	1.15	USE (2) 16 d NAILS INT	SE (2) 16 d NAILS INTO END GRAIN EACH END PLUS USE 10 d NAILS AT 10 in O.C. THROUGH PLATES						
CONDITION "B" - TOP C	HORD FLIP:									
TENSION (lbs)	CASE	CD								
84	WIND	1.6	USE (2) 6 d NAILS THR	USE (2) 6 d NAILS THROUGH SHEATHING EACH SIDE						
		ALTERNATE:	USE (2) 16 ga STAPLE THROUGH SHEATHING EACH SIDE							
SHEAR (lbs)	CASE	CD								
173	SNOW	1.15	USE (2) 16 d NAILS TO	ENAILED EA	CH END PLUS (	JSE 10 d NAILS AT 10 in	O.C. THROU	JGH PLATES		
CONDITION "C" - COLLA	R TIE:									
AT RAFTER			CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
529	WIND	1.6	NO GOOD	N/A	N/A	OK	4	10	OK	4
SHEAR (lbs)	CASE	CD						-		
529	WIND	1.6	USE (2) 16 d NAILS TH	ROUGH BAN	D INTO ENDGR	AIN				
		AND	OK FOR SIMPSON H3	TWIST STRA	P w/ (8) 8 d NAIL	S BAND TO RAFTER				
AT MATING WALL			CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
529	WIND	1.6	NO GOOD	N/A	N/A	OK	4	10	OK	4
SHEAR (lbs)	CASE	CD								
4	SNOW	1.15	USE (2) 16 d NAILS TH	ROUGH BAN	D INTO ENDGR	AIN	<del></del>			<del></del>

### **TRUSS CONNECTIONS**

PROJECT NUMBER: 170367

TRUSS NUMBER: 4BOX-CAPE-27-6

TRUSS PITCH: 12/12
TRUSS SPAN: 27'-6"





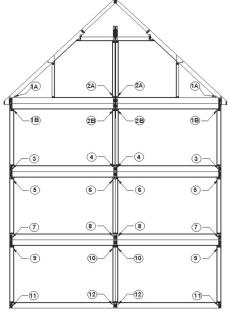
						_					
CONDITION "D" - OUTER	KNEE WALL	S:	CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS	
820	SNOW	1.15	NO GOOD	N/A	N/A	OK	8	16	OK	8	
COMPRESSION (lbs)	CASE	CD			-						
572	SNOW	1.15	USE (5) 16 d NAILS TH	ROUGH CHC	RD BLOCK						
CONDITION "E" - INNER I	KNEE WALLS	S:	CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS	
0	SNOW	1.15	ОК	2	2	OK	2	2	OK	2	
CONDITION "F" - HEEL:											
TOP CHORD (lbs)	CASE	CD									
972	SNOW	1.15	USE (1) 1/2" BOLT (DO	UBLE SHEAF	R; 3/8" SIDE PLA	TES)					
			PLUS (3) 6 d NAILS OR (4) 16 ga STAPLES PER GUSSET EACH SIDE								
		ALTERNATE:	USE (1) 3/4" BOLT (DOUBLE SHEAR; 1/2" SIDE PLATES)								
			PLUS NO ADDITIONAL	<b>FASTENERS</b>	REQUIRED						
BOTTOM CHORD (lbs)	CASE	CD									
786	SNOW	1.15	USE (8) 6 d NAILS OR (	(10) 16 ga ST	APLES PER GU	SSET EACH SIDE					
CONDITION "G" - BOTTO	M CHORD AT	MATING LINE:									
			CHECK STRAP	QTY/END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS	
786	SNOW	1.15	NO GOOD	N/A	N/A	OK	8	15	OK	8	
		ALTERNATE:	USE (10) 16 d NAILS TI	ROUGH DE	CKING EACH SI	DE			•		

### **COMPONENT LOAD SUMMARY**

EXTERIOR WALL DEAD LOAD =	12	psf x	10	ft =	120 plf
MATING WALL DEAD LOAD =	8	psf x	10	ft =	80 plf
FLOOR DEAD LOAD =	10	psf x	13.75	ft / 2 =	68.75 plf
FLOOR LIVE LOAD =	40	psf x	13.75	ft / 2 =	275 plf
CEILING DEAD LOAD =	5	psf x	13.75	ft / 2 =	34.38 plf

LOCATION 1 = EXT. WALL HEADER & EXT. WALL STUD
LOCATION 2 = M. WALL HEADER & M. WALL STUD
LOCATION 3 = PERIMETER BAND
LOCATION 4 = CENTER GIRDER
LOCATION 5 = EXT. WALL HEADER & EXT. WALL STUD
LOCATION 6 = M. WALL HEADER & M. WALL STUD
LOCATION 7 = PERIMETER BAND
LOCATION 8 = CENTER GIRDER
LOCATION 9 = EXT. WALL HEADER & EXT. WALL STUD
LOCATION 10 = M. WALL HEADER & M. WALL STUD
LOCATION 11 = PERIMETER BAND
LOCATION 12 = CENTER GIRDER
LOCATIONS 3, 4, 7, 8, 11 & 12 MAY BE USED TO GENERATE
FOUNDATION LOADS

\* CROSS SECTION IS FOR REFERENCE ONLY AND MAY NOT REFLECT ACTUAL TRUSS



### TRUSS 4BOX-CAPE-27-6, 12/12 PITCH, 27'-6" WIDTH

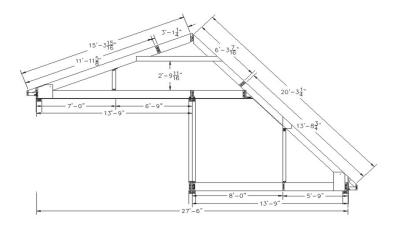
### COMPONENT LOADS (lbs/ft)

20 nof	GROUND	CNION	

	30 psi GROUND 3NOW			(IVIATING	WALL LO	ADS ANE	FER SIDE	OF LINE)							
	LOCATION	1A	1B	2A	2B	3	4	5	6	7	8	9	10	11	12
	DEAD LOAD	357	391	58	92	546	207	580	241	769	390	803	424	992	573
	LIVE LOAD	618	652	428	462	893	703	893	703	1168	978	1168	978	1443	1253
ı	TOTAL LOAD	975	1044	486	555	1439	910	1473	944	1937	1368	1971	1402	2435	1826

C & C UPLIFT														
LOCATION	1A	1B	2A	2B	3	4	5	6	7	8	9	10	11	12
UPLIFT (0.6) DEAD LOAD	214	235	35	55	328	124	348	145	461	234	482	254	595	344
110 mph UPLIFT	-268	-33	0	-	-	-	-	-	-	-	-	-	-	-





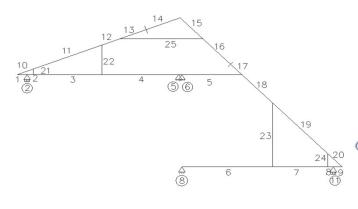
TRUSS NO.: VSHED-27-7 TRUSS CENTERS:

**APPLIED MWFRS UPLIFT:** 32.76 psf WINDWARD AT 110 mph

22.80 psf LEEWARD AT 110 mph

16 in O.C.

APPLIED C & C UPLIFT: 46.65 psf AT 110 mph



LOW (12/12) SIDE

\* BALANCED SNOW LOAD: 17.76 psf
UNBALANCED SNOW LOAD: 47.51 psf
OPPOSITE SIDE UNB. SNOW LOAD: 5.33 psf
UNBALANCED SNOW LOAD LENGTH: 4.43 ft

APPLIED MWFRS UPLIFT: 33.61 psf WINDWARD AT 110 mph

19.09 psf LEEWARD AT 110 mph

APPLIED C & C UPLIFT: 36.21 psf AT 110 mph

TC DL: 10 psf BC DL: 10 psf

**BC LL**: 10 psf WHERE h < 42" **BC LL**: 20 psf WHERE h ≧ 42"

LOWER BC LL: 40 psf BETWEEN KNEEWALLS

MEMBER INFORMATION:

	SIZE &
MEMBER	SPECIES
1 - 5 & 6 - 9	2 x 10 SPF #2
10 - 13 & 17 - 20	2 x 8 SPF #2
14 - 16	2 x 4 SPF #2
21 - 24	2 x 4 SPF #2
25	2 x 6 SPF #2

07710/1



	MAXIMUM SUPPORT REACTIONS	<u>S (lbs):</u>		MWFRS	C & C
			DL + LL +	0.6 DL +	0.6 DL +
		DEAD	30 psf	110 mph	110 mph
		LOAD	GSL	UPLIFT	UPLIFT
	HS EXT. WALL VERTICAL (1)	284	645	-263	-440
	MATEWALL VERTICAL (5)	154	363	-140	-206
	MATEWALL VERTICAL (6)	42	77	0	0
LS	MATEWALL. WALL VERTICAL (8)	81	303	0	0
	LS EXT. WALL VERTICAL(11)	529	1324	-338	-442
	·				

NOTES: 1. RIDGE BEAM REACTIONS ARE <u>TOTAL</u> FOR BOTH SIDES.

- 2. WIND PER ASCE 7-05, 110 mph (Vult), EXP. C.
- 3. SNOW PER ASCE 7-05, 30 psf GSL, Ct = 1.1, Ce = 1.0
  DRIFTING LENGTH IS LATERAL DISTANCE FROM RIDGE.
- 4. COMPONENT DESIGN IS BASED ON C & C PRESSURES
  TRUSS UPLIFT CONNECTIONS ARE BASED ON MWFRS PRESSURES.

<u>MUMIXA</u>	INTERAC	TION &	DEFLECTION	ON:

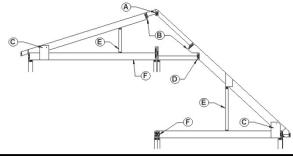
	HIGH SIDE	MAXIMUM		LOW SIDE	MAXIMUM	
	MAXIMUM	DEFLECTION		MAXIMUM	DEFLECTION	
	CSI	(in)	l /	CSI	(in)	l /
BOTTOM CHORD	0.970	0.385	609	0.404	0.121	1405
TOP CHORD	0.506	0.852	217	0.882	0.296	821
WEB	0.204	0.00	****	N/A	N/A	N/A
					BARLOW ENGIN	JEERING P.C.



### TRUSS CONNECTIONS

PROJECT NUMBER: 170367
TRUSS NUMBER: VSHED-27-7
TRUSS PITCH: 4.5/12 & 12/12

TRUSS SPAN: 27'-7"



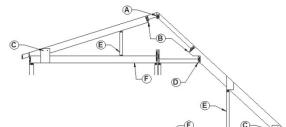
### UPLIFT CONNECTIONS (MWFRS LOADS):

110 mph

HIGH SIDE EXTERIOR WA	<b>LL</b>		CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END
UPLIFT (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
263	WIND	1.6	OK	4	5	OK	2	5	OK	2
	ALTERNATE:	(3) 16 d NAIL	S TOENAILED THROUG	H BC INTO B	AND PLUS (2) 16	d NAILS THROUGH SH	EATHING IN	TO BAND AND S	TUD	
LOW SIDE EXTERIOR WA	LL		CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END
UPLIFT (lbs / PER SIDE)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
338	WIND	1.6	OK	4	7	OK	3	7	OK	2
	ALTERNATE:	(4) 16 d NAIL	S TOENAILED THROUG	H BC INTO B	AND PLUS (3) 16	d NAILS THROUGH SH	EATHING IN	TO BAND AND S	TUD	
HIGH SIDE MATING WALL	-		CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END
UPLIFT (lbs / PER SIDE)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
140	WIND	1.6	OK	2	3	OK	2	3	OK	2
	ALTERNATE:	(2) 16 d NAIL	S TOENAILED THROUG	H BC INTO B	AND PLUS (2) 16	d NAILS THROUGH SH	EATHING IN	TO BAND AND S	TUD	

### TRUSS CONNECTIONS

PROJECT NUMBER: 170367
TRUSS NUMBER: VSHED-27-7
TRUSS PITCH: 4.5/12 & 12/12
TRUSS SPAN: 27'-7"





						_	E)	C		
MAXIMUM OF DL + LL +	30 psf GSL &	0.6 DL + 110 n	nph WIND							
CONDITION "A" - RIDGE:			CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	T QTY / ENI
	CASE									
TENSION (lbs)		CD	1 1/2" x 26ga STRAP		"	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE		10 d NAILS
78	WIND	1.6	OK	2	2	OK	2	2	OK	2
			: USE (2) 8 d NAILS EAC	H END OF 1 x	( 4					
SHEAR (lbs)	CASE	CD	1							
104	SNOW	1.15	USE (2) 16 d NAILS INT	O END GRAII	N EACH END PL	US USE 10 d NAILS AT	17 in O.C. TH	ROUGH PLATES	<u> </u>	
CONDITION "B" - TOP CI			1							
TENSION (lbs)	CASE	CD								
341	WIND	1.6	USE (5) 6 d NAILS THR							
	ALTERNATE	1	USE (8) 16 ga STAPLE	THROUGH SI	HEATHING EACH	H SIDE				
SHEAR (lbs)	CASE	CD								
104	SNOW	1.15	USE (2) 16 d NAILS TO	ENAILED EAC	CH END PLUS US	SE 10 d NAILS AT 17 in 0	D.C. THROUG	SH PLATES		
CONDITION "C" - HEEL:										
TOP CHORD (lbs)	CASE	CD								
992	SNOW	1.15	USE (1) 1/2" BOLT (DO	UBLE SHEAR	; 3/8" SIDE PLAT	ES)				
			PLUS (3) 6 d NAILS OR	(4) 16 ga STA	APLES PER GUS	SET EACH SIDE				
		ALTERNATE:	USE (1) 5/8" BOLT (DO	., .						
			PLUS NO ADDITIONAL	FASTENERS	REQUIRED					
BOTTOM CHORD (lbs)	CASE	CD								
781	SNOW	1.15	USE (8) 6 d NAILS OR (	(10) 16 ga STA	APLES PER GUS	SET EACH SIDE				
CONDITION "D" - COLLA	R TIE:									
AXIAL (lbs)	CASE	CD								
511	SNOW	1.15	USE (4) 16 d NAILS TH	ROUGH TIE II	NTO RAFTER					
CONDITION "E" - KNEE	WALL:									
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
470	WIND	1.6	OK	6	9	OK	4	9	OK	4
COMPRESSION (lbs)	CASE	CD								
597	SNOW	1.15	USE (5) 16 d NAILS TH	ROUGH CHO	RD BLOCK					
CONDITION "F" - BOTTO	M CHORD AT	MATING LINE	<b>.</b>							
SHEAR (lbs)	CASE	CD	SIMPSON A34							
363	SNOW	1.15	OK							
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
781	SNOW	1.15	NO GOOD	N/A	N/A	OK	8	15	OK	5

### **COMPONENT LOAD SUMMARY**

EXTERIOR WALL DEAD LOAD = 12 psf x 10 ft = 120 plf

MATING WALL DEAD LOAD = 8 psf x 10 ft = 80 plf

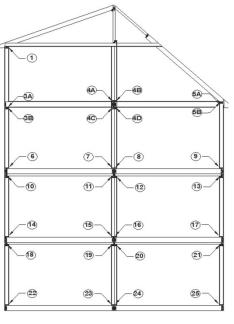
FLOOR DEAD LOAD = 10 psf x 13.75 ft / 2 69 plf

FLOOR LIVE LOAD = 40 psf x 13.75 ft / 2 275 plf

CEILING DEAD LOAD = 5 psf x 13.75 ft / 2 34 plf

LOCATION 14 = PERIMETER BAND
LOCATION 15 = CENTER GIRDER
LOCATION 16 = CENTER GIRDER
LOCATION 17 = PERIMETER BAND
LOCATION 18 = EXT. WALL HEADER & EXT. WALL STUD
LOCATION 19 = M. WALL HEADER & M. WALL STUD
LOCATION 20 = M. WALL HEADER & M. WALL STUD
LOCATION 21 = EXT. WALL HEADER & EXT. WALL STUD
LOCATION 22 = PERIMETER BAND
LOCATION 23 = CENTER GIRDER
LOCATION 24 = CENTER GIRDER
LOCATION 25 = PERIMETER BAND

# \* CROSS SECTION IS FOR REFERENCE ONLY AND MAY NOT REFLECT ACTUAL TRUSS



17

473

18

882

1096

1978

19

585

879

### TRUSS VSHED-27-7, 4.5/12 PITCH, 27'-7" WIDTH

### **COMPONENT LOADS (lbs/ft)**

30 psf GROUND SNOW (RIDGE BEAM LOADS ARE TOTAL FOR BOTH SIDES OF LINE, MATING WALL LOADS ARE PER SIDE OF LINE)

30 psi GROUND SNOW					(17)	IDGE B	EAW L	JADS A	INE TO	TAL FO	IN BOT	H SIDE	3 OF L	IIN⊏, IVIÆ	ATTING V	VALLL	UADS I	ANEFE	K SIDE	OF LIN	1
LOCATION	1	3A	3B	4A	4B	4C	4D	5A	5B	6	7	8	9	10	11	12	13	14	15	16	ĺ
DEAD LOAD	213	436	470	219	172	253	206	61	95	625	368	321	250	659	402	355	284	848	551	504	ı
LIVE LOAD	271	546	580	329	285	363	319	167	201	821	604	560	442	821	604	560	442	1096	879	835	ĺ
TOTAL LOAD	484	982	1050	548	458	616	526	228	296	1446	972	881	692	1480	1006	915	726	1944	1430	1339	ĺ
LOCATION	22	23	24	25																	
DEAD LOAD	1071	734	687	696																	
LIVE LOAD	1371	1154	1110	992																	

### C & C UPLIFT

TOTAL LOAD

LOCATION	1	3A	3B	4A	4B	4C	4D	5A	5B	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
UPLIFT (0.6) DEAD LOAD	128	262	282	131	103	152	124	37	57	375	221	193	150	395	241	213	170	509	331	302	284	529	351	323	304
110 mph UPLIFT	-330	-196	-176	-9	0	0	0	-332	-312	-83	-	-	-219	-63	-	-	-199	-	-	-	-	-	-	-	-154
LOCATION	22	23	2/	25																					

UPLIFT (0.6) DEAD LOAD 643 440 412 418

110 mph UPLIFT - - - - -40

2442 1888 1797 1688



21

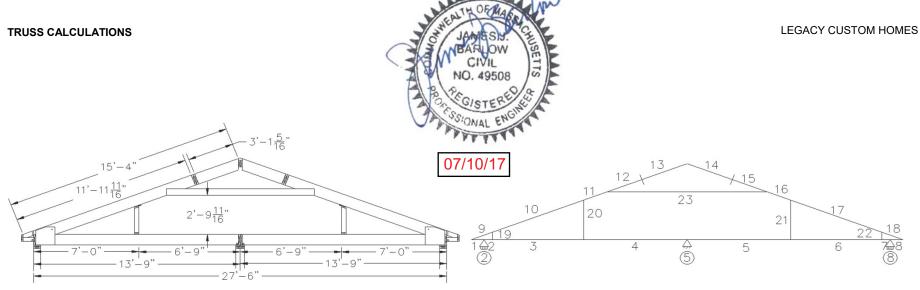
1224

20

538 507

835 717

1464 | 1373



**GROUND SNOW LOAD:** 30 psf TC DL: 10 psf \* BALANCED SNOW LOAD: 23.1 psf BC DL: 10 psf

UNBALANCED SNOW LOAD: 41.289 psf BC LL: 10 psf WHERE h < 42" 10 psf WHERE h ≥ 42" OPPOSITE SIDE UNB. SNOW LOAD: 6.93 psf BC LL: **UNBALANCED SNOW LOAD LENGTH:** 

7.27 ft BC LL: 20 psf BETWEEN KNEEWALLS

APPLIED MWFRS UPLIFT: 32.77 psf WINDWARD AT 110 mph 22.81 psf LEEWARD AT 110 mph

APPLIED C & C UPLIFT: 32.77 psf AT 110 mph

TRUSS NO.: TR4.5-27-6

**JOB NO.:** 170367 **PITCH:** 4.5/12

**SPAN**: 27'-6"

TRUSS CENTERS: 16 in O.C.

### MEMBER INFORMATION:

	SIZE &
MEMBER	SPECIES
1 - 8	2 x 10 SPF #2
9 - 12 & 15 - 18	2 x 10 SPF #2
13 & 14	2 x 6 SPF #2
19 - 22	2 x 4 SPF #2
23	2 x 6 SPF #2

**NOTES:** 1. MATING WALL REACTIONS ARE <u>TOTAL</u> FOR BOTH SIDES.

- 2. WIND PER ASCE 7-05, 110 mph, EXP. C.
- 3. SNOW PER ASCE 7-05, 30 psf GSL, Ct = 1.1, Ce = 1.0 DRIFTING LENGTH IS LATERAL DISTANCE FROM RIDGE.
- 4. COMPONENT DESIGN IS BASED ON C & C PRESSURES TRUSS UPLIFT CONNECTIONS ARE BASED ON MWFRS PRESSURES.
- 5. MEMBER 23 IS BRACED AT MIDPOINT



MAXIMUM SUPPORT REA	IAXIMUM SUPPORT REACTIONS (lbs):								
		DL + LL +	0.6 DL +	0.6 DL +					
	DEAD	30 psf	110 mph	110 mph					
	LOAD	GSL	UPLIFT	UPLIFT					
EXTERIOR WALL	413	900	-303	-350					
MATING WALL	132	458	0	0					

### **MAXIMUM INTERACTION & DEFLECTION:**

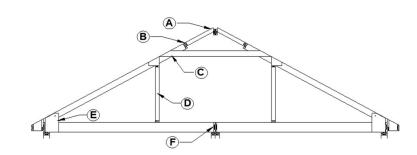
		MAXIMUM	
	MAXIMUM	DEFLECTION	
	CSI	(in)	l /
BOTTOM CHORD	0.584	0.182	948
TOP CHORD	0.212	0.362	510
WEB	0.360	0.00	****



### TRUSS CONNECTIONS

PROJECT NUMBER: 170367
TRUSS NUMBER: TR4.5-27-6
TRUSS PITCH: 4.5/12

TRUSS SPAN: 27'-6"



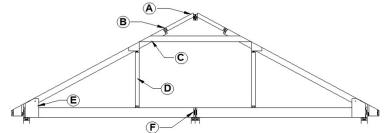
### **UPLIFT CONNECTIONS (MWFRS LOADS):**

110 mph										
EXTERIOR WALL			CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END
UPLIFT (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
303	WIND	1.6	OK	2	3	OK	2	3	ОК	3
Ā	ALTERNATE:	(4) 16 d NAIL	S TOENAILED THROUG	SH BC INTO E	BAND PLUS (3) 1	6 d NAILS THROUGH S	HEATHING II	NTO BAND AND	STUD	
MATING WALL			CHECK STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / END
UPLIFT (lbs / PER SIDE)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAILS
0	WIND	1.6	NO CONN REQ'D	N/A	N/A	NO CONN REQ'D	N/A	N/A	NO CONN REQ'D	N/A
ļ ,	ALTERNATE:	NO CONN RE	EQ'D					•		

### TRUSS CONNECTIONS

PROJECT NUMBER: 170367
TRUSS NUMBER: TR4.5-27-6
TRUSS PITCH: 4.5/12

TRUSS SPAN : 27'-6"





					<u> </u>										
MAXIMUM OF DL + LL + 3	0 psf GSL &	0.6 DL + 110 ı	mph WIND												
				,		Ī									
CONDITION "A" - RIDGE:			CHECK STRAP	QTY / END		CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / EN					
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	- 3	1 1/2" x 20 ga STRAP		16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAIL					
150	WIND	1.6	OK	2	2	OK	2	2	OK	2					
			USE (2) 8 d NAILS EAC	H END OF 1	x 4										
SHEAR (lbs)	CASE	CD													
105	SNOW	1.15	USE (2) 16 d NAILS IN	TO END GRAI	IN EACH END P	LUS USE 10 d NAILS AT	17 in O.C. TI	HROUGH PLATE	S						
CONDITION "B" - TOP CH															
TENSION (lbs)	CASE	CD													
140	WIND		USE (2) 6 d NAILS THE												
			: USE (4) 16 ga STAPLE	THROUGH S	HEATHING EAC	CH SIDE									
SHEAR (lbs)	CASE	CD													
105	SNOW	1.15	USE (2) 16 d NAILS TO	ENAILED EA	CH END PLUS L	JSE 10 d NAILS AT 17 in	O.C. THROL	JGH PLATES							
CONDITION "C" - COLLA															
AXIAL (lbs)	CASE	CD													
1099	SNOW	1.15	USE (8) 16 d NAILS EA	CH END											
CONDITION "D" - KNEE V	VALLS:		CHECK STRAP												
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS20 STRAP	10 d NAIL					
290	SNOW	1.15	ОК	3	3	OK	2	3	OK	3					
COMPRESSION (lbs)	CASE	CD													
244	SNOW	1.15	USE (2) 16 d NAILS TH	ROUGH CHC	RD BLOCK										
CONDITION "E" - HEEL:															
TOP CHORD (lbs)	CASE	CD													
1368	SNOW	1.15	USE (1) 1/2" BOLT (DO	UBLE SHEAF	R; 3/8" SIDE PLA	TES)									
			PLUS (7) 6 d NAILS OF	<u> </u>											
			USE (1) 3/4" BOLT (DO			E PLATES)									
	1	,	PLUS NO ADDITIONAL	FASTENERS	REQUIRED										
BOTTOM CHORD (lbs)	CASE	CD													
1293	SNOW	1.15	USE (12) 6 d NAILS OF	R (16) 16 ga S	TAPLES PER GI	JSSET EACH SIDE									
CONDITION "F" - BOTTO	M CHORD AT	MATING LIN		,		<u> </u>									
		1	CHECK STRAP	QTY / END		CHECK ALT. STRAP	QTY / END	QTY / END	CHECK ALT. STRAP	QTY / EN					
TENSION (lbs)	CASE	CD	1 1/2" x 26ga STRAP	10 d NAILS	16 ga STAPLE	1 1/2" x 20 ga STRAP	10 d NAILS	16 ga STAPLE	SIMPSON CS14 STRAP	10 d NAIL					
1293	SNOW	1.15	NO GOOD	N/A	N/A	NO GOOD	N/A	N/A	OK	11					
		ALTERNATE:	: USE (10) 16 d NAILS T	HROUGH DE	CKING EACH SI	DE									

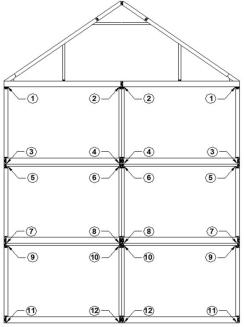
LEGACY CUSTOM HOMES TRUSS CALCULATIONS

### **COMPONENT LOAD SUMMARY**

EXTERIOR WALL DEAD LOAD =	12	psf x	10	ft =	120 plf
MATING WALL DEAD LOAD =	8	psf x	10	ft =	80 plf
FLOOR DEAD LOAD =	10	psf x	13.75	ft / 2 =	68.75 plf
FLOOR LIVE LOAD =	40	psf x	13.75	ft / 2 =	275 plf
CEILING DEAD LOAD =	5	psf x	13.75	ft / 2 =	34.38 plf

LOCATION 1 = EXT. WALL HEADER & EXT. WALL STUD
LOCATION 2 = M. WALL HEADER & M. WALL STUD
LOCATION 3 = PERIMETER BAND
LOCATION 4 = CENTER GIRDER
LOCATION 5 = EXT. WALL HEADER & EXT. WALL STUD
LOCATION 6 = M. WALL HEADER & M. WALL STUD
LOCATION 7 = PERIMETER BAND
LOCATION 8 = CENTER GIRDER
LOCATION 9 = EXT. WALL HEADER & EXT. WALL STUD
LOCATION 10 = M. WALL HEADER & M. WALL STUD
LOCATION 11 = PERIMETER BAND
LOCATION 12 = CENTER GIRDER
LOCATIONS 3, 4, 7, 8, 11 & 12 MAY BE USED TO GENERATE
FOUNDATION LOADS

### \* CROSS SECTION IS FOR REFERENCE ONLY AND MAY NOT REFLECT ACTUAL TRUSS



### TRUSS TR4.5-27-6, 4.5/12 PITCH, 27'-6" WIDTH

### COMPONENT LOADS (lbs/ft)

### 30 nsf GROUND SNOW

30 psf GROUND SNOW	0 psf GROUND SNOW (MATING WALL LOADS ARE PER SIDE OF LINE)														
LOCATION	1	2	3	4	5	6	7	8	9	10	11	12			
DEAD LOAD	310	50	499	199	533	233	722	382	756	416	945	565			
LIVE LOAD	365	122	640	397	640	397	915	672	915	672	1190	947			
TOTAL LOAD	675	172	1139	596	1173	630	1637	1054	1671	1088	2135	1512			

C & C UPLIFT	% C UPLIFT														
LOCATION	1	2	3	4	5	6	7	8	9	10	11	12			
UPLIFT (0.6) DEAD LOAD	186	30	299	119	320	140	433	229	454	250	567	339			
110 mph UPLIFT	-263	0	-150	-	-129	1	-16	-	-	-	-	-			



### UNIFORMLY LOADED **BEAM CHARTS**

### SITTING ROOM BEAM

### NOTES:

- 1. LOADS ARE UNIFORM ALONG BEAM LENGTH.
- 2. DEFLECTION LIMITS: L/240
- 4. MULTIPLE PLIES ARE TO BE FASTENED PER MANFACTURER / CODE REQUIREMENTS.
- 5. DESIGNER TO ACCOUNT FOR REQUIRED BEARING AREA & SUPPORT STUDS.
- 3. BEAMS ARE ASSUMED TO BE LATERALLY BRACED. 6. SPANS ARE LIMITED BY THE MAXIMUM SPAN DUE TO BENDING, DEFLECTION, OR SHEAR.
- 7. SPLITS LIMITED TO 3/4 x DEPTH IN SOLID SAWN LUMBER.
- 8. DURATION FACTOR (Cd) = 1.15 & REPETITIVE FACTOR (Cr) = 1.0.
- 9. "-" DENOTES SPAN GREATER THAN 30'-0".
- 10. SINGLE MEMBER LVL'S GREATER THAN 14" DEEP ARE NOT TO BE USED EXCEPT FOR MATING WALL LOCATIONS WHERE ONE EACH SIDE ARE FASTENED TOGETHER TO FORM A DOUBLE MEMBER

### **UNIFORMLY LOADED BEAM (I/240) SPAN CALCULATION**

			MAXIMUM	LIMITED	REQ'D												
MEMBER	LOAD (plf)	QUANTITY	SPAN	BY	BEARING (in <sup>2</sup> )	QUANTITY	SPAN	BY	BEARING (in <sup>2</sup> )	QUANTITY	SPAN	BY	BEARING (in <sup>2</sup> )	QUANTITY	SPAN	BY	BEARING (in <sup>2</sup> )
2 x 4 SPF #2	250	1	3 ' - 6"	Lb	1.033	2	4 ' - 11"	Lb	1.46	3	5 ' - 10"	Ld	1.72	4	6 ' - 5"	Ld	1.893
2 x 6 SPF #2	250	1	5 ' - 1"	Lb	1.508	2	7 ' - 3"	Lb	2.133	3	8 ' - 10"	Lb	2.612	4	10 ' - 1"	Ld	2.975
2 x 8 SPF #2	250	1	6 ' - 6"	Lb	1.913	2	9 ' - 2"	Lb	2.706	3	11 ' - 3"	Lb	3.314	4	13 ' - 0"	Lb	3.826
2 x 10 SPF #2	250	1	7 ' - 11"	Lb	2.337	2	11 ' - 2"	Lb	3.305	3	13 ' - 9"	Lb	4.048	4	15 ' - 10"	Lb	4.674
2 x 12 SPF #2	250	1	9 ' - 2"	Lb	2.71	2	13 ' - 0"	Lb	3.833	3	15 ' - 11"	Lb	4.694	4	18 ' - 5"	Lb	5.42
1.5 x 5.5 LVL	250	1	7 ' - 2"	Ld	1.019	2	9 ' - 0"	Ld	1.284	3	10 ' - 4"	Ld	1.47	4	11 ' - 4"	Ld	1.618
1.5 x 7.25 LVL	250	1	9 ' - 5"	Ld	1.344	2	11 ' - 11"	Ld	1.693	3	13 ' - 7"	Ld	1.938	4	15 ' - 0"	Ld	2.133
1.5 x 9.25 LVL	250	1	12 ' - 0"	Ld	1.715	2	15 ' - 2"	Ld	2.16	3	17 ' - 4"	Ld	2.473	4	19 ' - 1"	Ld	2.722
1.5 x 11.25 LVL	250	1	14 ' - 8"	Ld	2.085	2	18 ' - 5"	Ld	2.627	3	21 ' - 2"	Ld	3.008	4	23 ' - 3"	Ld	3.31
1.5 x 12 LVL	250	1	15 ' - 7"	Ld	2.224	2	19 ' - 8"	Ld	2.803	3	22 ' - 7"	Ld	3.208	4	24 ' - 10"	Ld	3.531
1.5 x 14 LVL	250	1	18 ' - 3"	Ld	2.595	2	23 ' - 0"	Ld	3.27	3	26 ' - 4"	Ld	3.743	4	29 ' - 0"	Ld	4.119
1.5 x 16 LVL	250	1	20 ' - 10"	Ld	2.966	2	26 ' - 3"	Ld	3.737	-	-	-	-	-	-	-	-
1.5 x 18 LVL	250	1	23 ' - 5"	Ld	3.337	2	29 ' - 7"	Ld	4.204	-	-	-	-	-	-	-	-
1.5 x 20 LVL	250	1	26 ' - 1"	Ld	3.707	-	-	-	-	-	-	-	-	-	-	-	-
1.5 x 24 LVL	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
2 x 4 SPF #2	300	1	3 ' - 2"	Lb	1.131	2	4 ' - 6"	Lb	1.6	3	5 ' - 6"	Ld	1.943	4	6 ' - 0"	Ld	2.138
2 x 6 SPF #2	300	1	4 ' - 8"	Lb	1.652	2	6 ' - 7"	Lb	2.336	3	8 ' - 1"	Lb	2.861	4	9 ' - 4"	Lb	3.304
2 x 8 SPF #2	300	1	5 ' - 11"	Lb	2.096	2	8 ' - 4"	Lb	2.964	3	10 ' - 3"	Lb	3.63	4	11 ' - 10"	Lb	4.192
2 x 10 SPF #2	300	1	7 ' - 3"	Lb	2.56	2	10 ' - 3"	Lb	3.621	3	12 ' - 6"	Lb	4.434	4	14 ' - 6"	Lb	5.12
2 x 12 SPF #2	300	1	8 ' - 4"	Lb	2.969	2	11 ' - 10"	Lb	4.198	3	14 ' - 6"	Lb	5.142	4	16 ' - 9"	Lb	5.938
1.5 x 5.5 LVL	300	1	6 ' - 9"	Ld	1.151	2	8 ' - 6"	Ld	1.45	3	9 ' - 8"	Ld	1.66	4	10 ' - 8"	Ld	1.828
1.5 x 7.25 LVL	300	1	8 ' - 10"	Ld	1.518	2	11 ' - 2"	Ld	1.912	3	12 ' - 10"	Ld	2.189	4	14 ' - 1"	Ld	2.409
1.5 x 9.25 LVL	300	1	11 ' - 4"	Ld	1.936	2	14 ' - 3"	Ld	2.439	3	16 ' - 4"	Ld	2.793	4	18 ' - 0"	Ld	3.074
1.5 x 11.25 LVL	300	1	13 ' - 9"	Ld	2.355	2	17 ' - 4"	Ld	2.967	3	19 ' - 11"	Ld	3.396	4	21 ' - 11"	Ld	3.738
1.5 x 12 LVL	300	1	14 ' - 8"	Ld	2.512	2	18 ' - 6"	Ld	3.165	3	21 ' - 3"	Ld	3.623	4	23 ' - 4"	Ld	3.987
1.5 x 14 LVL	300	1	17 ' - 2"	Ld	2.93	2	21 ' - 7"	Ld	3.692	3	24 ' - 9"	Ld	4.226	4	27 ' - 3"	Ld	4.652
1.5 x 16 LVL	300	1	19 ' - 7"	Lb	3.34	2	24 ' - 9"	Ld	4.22	3	28 ' - 4"	Ld	4.83	-	-	-	-
1.5 x 18 LVL	300	1	21 ' - 11"	Lb	3.742	2	27 ' - 10"	Ld	4.747	-	-	-	-	-	-	-	-
1.5 x 20 LVL	300	1	24 ' - 3"	Lb	4.144	-	-	-	-	-	-	-	-	-	-	-	-
1.5 x 24 LVL	300	1	29 ' - 0"	Lb	4.944	-	-	-	-	-	-	-	-	-	-	-	-

