EXISTING GRADE, INC.

Land Surveyors - Civil Engineers

Storm Water Drainage Report for Wildwood Lane- Lot 61 Bourne, Massachusetts

Prepared for:

Ocean Dunes, LLC 498 Newtown Road Littleton, Massachusetts 01460

Prepared by:

Existing Grade, Inc. 62 Riedell Road Douglas, Massachusetts 01516

> January 03, 2024 EGI Project No. 1292



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Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.





A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals. This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



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Checklist for Stormwater Report

B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

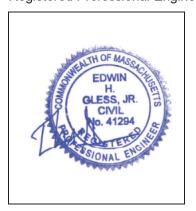
Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



Edwin Glass 01/03/2024
Signature and Date

Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?		
New development New development		
Redevelopment		
☐ Mix of New Development and Redevelopment		



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Checklist for Stormwater Report

Checklist (continued)

LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

	No disturbance to any Wetland Resource Areas		
\boxtimes	Site Design Practices (e.g. clustered development, reduced frontage setbacks)		
	Reduced Impervious Area (Redevelopment Only)		
	Minimizing disturbance to existing trees and shrubs		
	LID Site Design Credit Requested:		
	☐ Credit 1		
	☐ Credit 2		
	☐ Credit 3		
	Use of "country drainage" versus curb and gutter conveyance and pipe		
	Bioretention Cells (includes Rain Gardens)		
	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)		
	Treebox Filter		
	Water Quality Swale		
	Grass Channel		
	Green Roof		
	Other (describe):		
Sta	ndard 1: No New Untreated Discharges		
\boxtimes	No new untreated discharges		
	Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth		
\boxtimes	Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.		



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Checklist for Stormwater Report

Cł	Checklist (continued)			
Sta	andard 2: Peak Rate	Attenuation		
	Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding. Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.			
	development rates for flooding increases du	r the 2-year and 10-year 24-hor ring the 100-year 24-hour storr	at peak discharge rates do not exceed pre- cur storms. If evaluation shows that off-site n, calculations are also provided to show that ed pre-development rates for the 100-year 24-	
Sta	andard 3: Recharge			
\boxtimes	Soil Analysis provided	d.		
\boxtimes	Required Recharge Volume calculation provided.			
	Required Recharge v	olume reduced through use of	the LID site Design Credits.	
\boxtimes	Sizing the infiltration,	BMPs is based on the following	g method: Check the method used.	
	⊠ Static □	☐ Simple Dynamic	☐ Dynamic Field ¹	
	Runoff from all imper	vious areas at the site discharg	ing to the infiltration BMP.	
	Runoff from all impervious areas at the site is <i>not</i> discharging to the infiltration BMP and calculation are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.			
\boxtimes	Recharge BMPs have	e been sized to infiltrate the Re	quired Recharge Volume.	
	Recharge BMPs have been sized to infiltrate the Required Recharge Volume <i>only</i> to the maximum extent practicable for the following reason:			
	☐ Site is comprised solely of C and D soils and/or bedrock at the land surface			
	☐ M.G.L. c. 21E site	es pursuant to 310 CMR 40.000	00	
	☐ Solid Waste Landfill pursuant to 310 CMR 19.000			
	Project is otherwise practicable.	se subject to Stormwater Mana	gement Standards only to the maximum extent	
\boxtimes	Calculations showing	that the infiltration BMPs will d	rain in 72 hours are provided.	
	Property includes a M	I.G.L. c. 21E site or a solid was	te landfill and a mounding analysis is included.	

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



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Checklist for Stormwater Report

CI	necklist (continued)
Sta	andard 3: Recharge (continued)
	The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10-year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
	Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.
Sta	andard 4: Water Quality
The	e Long-Term Pollution Prevention Plan typically includes the following: Good housekeeping practices; Provisions for storing materials and waste products inside or under cover; Vehicle washing controls; Requirements for routine inspections and maintenance of stormwater BMPs; Spill prevention and response plans; Provisions for maintenance of lawns, gardens, and other landscaped areas; Requirements for storage and use of fertilizers, herbicides, and pesticides; Pet waste management provisions; Provisions for operation and management of septic systems; Provisions for solid waste management; Snow disposal and plowing plans relative to Wetland Resource Areas; Winter Road Salt and/or Sand Use and Storage restrictions; Street sweeping schedules; Provisions for prevention of illicit discharges to the stormwater management system; Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL; Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan; List of Emergency contacts for implementing Long-Term Pollution Prevention Plan. A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent. Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge: is within the Zone II or Interim Wellhead Protection Area
	is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)

involves runoff from land uses with higher potential pollutant loads.

applicable, the 44% TSS removal pretreatment requirement, are provided.

☐ The Required Water Quality Volume is reduced through use of the LID site Design Credits.

Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if



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Checklist for Stormwater Report

Cł	necklist (continued)
Sta	andard 4: Water Quality (continued)
\boxtimes	The BMP is sized (and calculations provided) based on:
	☐ The ½" or 1" Water Quality Volume or
	☐ The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
	The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
	A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.
Sta	ndard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)
	The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report. The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted <i>prioto</i> to the discharge of stormwater to the post-construction stormwater BMPs.
	The NPDES Multi-Sector General Permit does <i>not</i> cover the land use.
	LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
	All exposure has been eliminated.
	All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list.
	The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.
Sta	andard 6: Critical Areas
	The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
	Critical areas and BMPs are identified in the Stormwater Report.



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Checklist for Stormwater Report

Checklist (continued)

	andard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum tent practicable
Ш	The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:
	☐ Limited Project
	 Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area. Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area Marina and/or boatyard provided the hull painting, service and maintenance areas are protected
	from exposure to rain, snow, snow melt and runoff
	☐ Bike Path and/or Foot Path
	Redevelopment Project
	Redevelopment portion of mix of new and redevelopment.
	Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report. The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures:
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



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Checklist for Stormwater Report

Checklist (continued)

	andard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control ntinued)		
	The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has <i>not</i> been included in the Stormwater Report but will be submitted <i>before</i> land disturbance begins.		
	The project is <i>not</i> covered by a NPDES Construction General Permit.		
	The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.		
	The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.		
Sta	ndard 9: Operation and Maintenance Plan		
	The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:		
	Name of the stormwater management system owners;		
	☑ Party responsible for operation and maintenance;		
	Schedule for implementation of routine and non-routine maintenance tasks;		
	☐ Plan showing the location of all stormwater BMPs maintenance access areas;		
	☐ Description and delineation of public safety features;		
	☐ Estimated operation and maintenance budget; and		
	Operation and Maintenance Log Form.		
	The responsible party is <i>not</i> the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:		
	A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;		
	A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.		
Sta	ndard 10: Prohibition of Illicit Discharges		
	The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;		
	An Illicit Discharge Compliance Statement is attached;		
\boxtimes	NO Illicit Discharge Compliance Statement is attached but will be submitted <i>prior to</i> the discharge of any stormwater to post-construction BMPs.		

2. Introduction

Project Summary

The proposent, Ocean Dunes, LLC, proposes to construct 7 townhouse style buildings (Lot 61 on the proposed site plans) for the property located at 61 Wildwood Lane, Bourne MA. The proposed project will include the construction of 7 new multifamily style townhouse buildings, one new pass through parking lot consisting of: bituminous concrete surface, asphalt sloped curbing, storm water management infrastructures inclusive of catch basins, drain manholes, pipe conveyance systems, and drywells as shown on the design plans. All of the proposed buildings will be tied into a total of 6 proposed septic systems with connections to town water via new mains through the property. The proposed project will be conducted per the Massachusetts Department of Environmental Protection requirements, Local Town and State bylaws, as well as using best management practices.

The property is listed by the Town of Bourne Assessor's Department as Lot 62, Parcel 99 on Assessors Map 7 and historically laid within the Residential 20 (R-20) zoning district at the time of original permitting based upon a review of records on file at the Town of Bourne Planning and Zoning Offices. The property is located within the FEMA Flood Zone X Area (area outside mapped flood plain) based upon a review of FIRM Map 25001C0316K, Panel 316 of 550, last revised July 06, 2021. Currently there is municipal water as well as underground electric telephone/ cable to service the property.

The property's address is recorded as 61 Wildwood Lane, Bourne MA and abuts Ocean Pines Road to the West, Wildwood Lane to the South, and dedicated open space parcels and private residential properties to the North and East. Access to the site is via proposed pass through driveway along Wildwood Lane to the South and Ocean Pines Road to the West. The existing site is comprised a cleared storage lot which was permitted under the original historic site plan approval.

The Barnstable County Soil Survey, issued by the US Department of Agriculture was referenced to determine the type and hydrologic group of the soils located on the property. The property is comprised of mostly hydrologic soil group A type soils, as confirmed via numerous percolation and soil tests for the property.

Pre- and Post-Development Analysis

The pre- and post-development conditions were analyzed utilizing Hydrocad, a storm water modeling program, to model the hydrologic impacts of the proposed development on adjacent properties. The modeling program is based upon Soil Conservation Service's (SCS) Technical Release 55 (TR-55) and TR-20, programs to estimate the runoff and peak rates for small watersheds. As part of this analysis, two (2) separate models; one for the pre-development conditions, and one

for post-development conditions were created and three (3) points of comparison, or Design Points, were analyzed. The Design Points as well as the Watershed areas and associated time of concentration paths (Tc), are shown on the pre and post-development watershed plans, which are located in this report.

The pre- and post development conditions were analyzed for the 2, 10, 25 and 100-year Type III 24 hour storm events. The rainfall intensities used for each storm event were obtained from the latest NOAA Precipitation Frequency Data Server (PFDS) for the project location, and are shown in the table below.

Storm	Intensity (24-hr Duration
Event	(in)
2-year	3.41
10-year	4.98
25-year	5.95
100-year	7.46

The Barnstable County Soil Survey, issued by the US Department of Agriculture was referenced to determine the type and hydrologic group of the soils located on the property.

3. Compliance with Storm Water Management Standards

Standard 1: No New Untreated Discharges

The development is designed so that no new storm water conveyances do not discharge *untreated* pavement runoff into or cause erosion to wetland resource areas.

Standard 2: Peak Rate Attenuation

Pre- and Post Development storm water analysis calculations were performed for the 2, 10, 25 and 100-year Type III 24 hour storm events and a comparison of the peak rates at the design points for each storm event, under pre- and post-development conditions are summarized in the tables below:

	Design Point "Wildwood"	
Storm Event	Pre- Development	Post- Development
2-year	0.47 cfs	0.00 cfs
10-year	0.92 cfs	0.01 cfs
25-year	1.22 cfs	0.05 cfs
100-year	1.70 cfs	0.20 cfs

	Design Point "Northern Runoff"		
Storm Event	Pre- Development	Post- Development	
2-year	2.38 cfs	1.16 cfs	
10-year	5.02 cfs	1.79 cfs	
25-year	6.79 cfs	2.41 cfs	
100-year	9.66 cfs	3.19 cfs	

	Design Point "Ocean Pines"		
Storm	Pre-	Post-	
Event	Development	Development	
2-year	0.22 cfs	0.00 cfs	
10-year	0.75 cfs	0.00 cfs	
25-year	1.16 cfs	0.04 cfs	
100-year	1.86 cfs	0.16 cfs	

As shown in the tables above, the peak rates of storm water runoff generated under post-development conditions will be less than the peak rates generated under pre-development conditions and meet the requirements provided by the State of Massachusetts Stormwater Management Standards.

Complete runoff calculations for the 2, 10, 25 and 100-year Type III storm events including cover, soils types, area listings, and time of concentration paths for the pre-development conditions and post-development conditions are provided in Appendices A and B, respectively.

Standard 3: Groundwater Recharge

The groundwater recharge volume required for the development will be achieved through the proposed infiltration basin. Refer to Appendix C for all Groundwater Recharge Calculations and drywell sizing.

Standard 4: Water Quality

The storm water management system was designed with a treatment train consisting of street sweeping, deep sump catch basins, drywell pits, and cultec chambers to facilitate the required removal of 80% Total Suspended Solids (TSS) as shown in Appendix C.

Standard 5: Land Uses with higher Potential Pollutant Loads (LUHPPLs)

The proposed development is not a LUHPPL and therefore Standard 5 is not applicable.

Standard 6: Critical Areas

The proposed development does not discharge to a critical area and therefore Standard 6 is not applicable.

Standard 7: Redevelopment and Other Projects Subject to the Standards Only to the Maximum Extent Practicable

The proposed development is not a redevelopment and therefore Standard 7 is not applicable.

Standard 8: Constr. Period Pollution Prevention and Erosion & Sedimentation Control

A Construction Period Pollution Prevention, including an Erosion and Sedimentation Control Plan is provided in Appendix D.

Standard 9: Operation and Maintenance Plan

The Operation and Maintenance Plan is provided in Appendix E.

Standard 10: Prohibition of Illicit Discharges

There are no illicit discharges anticipated for the proposed development however measures to prevent illicit discharges will be included within the Long-Term Pollution Prevention Plan. Also, as required, an Illicit Discharge Compliance Statement will be submitted prior to the discharge of any storm water to the post-construction storm water Best Management Practices (BMPs).





1292_LOT 61 EXCON

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Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
1.840	77	Newly graded area, HSG A (E1, E2, E3)
0.313	30	Woods, Good, HSG A (E1, E2, E3)
2.152	70	TOTAL AREA

1292_LOT 61 EXCON

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
2.152	HSG A	E1, E2, E3
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
0.000	Other	
2.152		TOTAL AREA

1292_LOT 61 EXCON

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Ground Covers (all nodes)

HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment
(acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers
1.840	0.000	0.000	0.000	0.000	1.840	Newly graded ar	ea E1, E2, E3
0.313	0.000	0.000	0.000	0.000	0.313	Woods, Good	E1, E2, E3
2.152	0.000	0.000	0.000	0.000	2.152	TOTAL AREA	

Bourne_Wildwood Lane - Lot 61 Type II 24-hr 2-YR Rainfall=3.41"

1292 LOT 61 EXCON

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Time span=5.00-24.00 hrs, dt=0.05 hrs, 381 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchmente1: WILDWOODFLOW Runoff Area=12,921 sf 0.00% Impervious Runoff Depth>1.29"

Flow Length=171' Tc=16.3 min CN=76 Runoff=0.47 cfs 0.032 af

SubcatchmentE2: NORTHERNFLOW Runoff Area=62,611 sf 0.00% Impervious Runoff Depth>1.06"

Flow Length=266' Tc=8.6 min CN=72 Runoff=2.38 cfs 0.127 af

SubcatchmentE3: OCEANPINESFLOW Runoff Area=18,229 sf 0.00% Impervious Runoff Depth>0.45"

Flow Length=186' Tc=8.9 min CN=59 Runoff=0.22 cfs 0.016 af

Total Runoff Area = 2.152 ac Runoff Volume = 0.175 af Average Runoff Depth = 0.97" 100.00% Pervious = 2.152 ac 0.00% Impervious = 0.000 ac

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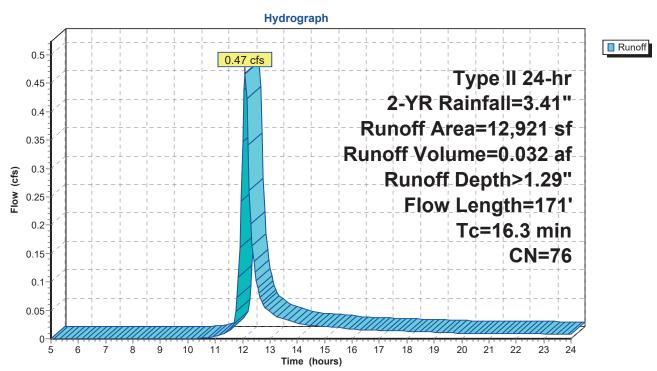
Summary for Subcatchment E1: WILDWOOD FLOW

Runoff = 0.47 cfs @ 12.09 hrs, Volume= 0.032 af, Depth> 1.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-YR Rainfall=3.41"

_	Α	rea (sf)	CN [Description		
		12,697	77 N	lewly grad	ed area, H	SG A
_		224	30 V	Voods, Go	od, HSG A	
		12,921	76 V	Veighted A	verage	
		12,921	1	00.00% P	ervious Are	ea
	Тс	Length	Slope	,	. ,	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	15.8	50	0.0100	0.05		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.41"
	0.5	121	0.0741	4.38		Shallow Concentrated Flow, B-C
_						Unpaved Kv= 16.1 fps
_	16.3	171	Total			

Subcatchment E1: WILDWOOD FLOW



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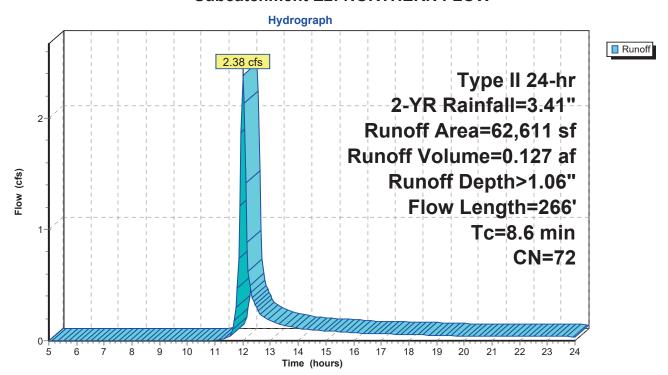
Summary for Subcatchment E2: NORTHERN FLOW

Runoff = 2.38 cfs @ 12.01 hrs, Volume= 0.127 af, Depth> 1.06"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-YR Rainfall=3.41"

	Aı	rea (sf)	CN [Description		
		56,005	77 N	lewly grad	ed area, H	SG A
		6,606	30 V	Voods, Go	od, HSG A	
		62,611	72 \	Veighted A	verage	
		62,611	1	00.00% P	ervious Are	ea
	Тс	Length	Slope	•	. ,	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.7	50	0.0600	0.11		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.41"
	0.9	216	0.0613	3.99		Shallow Concentrated Flow, B-C
						Unpaved Kv= 16.1 fps
	8.6	266	Total			

Subcatchment E2: NORTHERN FLOW



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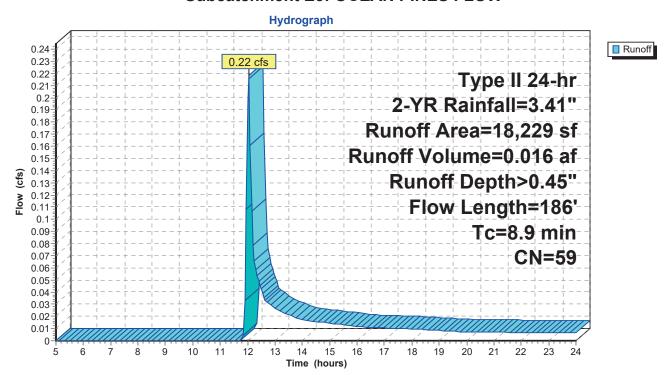
Summary for Subcatchment E3: OCEAN PINES FLOW

Runoff = 0.22 cfs @ 12.04 hrs, Volume= 0.016 af, Depth> 0.45"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-YR Rainfall=3.41"

A	rea (sf)	CN E	escription		
	11,435	77 N	lewly grad	ed area, H	SG A
	6,794	30 V	Voods, Go	od, HSG A	
	18,229	59 V	Veighted A	verage	
	18,229	1	00.00% P	ervious Are	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.3	50	0.0500	0.10		Sheet Flow, A-B
					Woods: Light underbrush n= 0.400 P2= 3.41"
0.6	136	0.0511	3.64		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
8.9	186	Total			

Subcatchment E3: OCEAN PINES FLOW



Bourne_Wildwood Lane - Lot 61 Type II 24-hr 10-YR Rainfall=4.98"

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Time span=5.00-24.00 hrs, dt=0.05 hrs, 381 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

SubcatchmentE1: WILDWOODFLOW Runoff Area=12,921 sf 0.00% Impervious Runoff Depth>2.51"

Flow Length=171' Tc=16.3 min CN=76 Runoff=0.92 cfs 0.062 af

SubcatchmentE2: NORTHERNFLOW Runoff Area=62,611 sf 0.00% Impervious Runoff Depth>2.18"

Flow Length=266' Tc=8.6 min CN=72 Runoff=5.02 cfs 0.261 af

SubcatchmentE3: OCEANPINESFLOW Runoff Area=18,229 sf 0.00% Impervious Runoff Depth>1.22"

Flow Length=186' Tc=8.9 min CN=59 Runoff=0.75 cfs 0.043 af

Total Runoff Area = 2.152 ac Runoff Volume = 0.365 af Average Runoff Depth = 2.04" 100.00% Pervious = 2.152 ac 0.00% Impervious = 0.000 ac

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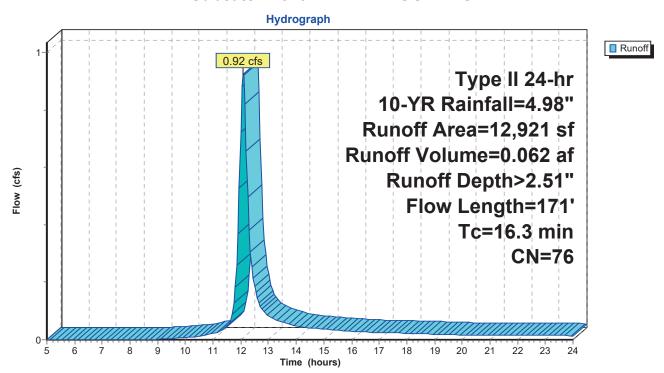
Summary for Subcatchment E1: WILDWOOD FLOW

Runoff = 0.92 cfs @ 12.09 hrs, Volume= 0.062 af, Depth> 2.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR Rainfall=4.98"

A	rea (sf)	CN E	Description		
	12,697	77 N	lewly grad	ed area, H	SG A
	224	30 V	Voods, Go	od, HSG A	
	12,921	76 V	Veighted A	verage	
	12,921	1	00.00% P	ervious Are	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
15.8	50	0.0100	0.05		Sheet Flow, A-B
					Woods: Light underbrush n= 0.400 P2= 3.41"
0.5	121	0.0741	4.38		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
16.3	171	Total			

Subcatchment E1: WILDWOOD FLOW



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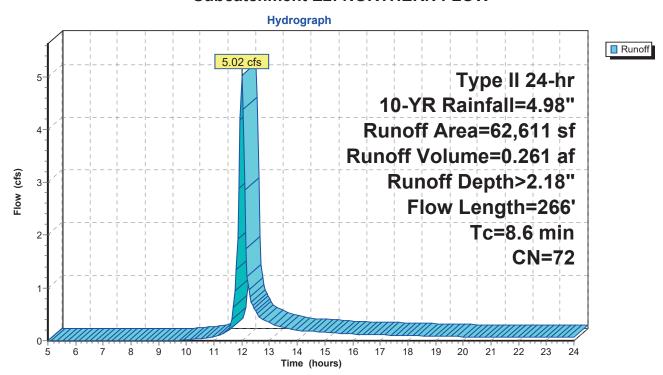
Summary for Subcatchment E2: NORTHERN FLOW

Runoff = 5.02 cfs @ 12.00 hrs, Volume= 0.261 af, Depth> 2.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR Rainfall=4.98"

	Aı	rea (sf)	CN [Description		
		56,005	77 N	lewly grad	ed area, H	SG A
		6,606	30 V	Voods, Go	od, HSG A	
		62,611	72 \	Veighted A	verage	
		62,611	1	00.00% P	ervious Are	ea
	Тс	Length	Slope	•	. ,	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.7	50	0.0600	0.11		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.41"
	0.9	216	0.0613	3.99		Shallow Concentrated Flow, B-C
						Unpaved Kv= 16.1 fps
	8.6	266	Total			

Subcatchment E2: NORTHERN FLOW



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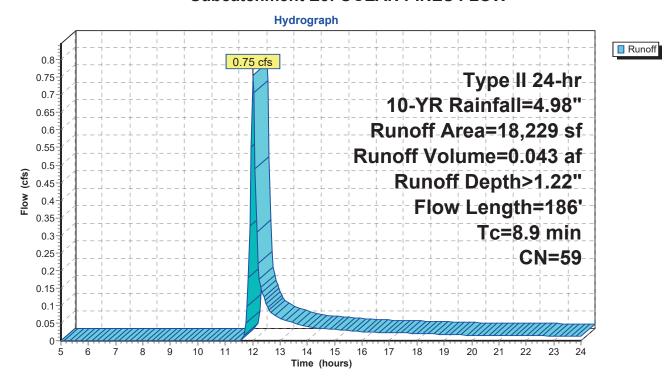
Summary for Subcatchment E3: OCEAN PINES FLOW

Runoff = 0.75 cfs @ 12.02 hrs, Volume= 0.043 af, Depth> 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR Rainfall=4.98"

A	rea (sf)	CN E	escription		
	11,435	77 N	lewly grad	ed area, H	SG A
	6,794	30 V	Voods, Go	od, HSG A	
	18,229	59 V	Veighted A	verage	
	18,229	1	00.00% P	ervious Are	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.3	50	0.0500	0.10		Sheet Flow, A-B
					Woods: Light underbrush n= 0.400 P2= 3.41"
0.6	136	0.0511	3.64		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
8.9	186	Total			

Subcatchment E3: OCEAN PINES FLOW



Bourne_Wildwood Lane - Lot 61 Type II 24-hr 25-YR Rainfall=5.95"

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Time span=5.00-24.00 hrs, dt=0.05 hrs, 381 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

SubcatchmentE1: WILDWOODFLOW Runoff Area=12,921 sf 0.00% Impervious Runoff Depth>3.32"

Flow Length=171' Tc=16.3 min CN=76 Runoff=1.22 cfs 0.082 af

SubcatchmentE2: NORTHERNFLOW Runoff Area=62,611 sf 0.00% Impervious Runoff Depth>2.95"

Flow Length=266' Tc=8.6 min CN=72 Runoff=6.79 cfs 0.353 af

SubcatchmentE3: OCEANPINESFLOW Runoff Area=18,229 sf 0.00% Impervious Runoff Depth>1.80"

Flow Length=186' Tc=8.9 min CN=59 Runoff=1.16 cfs 0.063 af

Total Runoff Area = 2.152 ac Runoff Volume = 0.498 af Average Runoff Depth = 2.78" 100.00% Pervious = 2.152 ac 0.00% Impervious = 0.000 ac

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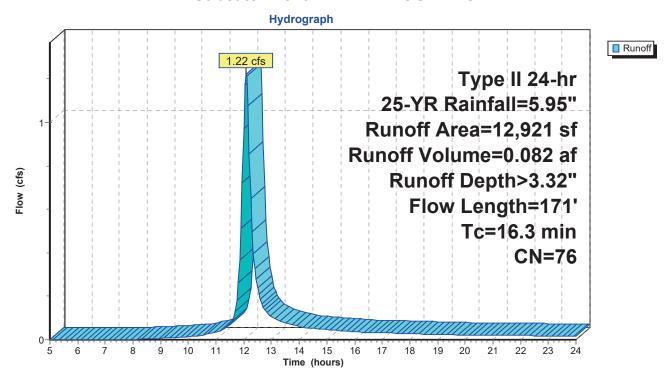
Summary for Subcatchment E1: WILDWOOD FLOW

Runoff = 1.22 cfs @ 12.09 hrs, Volume= 0.082 af, Depth> 3.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR Rainfall=5.95"

A	rea (sf)	CN [Description		
	12,697	77 I	Newly grad	ed area, H	SG A
	224	30 \	Voods, Go	od, HSG A	
	12,921	76 \	Veighted A	verage	
	12,921	•	100.00% P	ervious Are	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
15.8	50	0.0100	0.05		Sheet Flow, A-B
					Woods: Light underbrush n= 0.400 P2= 3.41"
0.5	121	0.0741	4.38		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
16.3	171	Total			

Subcatchment E1: WILDWOOD FLOW



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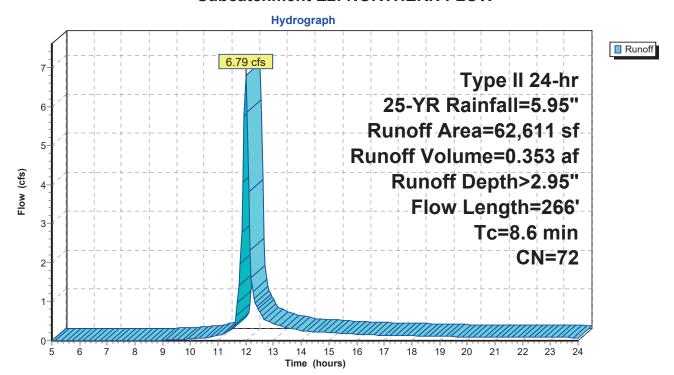
Summary for Subcatchment E2: NORTHERN FLOW

Runoff = 6.79 cfs @ 12.00 hrs, Volume= 0.353 af, Depth> 2.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR Rainfall=5.95"

A	rea (sf)	CN E	escription		
	56,005	77 N	lewly grad	ed area, H	SG A
	6,606	30 V	Voods, Go	od, HSG A	
	62,611	72 V	Veighted A	verage	
	62,611	1	00.00% P	ervious Are	ea
_					
Tc	Length	Slope		Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.7	50	0.0600	0.11		Sheet Flow, A-B
					Woods: Light underbrush n= 0.400 P2= 3.41"
0.9	216	0.0613	3.99		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
8.6	266	Total			

Subcatchment E2: NORTHERN FLOW



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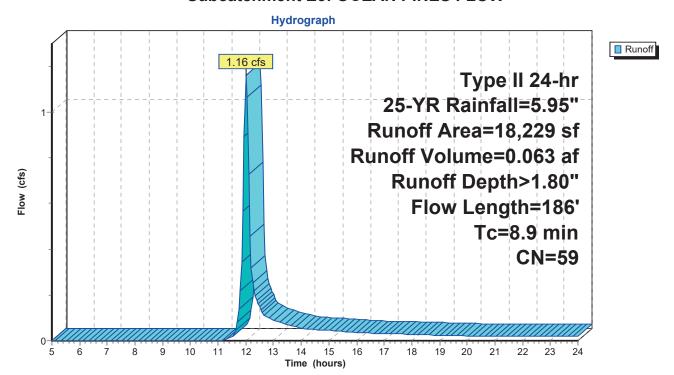
Summary for Subcatchment E3: OCEAN PINES FLOW

Runoff = 1.16 cfs @ 12.01 hrs, Volume= 0.063 af, Depth> 1.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR Rainfall=5.95"

A	rea (sf)	CN E	escription		
	11,435	77 N	lewly grad	ed area, H	SG A
	6,794	30 V	Voods, Go	od, HSG A	
	18,229	59 V	Veighted A	verage	
	18,229	1	00.00% P	ervious Are	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.3	50	0.0500	0.10		Sheet Flow, A-B
					Woods: Light underbrush n= 0.400 P2= 3.41"
0.6	136	0.0511	3.64		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
8.9	186	Total			

Subcatchment E3: OCEAN PINES FLOW



Bourne_Wildwood Lane - Lot 61 Type II 24-hr 100-YR Rainfall=7.46"

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Time span=5.00-24.00 hrs, dt=0.05 hrs, 381 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchmente1: WILDWOODFLOW Runoff Area=12,921 sf 0.00% Impervious Runoff Depth>4.65"

Flow Length=171' Tc=16.3 min CN=76 Runoff=1.70 cfs 0.115 af

SubcatchmentE2: NORTHERNFLOW Runoff Area=62,611 sf 0.00% Impervious Runoff Depth>4.22"

Flow Length=266' Tc=8.6 min CN=72 Runoff=9.66 cfs 0.505 af

SubcatchmentE3: OCEANPINES FLOW

Runoff Area=18,229 sf 0.00% Impervious Runoff Depth>2.82"
Flow Length=186' Tc=8.9 min CN=59 Runoff=1.86 cfs 0.098 af

Total Runoff Area = 2.152 ac Runoff Volume = 0.718 af Average Runoff Depth = 4.01" 100.00% Pervious = 2.152 ac 0.00% Impervious = 0.000 ac

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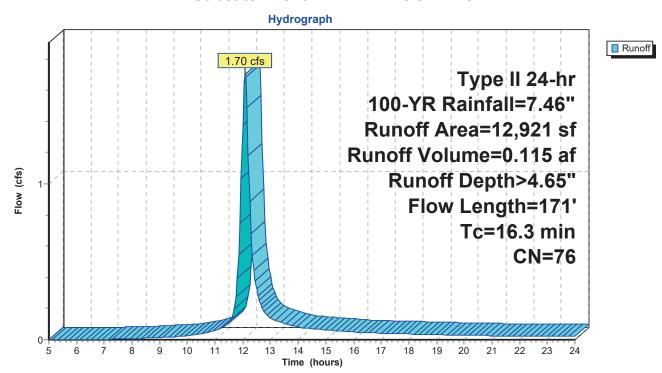
Summary for Subcatchment E1: WILDWOOD FLOW

Runoff = 1.70 cfs @ 12.08 hrs, Volume= 0.115 af, Depth> 4.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR Rainfall=7.46"

A	rea (sf)	CN [Description		
	12,697	77 N	Newly grad	ed area, H	SG A
	224	30 V	Voods, Go	od, HSG A	
	12,921	76 V	Veighted A	verage	
	12,921	1	00.00% P	ervious Are	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
15.8	50	0.0100	0.05		Sheet Flow, A-B
					Woods: Light underbrush n= 0.400 P2= 3.41"
0.5	121	0.0741	4.38		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
16.3	171	Total			

Subcatchment E1: WILDWOOD FLOW



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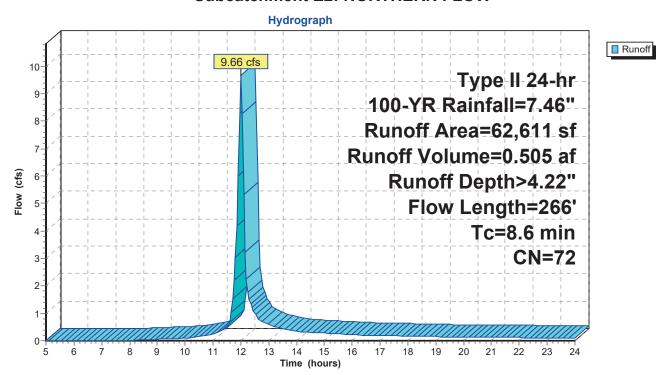
Summary for Subcatchment E2: NORTHERN FLOW

Runoff = 9.66 cfs @ 12.00 hrs, Volume= 0.505 af, Depth> 4.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR Rainfall=7.46"

	Aı	Area (sf) CN Description					
	56,005 77 Newly graded area, HSG A						
6,606 30 Woods, Good, HSG A							
	62,611 72 Weighted Average						
62,611 100.00% Pervious Area							
	Тс	Length	Slope	•	. ,	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	7.7	50	0.0600	0.11		Sheet Flow, A-B	
						Woods: Light underbrush n= 0.400 P2= 3.41"	
	0.9	216	0.0613	3.99		Shallow Concentrated Flow, B-C	
_						Unpaved Kv= 16.1 fps	
_	8.6	266	Total	•			

Subcatchment E2: NORTHERN FLOW



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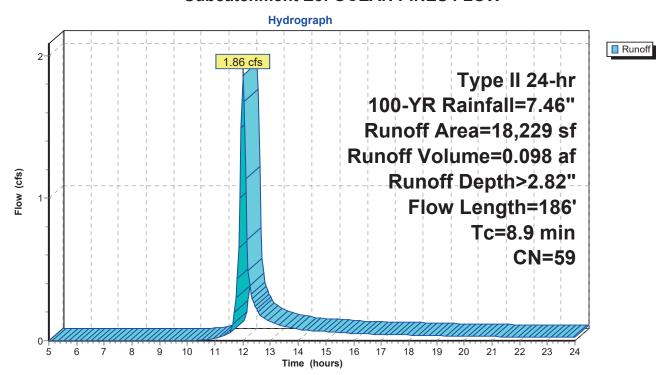
Summary for Subcatchment E3: OCEAN PINES FLOW

Runoff = 1.86 cfs @ 12.01 hrs, Volume= 0.098 af, Depth> 2.82"

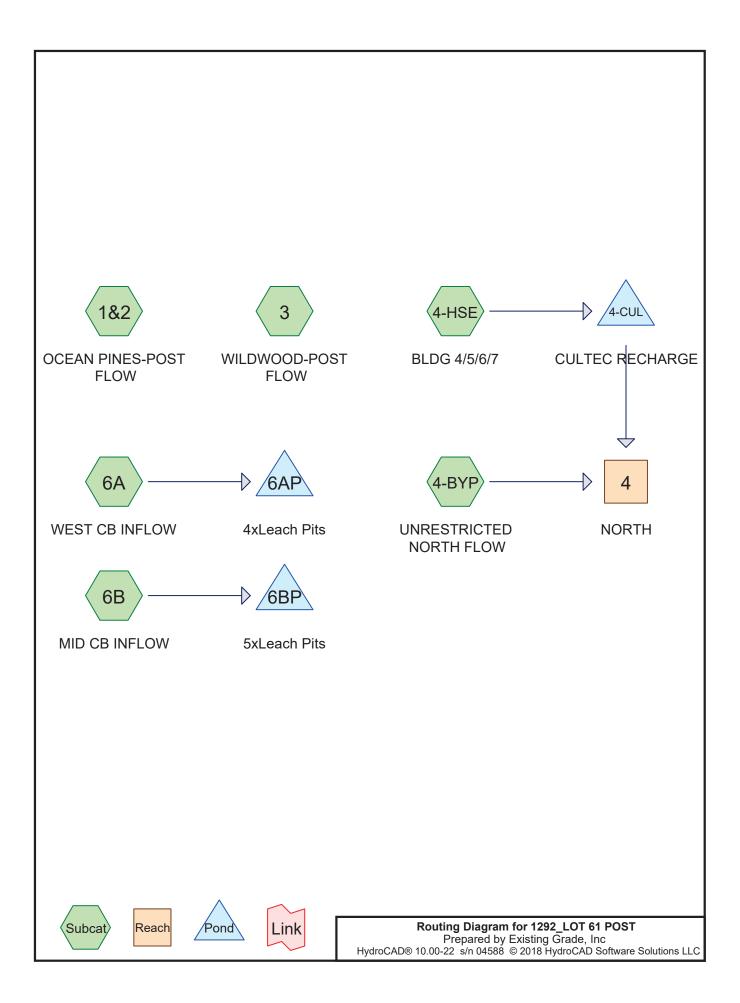
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR Rainfall=7.46"

A	Area (sf) CN Description							
	11,435 77 Newly graded area, HSG A							
	6,794 30 Woods, Good, HSG A							
18,229 59 Weighted Average								
18,229 100.00% Pervious Area								
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
8.3	50	0.0500	0.10		Sheet Flow, A-B			
					Woods: Light underbrush n= 0.400 P2= 3.41"			
0.6	136	0.0511	3.64		Shallow Concentrated Flow, B-C			
					Unpaved Kv= 16.1 fps			
8.9	186	Total	•					

Subcatchment E3: OCEAN PINES FLOW







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Area Listing (all nodes)

Area	CN	Description
 (acres)		(subcatchment-numbers)
1.181	39	>75% Grass cover, Good, HSG A (1&2, 3, 4-BYP, 6A, 6B)
0.490	98	Paved parking, HSG A (6A, 6B)
0.481	98	Roofs, HSG A (4-HSE, 6A)
2.152	66	TOTAL AREA

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
2.152	HSG A	1&2, 3, 4-BYP, 4-HSE, 6A, 6B
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
0.000	Other	
2.152		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
 1.181	0.000	0.000	0.000	0.000	1.181	>75% Grass cover,	Good 1&2, 3,
							4-BYP, 6A,
							6B
0.490	0.000	0.000	0.000	0.000	0.490	Paved parking	6A, 6B
0.481	0.000	0.000	0.000	0.000	0.481	Roofs	4-HSE, 6A
2.152	0.000	0.000	0.000	0.000	2.152	TOTAL AREA	

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Pipe Listing (all nodes)

Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Diam/Width	Height	Inside-Fill
	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)
1	4-CUL	82.00	81.00	25.0	0.0400	0.010	6.0	0.0	0.0

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Time span=5.00-24.00 hrs, dt=0.05 hrs, 381 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchmentl &2: OCEANPINES-POSTFLOW Runoff Area=6,195 sf 0.00% Impervious Runoff Depth>0.00" Flow Length=104' Tc=7.1 min CN=39 Runoff=0.00 cfs 0.000 af

Subcatchment3: WILDWOOD-POSTFLOW
Runoff Area=7,030 sf 0.00% Impervious Runoff Depth>0.00"
Flow Length=48' Slope=0.1250 '/' Tc=5.7 min CN=39 Runoff=0.00 cfs 0.000 af

Subcatchment4-BYP:UNRESTRICTEDNORTH Runoff Area=24,134 sf 0.00% Impervious Runoff Depth>0.00" Flow Length=325' Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af

Subcatchment4-HSE:BLDG 4/5/6/7 Runoff Area=12,277 sf 100.00% Impervious Runoff Depth>3.10"
Tc=5.0 min CN=98 Runoff=1.37 cfs 0.073 af

Subcatchment6A: WESTCB INFLOW

Runoff Area=16,884 sf 81.81% Impervious Runoff Depth>2.10"

Tc=5.0 min CN=87 Runoff=1.44 cfs 0.068 af

Subcatchment6B: MID CB INFLOW

Runoff Area=27,241 sf 59.51% Impervious Runoff Depth>1.17"

Flow Length=374' Tc=18.2 min CN=74 Runoff=0.83 cfs 0.061 af

Reach4: NORTH Inflow=1.16 cfs 0.022 af
Outflow=1.16 cfs 0.022 af

Pond 4-CUL:CULTECRECHARGE
Peak Elev=82.86' Storage=0.014 af Inflow=1.37 cfs 0.073 af
Discarded=0.07 cfs 0.051 af Primary=1.16 cfs 0.021 af Outflow=1.23 cfs 0.073 af

Pond 6AP: 4xLeachPits

Peak Elev=79.14' Storage=0.026 af Inflow=1.44 cfs 0.068 af Outflow=0.13 cfs 0.068 af

Pond 6BP: 5xLeachPits

Peak Elev=81.83' Storage=0.019 af Inflow=0.83 cfs 0.061 af
Outflow=0.16 cfs 0.061 af

Total Runoff Area = 2.152 ac Runoff Volume = 0.202 af Average Runoff Depth = 1.13" 54.88% Pervious = 1.181 ac 45.12% Impervious = 0.971 ac

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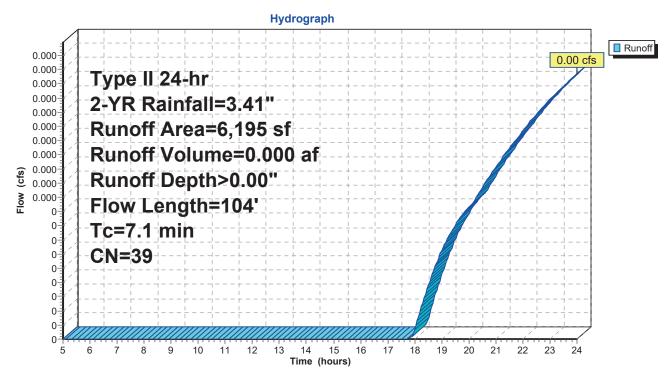
Summary for Subcatchment 1&2: OCEAN PINES-POST FLOW

Runoff = 0.00 cfs @ 24.00 hrs, Volume= 0.000 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-YR Rainfall=3.41"

	Aı	rea (sf)	CN D	escription			
		6,195	39 >	75% Gras	s cover, Go	ood, HSG A	
		6,195	1	00.00% Pe	ervious Are	a	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
-	7.0	50	0.0800	0.12	, ,	Sheet Flow, A-B	_
	0.1	54	0.3700	9.79		Grass: Bermuda n= 0.410 P2= 3.41" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps	
	7.1	104	Total				_

Subcatchment 1&2: OCEAN PINES-POST FLOW



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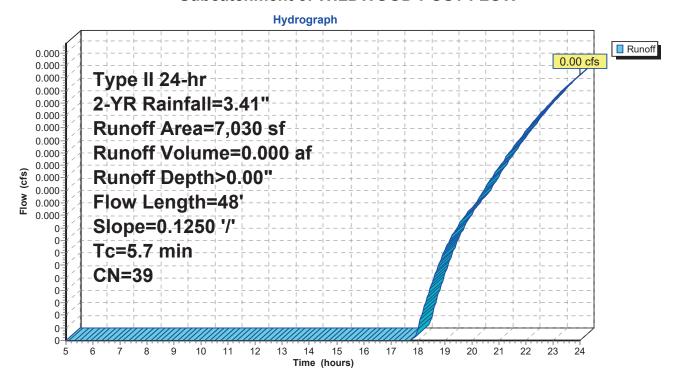
Summary for Subcatchment 3: WILDWOOD-POST FLOW

Runoff = 0.00 cfs @ 24.00 hrs, Volume= 0.000 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-YR Rainfall=3.41"

A	rea (sf)	CN [Description		
	7,030	39 >	75% Gras	s cover, Go	ood, HSG A
	7,030	1	00.00% P	ervious Are	ea
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.7	48	0.1250	0.14		Sheet Flow, A-B
					Grass: Bermuda n= 0.410 P2= 3.41"

Subcatchment 3: WILDWOOD-POST FLOW



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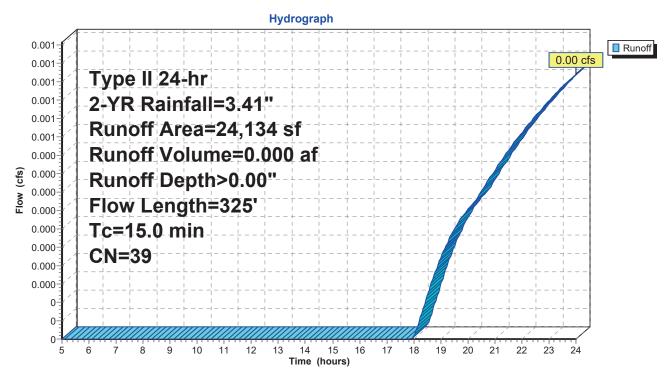
Summary for Subcatchment 4-BYP: UNRESTRICTED NORTH FLOW

Runoff = 0.00 cfs @ 24.00 hrs, Volume= 0.000 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-YR Rainfall=3.41"

	Aı	rea (sf)	CN D	escription			
-		24,134				ood, HSG A	_
-		24,134			ervious Are	,	_
	_				_		
	Tc	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		_
	13.7	50	0.0150	0.06		Sheet Flow, A-B	
						Grass: Bermuda n= 0.410 P2= 3.41"	
	1.3	275	0.0518	3.66		Shallow Concentrated Flow, B-C	
						Unpaved Kv= 16.1 fps	
_	15.0	325	Total				_

Subcatchment 4-BYP: UNRESTRICTED NORTH FLOW



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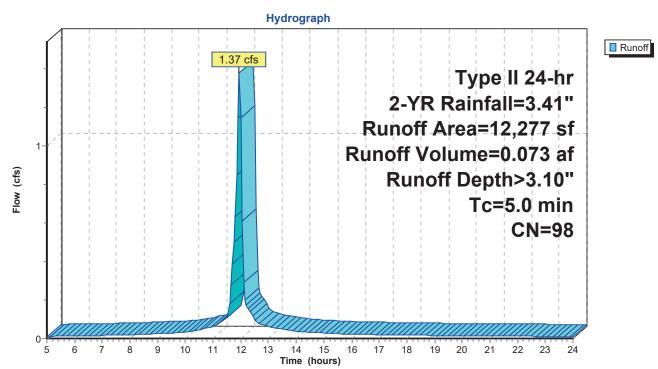
Summary for Subcatchment 4-HSE: BLDG 4/5/6/7

Runoff = 1.37 cfs @ 11.95 hrs, Volume= 0.073 af, Depth> 3.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-YR Rainfall=3.41"

Area (sf) CN	Description		
12,2	77 98	Roofs, HSC	A S	
12,2	77	100.00% In	npervious A	Area
Tc Ler (min) (fo	gth Slopet) (ft/	pe Velocity ft) (ft/sec)	Capacity (cfs)	Description
5.0				Direct Entry, DIRECT (MIN)

Subcatchment 4-HSE: BLDG 4/5/6/7



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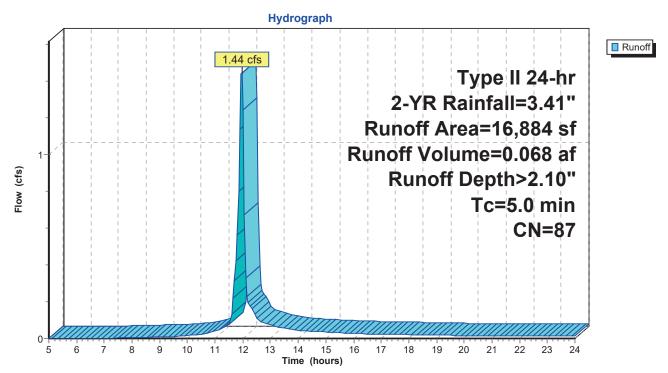
Summary for Subcatchment 6A: WEST CB INFLOW

Runoff = 1.44 cfs @ 11.96 hrs, Volume= 0.068 af, Depth> 2.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-YR Rainfall=3.41"

Area	(sf) CN	Description	Description					
5,	147 98	Paved parki	ng, HSG A	1				
3,	071 39	>75% Grass	s cover, Go	ood, HSG A				
8,	666 98	Roofs, HSG	iΑ					
16	884 87	Weighted A	verage					
3,	071	18.19% Per	vious Area					
13,	813	81.81% Imp	ervious Ar	ea				
Tc Le	ength Slo	ope Velocity	Capacity	Description				
(min)	feet) (f	ft/ft) (ft/sec)	(cfs)					
5.0				Direct Entry, DIRECT (MIN)				

Subcatchment 6A: WEST CB INFLOW



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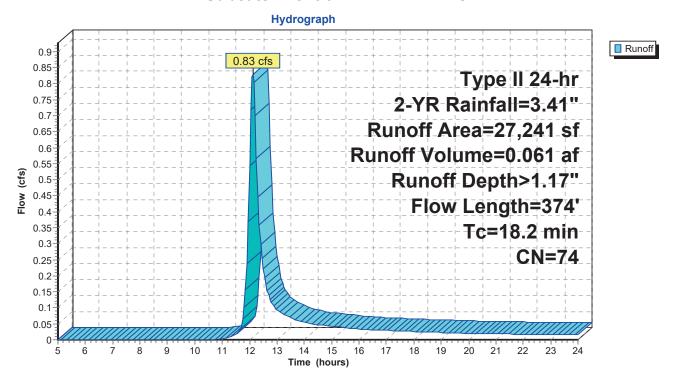
Summary for Subcatchment 6B: MID CB INFLOW

Runoff = 0.83 cfs @ 12.12 hrs, Volume= 0.061 af, Depth> 1.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-YR Rainfall=3.41"

_	Α	rea (sf)	CN [escription		
		16,212			ing, HSG A	
		11,029	39 >	<u>∙75% Gras</u>	s cover, Go	ood, HSG A
		27,241	74 V	Veighted A	verage	
		11,029	4	0.49% Pe	rvious Area	1
		16,212	5	9.51% lm	pervious Ar	rea
	Тс	Length	Slope	•	. ,	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	16.1	50	0.0100	0.05		Sheet Flow, A-B
						Grass: Bermuda n= 0.410 P2= 3.41"
	0.1	27	0.1850	6.92		Shallow Concentrated Flow, B-C
						Unpaved Kv= 16.1 fps
	2.0	297	0.0155	2.53		Shallow Concentrated Flow, C-D
						Paved Kv= 20.3 fps
	18.2	374	Total			

Subcatchment 6B: MID CB INFLOW



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Summary for Reach 4: NORTH

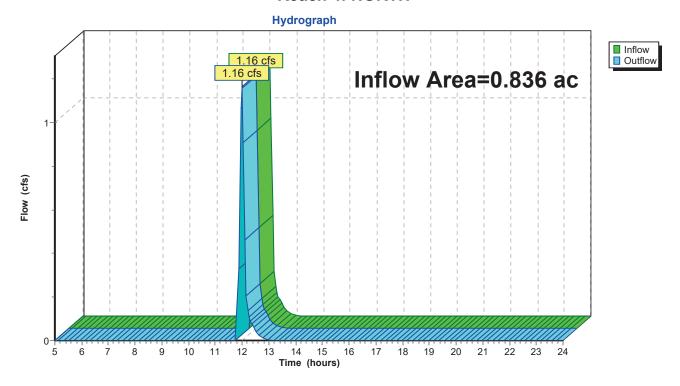
0.836 ac, 33.72% Impervious, Inflow Depth > 0.31" for 2-YR event Inflow Area =

Inflow 0.022 af

1.16 cfs @ 11.99 hrs, Volume= 1.16 cfs @ 11.99 hrs, Volume= Outflow 0.022 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs

Reach 4: NORTH



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Summary for Pond 4-CUL: CULTEC RECHARGE

Inflow Area = 0.282 ac,100.00% Impervious, Inflow Depth > 3.10" for 2-YR event
Inflow = 1.37 cfs @ 11.95 hrs, Volume= 0.073 af
Outflow = 1.23 cfs @ 11.99 hrs, Volume= 0.073 af, Atten= 10%, Lag= 2.3 min
Discarded = 0.07 cfs @ 11.99 hrs, Volume= 0.051 af
Primary = 1.16 cfs @ 11.99 hrs, Volume= 0.021 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 82.86'@ 11.99 hrs Surf.Area= 0.008 ac Storage= 0.014 af

Plug-Flow detention time=29.7 min calculated for 0.073 af (100% of inflow) Center-of-Mass det. time=29.2 min (792.1 - 762.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	80.00'	0.007 af	6.33'W x 52.50'L x 3.54'H Field A
			0.027 af Overall - 0.009 af Embedded = 0.018 af x 40.0% Voids
#2A	80.50'	0.009 af	Cultec R-330XLHDx 7 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 1 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	80.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'
#2	Primary	82.00'	6.0" Round Culvert X 2.00 L= 25.0' Ke= 0.900
	•		Inlet / Outlet Invert= 82.00' / 81.00' S= 0.0400' /' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 0.20 sf

Primary OutFlowMax=1.13 cfs @ 11.99 hrs HW=82.83' (Free Discharge) —2=Culvert (Inlet Controls 1.13 cfs @ 2.89 fps)

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Pond 4-CUL: CULTEC RECHARGE - Chamber Wizard Field A

ChamberModel = CultecR-330XLHD(CultecRecharger®330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 1 rows

7 Chambers/Row x 7.00' Long \pm 1.50' Row Adjustment \pm 50.50' Row Length \pm 12.0" End Stone x 2 \pm 52.50' Base Length

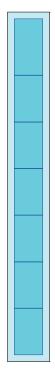
1 Rows x 52.0" Wide + 12.0" Side Stone x 2 = 6.33' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

7 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 1 Rows = 376.3 cf Chamber Storage

1,177.6 cf Field - 376.3 cf Chambers = 801.3 cf Stone x 40.0% Voids = 320.5 cf Stone Storage

Chamber Storage + Stone Storage = 696.8 cf = 0.016 af Overall Storage Efficiency = 59.2% Overall System Size = 52.50' x 6.33' x 3.54'

7 Chambers 43.6 cy Field 29.7 cy Stone

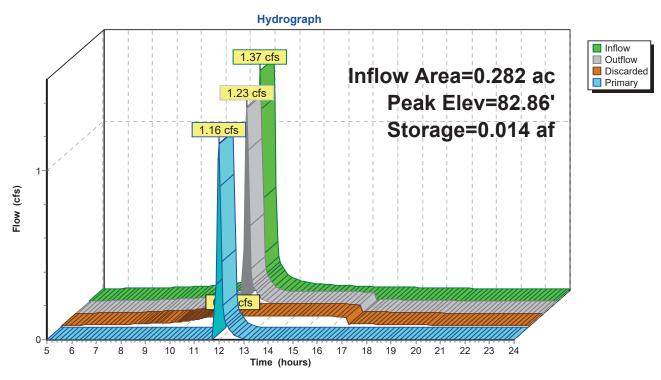




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Pond 4-CUL: CULTEC RECHARGE



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Summary for Pond 6AP: 4xLeach Pits

Inflow Area = 0.388 ac, 81.81% Impervious, Inflow Depth > 2.10" for 2-YR event

Inflow = 1.44 cfs @ 11.96 hrs, Volume= 0.068 af

Outflow = 0.13 cfs @ 12.44 hrs, Volume= 0.068 af, Atten= 91%, Lag= 28.9 min

Discarded = 0.13 cfs @ 12.44 hrs, Volume= 0.068 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 79.14'@ 12.44 hrs Surf.Area= 0.014 ac Storage= 0.026 af

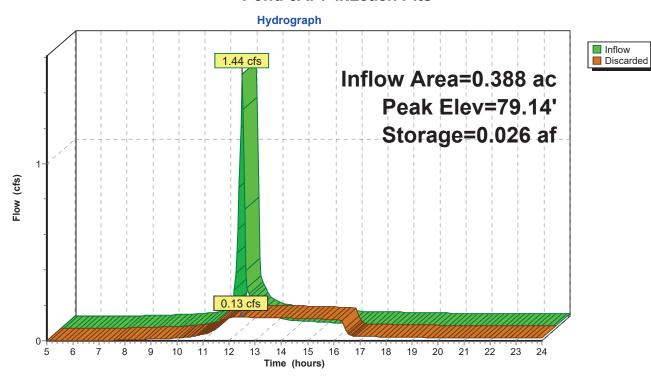
Plug-Flow detention time=66.3 min calculated for 0.068 af (100% of inflow) Center-of-Mass det. time=65.3 min (876.9 - 811.7)

Volume	Invert	Avail.Storage	Storage Description
#1	76.00'	0.069 af	14.00'D x 12.00'H 4' Stone Surround 4
			0.170 af Overall - 0.031 af Embedded = 0.138 af x 50.0% Voids
#2	76.00'	0.031 af	6.00'D x 12.00'H Vertical Cone/Cylinder 4 Inside #1
		0.100 af	Total Available Storage
Device	Routing	Invert Ou	tlet Devices

Device	Routing	Invert	Outlet Devices
#1	Discarded	76.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'

Discarded OutFlowMax=0.13 cfs @ 12.44 hrs HW=79.14' (Free Discharge) **1=Exfiltration** (Controls 0.13 cfs)

Pond 6AP: 4xLeach Pits



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Summary for Pond 6BP: 5xLeach Pits

Inflow Area = 0.625 ac, 59.51% Impervious, Inflow Depth > 1.17" for 2-YR event

Inflow = 0.83 cfs @ 12.12 hrs, Volume= 0.061 af

Outflow = 0.16 cfs @ 12.64 hrs, Volume= 0.061 af, Atten= 81%, Lag= 31.5 min

Discarded = 0.16 cfs @ 12.64 hrs, Volume= 0.061 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 81.83'@ 12.64 hrs Surf.Area= 0.018 ac Storage= 0.019 af

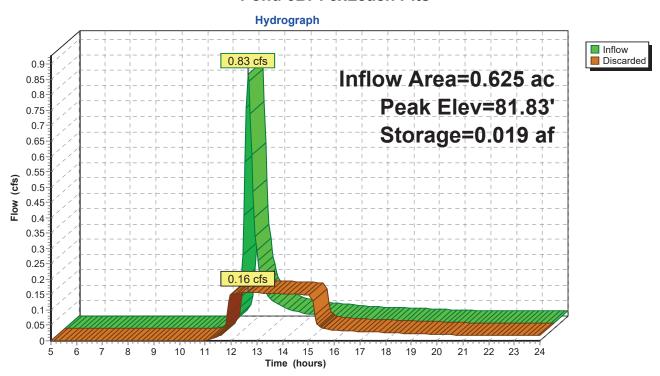
Plug-Flow detention time=39.6 min calculated for 0.061 af (100% of inflow) Center-of-Mass det. time=38.3 min (901.1 - 862.8)

Volume	Invert	Avail.Storage	Storage Description
#1	80.00'	0.087 af	14.00'D x 12.00'H 4' Stone Surround 5
			0.212 af Overall - 0.039 af Embedded = 0.173 af x 50.0% Voids
#2	80.00'	0.039 af	6.00'D x 12.00'H Vertical Cone/Cylinder 5 Inside #1
		0.125 af	Total Available Storage
			· ·

Device	Routing	Invert	Outlet Devices
#1	Discarded	80.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'

Discarded OutFlowMax=0.16 cfs @ 12.64 hrs HW=81.83' (Free Discharge) **1=Exfiltration** (Controls 0.16 cfs)

Pond 6BP: 5xLeach Pits



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Time span=5.00-24.00 hrs, dt=0.05 hrs, 381 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchmentl &2: OCEANPINES-POSTFLOW Runoff Area=6,195 sf 0.00% Impervious Runoff Depth>0.20" Flow Length=104' Tc=7.1 min CN=39 Runoff=0.00 cfs 0.002 af

Subcatchment3: WILDWOOD-POSTFLOW
Runoff Area=7,030 sf 0.00% Impervious Runoff Depth>0.20"
Flow Length=48' Slope=0.1250 '/' Tc=5.7 min CN=39 Runoff=0.01 cfs 0.003 af

Subcatchment4-BYP:UNRESTRICTEDNORTH Runoff Area=24,134 sf 0.00% Impervious Runoff Depth>0.19" Flow Length=325' Tc=15.0 min CN=39 Runoff=0.02 cfs 0.009 af

Subcatchment4-HSE:BLDG4/5/6/7 Runoff Area=12,277 sf 100.00% Impervious Runoff Depth>4.59" Tc=5.0 min CN=98 Runoff=2.02 cfs 0.108 af

Subcatchment6A: WESTCB INFLOW

Runoff Area=16,884 sf 81.81% Impervious Runoff Depth>3.55"

Tc=5.0 min CN=87 Runoff=2.37 cfs 0.115 af

Subcatchment6B: MID CB INFLOWRunoff Area=27,241 sf 59.51% Impervious Runoff Depth>2.34"
Flow Length=374' Tc=18.2 min CN=74 Runoff=1.71 cfs 0.122 af

Reach4: NORTH Inflow=1.79 cfs 0.051 af
Outflow=1.79 cfs 0.051 af

Pond 4-CUL:CULTECRECHARGE
Peak Elev=83.68' Storage=0.016 af Inflow=2.02 cfs 0.108 af
Discarded=0.07 cfs 0.065 af Primary=1.79 cfs 0.043 af Outflow=1.86 cfs 0.108 af

Pond 6AP: 4xLeachPits

Peak Elev=81.98' Storage=0.050 af Inflow=2.37 cfs 0.115 af
Outflow=0.14 cfs 0.114 af

Pond 6BP: 5xLeachPits

Peak Elev=84.92' Storage=0.051 af Inflow=1.71 cfs 0.122 af
Outflow=0.17 cfs 0.122 af

Total Runoff Area = 2.152 ac Runoff Volume = 0.358 af Average Runoff Depth = 2.00" 54.88% Pervious = 1.181 ac 45.12% Impervious = 0.971 ac

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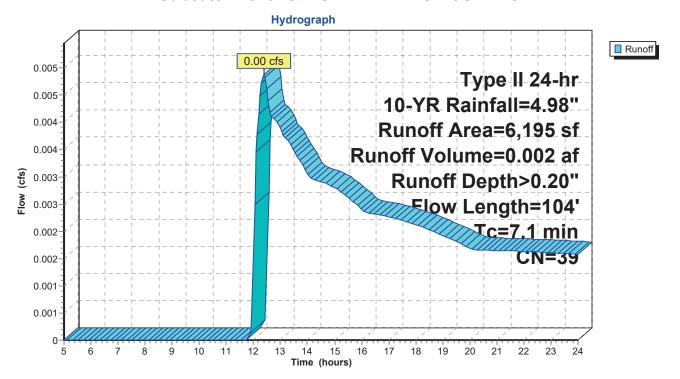
Summary for Subcatchment 1&2: OCEAN PINES-POST FLOW

Runoff = 0.00 cfs @ 12.38 hrs, Volume= 0.002 af, Depth> 0.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR Rainfall=4.98"

	Aı	rea (sf)	CN D	escription		
		6,195	39 >	75% Gras	s cover, Go	ood, HSG A
		6,195	1	00.00% P	ervious Are	a
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	7.0	50	0.0800	0.12	, ,	Sheet Flow, A-B
	0.1	54	0.3700	9.79		Grass: Bermuda n= 0.410 P2= 3.41" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
	7.1	104	Total			

Subcatchment 1&2: OCEAN PINES-POST FLOW



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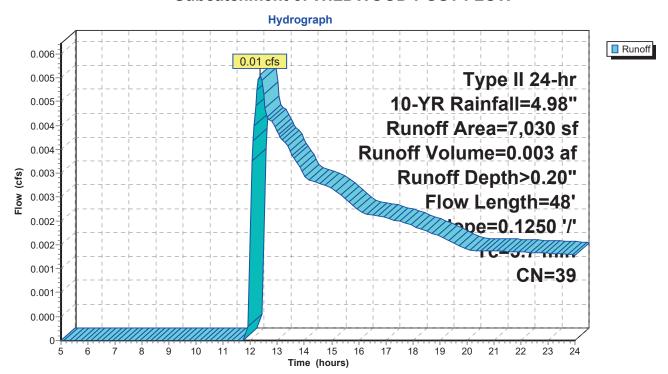
Summary for Subcatchment 3: WILDWOOD-POST FLOW

Runoff 0.01 cfs @ 12.36 hrs, Volume= 0.003 af, Depth> 0.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR Rainfall=4.98"

	A	rea (sf)	CN E	CN Description					
		7,030	39 >	39 >75% Grass cover, Good, HSG A					
		7,030	100.00% Pervious Area			a			
(Tc min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	5.7	48	0.1250	0.14		Sheet Flow, A-B			
						Grass: Bermuda n= 0.410 P2= 3.41"			

Subcatchment 3: WILDWOOD-POST FLOW



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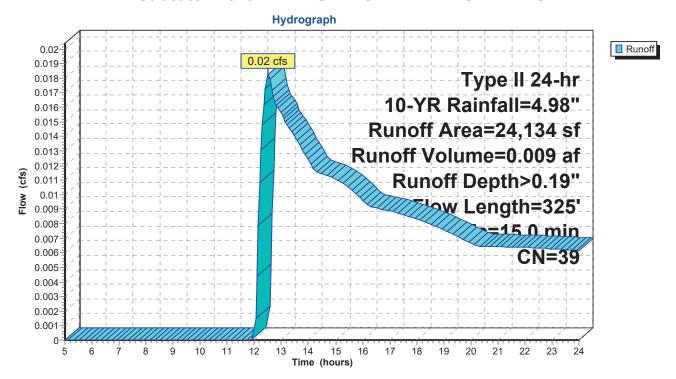
Summary for Subcatchment 4-BYP: UNRESTRICTED NORTH FLOW

Runoff = 0.02 cfs @ 12.51 hrs, Volume= 0.009 af, Depth> 0.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR Rainfall=4.98"

	Aı	rea (sf)	CN D	escription		
		24,134	39 >	75% Gras	s cover, Go	ood, HSG A
		24,134	1	00.00% P	ervious Are	ea
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	13.7	50	0.0150	0.06	, ,	Sheet Flow, A-B
	1.3	275	0.0518	3.66		Grass: Bermuda n= 0.410 P2= 3.41" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
	15.0	325	Total			

Subcatchment 4-BYP: UNRESTRICTED NORTH FLOW



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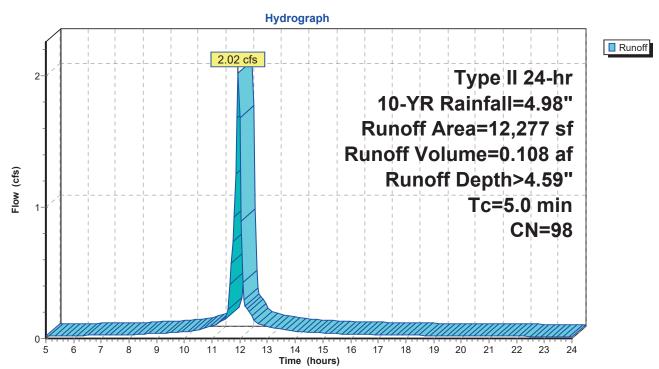
Summary for Subcatchment 4-HSE: BLDG 4/5/6/7

Runoff = 2.02 cfs @ 11.95 hrs, Volume= 0.108 af, Depth> 4.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR Rainfall=4.98"

Area (sf) CN	Description					
12,2	77 98	98 Roofs, HSG A					
12,2	77	100.00% In	npervious A	Area			
Tc Ler (min) (fo	gth Slopet) (ft/	pe Velocity ft) (ft/sec)	Capacity (cfs)	Description			
5.0				Direct Entry, DIRECT (MIN)			

Subcatchment 4-HSE: BLDG 4/5/6/7



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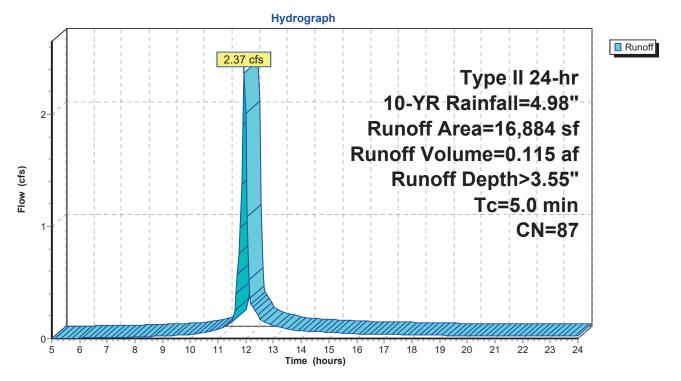
Summary for Subcatchment 6A: WEST CB INFLOW

Runoff = 2.37 cfs @ 11.95 hrs, Volume= 0.115 af, Depth> 3.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR Rainfall=4.98"

A	rea (sf)	CN	Description					
	5,147	98	Paved park	ing, HSG A	4			
	3,071	39	>75% Gras	s cover, Go	ood, HSG A			
	8,666	98	Roofs, HSC	A A				
	16,884	87	Weighted A	verage				
	3,071		18.19% Pe	rvious Area	1			
	13,813		81.81% Imp	rea				
Tc	Length	Slop	e Velocity	Capacity	Description			
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)				
5.0					Direct Entry, DIRECT (MIN)			

Subcatchment 6A: WEST CB INFLOW



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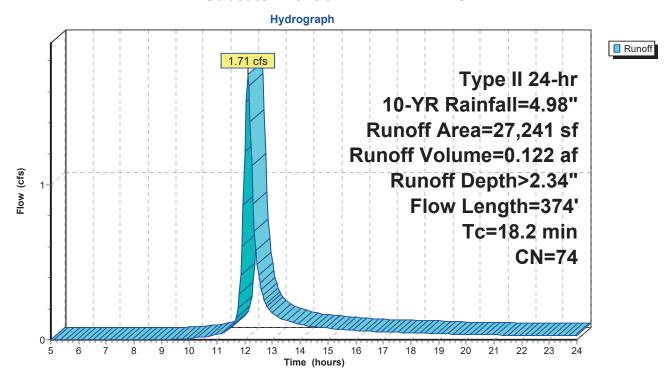
Summary for Subcatchment 6B: MID CB INFLOW

Runoff = 1.71 cfs @ 12.11 hrs, Volume= 0.122 af, Depth> 2.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-YR Rainfall=4.98"

_	Α	rea (sf)	CN [escription		
		16,212			ing, HSG A	
		11,029	39 >	<u>∙75% Gras</u>	s cover, Go	ood, HSG A
		27,241	74 V	Veighted A	verage	
		11,029	4	0.49% Pe	rvious Area	1
		16,212	5	9.51% lm	pervious Ar	rea
	Тс	Length	Slope	•	. ,	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	16.1	50	0.0100	0.05		Sheet Flow, A-B
						Grass: Bermuda n= 0.410 P2= 3.41"
	0.1	27	0.1850	6.92		Shallow Concentrated Flow, B-C
						Unpaved Kv= 16.1 fps
	2.0	297	0.0155	2.53		Shallow Concentrated Flow, C-D
						Paved Kv= 20.3 fps
	18.2	374	Total			

Subcatchment 6B: MID CB INFLOW



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Summary for Reach 4: NORTH

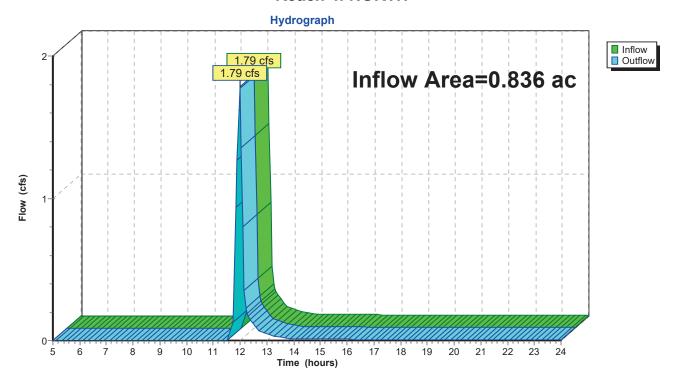
0.836 ac, 33.72% Impervious, Inflow Depth > 0.74" for 10-YR event Inflow Area =

Inflow 0.051 af

1.79 cfs @ 11.99 hrs, Volume= 1.79 cfs @ 11.99 hrs, Volume= Outflow 0.051 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs

Reach 4: NORTH



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Summary for Pond 4-CUL: CULTEC RECHARGE

Inflow Area = 0.282 ac,100.00% Impervious, Inflow Depth > 4.59" for 10-YR event
Inflow = 2.02 cfs @ 11.95 hrs, Volume= 0.108 af
Outflow = 1.86 cfs @ 11.99 hrs, Volume= 0.108 af, Atten= 8%, Lag= 2.3 min
Discarded = 0.07 cfs @ 11.99 hrs, Volume= 0.065 af
Primary = 1.79 cfs @ 11.99 hrs, Volume= 0.043 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 83.68'@ 11.99 hrs Surf.Area= 0.008 ac Storage= 0.016 af

Plug-Flow detention time=27.7 min calculated for 0.108 af (100% of inflow) Center-of-Mass det. time=27.4 min (787.4 - 760.0)

Volume	Invert	Avail.Storage	Storage Description	
#1A	80.00'	0.007 af	6.33'W x 52.50'L x 3.54'H Field A	
			0.027 af Overall - 0.009 af Embedded = 0.018 af x 40.0% Voids	
#2A	80.50'	0.009 af	Cultec R-330XLHDx 7 Inside #1	
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf	
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap	
			Row Length Adjustment= +1.50' x 7.45 sf x 1 rows	
		0.016 af	Total Available Storage	

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	80.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'
#2	Primary	82.00'	6.0" Round Culvert X 2.00 L= 25.0' Ke= 0.900
	•		Inlet / Outlet Invert= 82.00' / 81.00' S= 0.0400' /' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 0.20 sf

Discarded OutFlowMax=0.07 cfs @ 11.99 hrs HW=83.61' (Free Discharge) **1=Exfiltration** (Controls 0.07 cfs)

Primary OutFlowMax=1.74 cfs @ 11.99 hrs HW=83.60' (Free Discharge) 2=Culvert (Inlet Controls 1.74 cfs @ 4.42 fps)

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Pond 4-CUL: CULTEC RECHARGE - Chamber Wizard Field A

ChamberModel = CultecR-330XLHD(CultecRecharger®330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 1 rows

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length

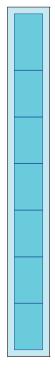
1 Rows x 52.0" Wide + 12.0" Side Stone x 2 = 6.33' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

7 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 1 Rows = 376.3 cf Chamber Storage

1,177.6 cf Field - 376.3 cf Chambers = 801.3 cf Stone x 40.0% Voids = 320.5 cf Stone Storage

Chamber Storage + Stone Storage = 696.8 cf = 0.016 af Overall Storage Efficiency = 59.2% Overall System Size = 52.50' x 6.33' x 3.54'

7 Chambers 43.6 cy Field 29.7 cy Stone

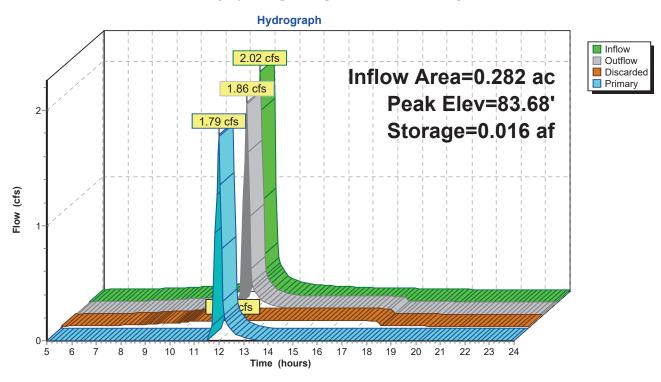




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Pond 4-CUL: CULTEC RECHARGE



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Summary for Pond 6AP: 4xLeach Pits

Inflow Area = 0.388 ac, 81.81% Impervious, Inflow Depth > 3.55" for 10-YR event

Inflow = 2.37 cfs @ 11.95 hrs, Volume= 0.115 af

Outflow = 0.14 cfs @ 12.67 hrs, Volume= 0.114 af, Atten= 94%, Lag= 43.3 min

Discarded = 0.14 cfs @ 12.67 hrs, Volume= 0.114 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 81.98'@ 12.67 hrs Surf.Area= 0.014 ac Storage= 0.050 af

Plug-Flow detention time=127.9 min calculated for 0.114 af (100% of inflow)

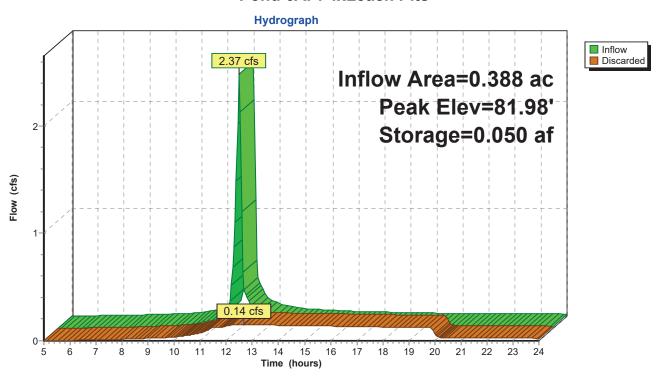
Center-of-Mass det. time=126.9 min (923.8 - 796.8)

Volume	Invert	Avail.Storage	Storage Description
#1	76.00'	0.069 af	14.00'D x 12.00'H 4' Stone Surround 4
			0.170 af Overall - 0.031 af Embedded = 0.138 af x 50.0% Voids
#2	76.00'	0.031 af	6.00'D x 12.00'H Vertical Cone/Cylinder 4 Inside #1
		0.100 af	Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	76.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'

Discarded OutFlowMax=0.14 cfs @ 12.67 hrs HW=81.98' (Free Discharge) **1=Exfiltration** (Controls 0.14 cfs)

Pond 6AP: 4xLeach Pits



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Summary for Pond 6BP: 5xLeach Pits

Inflow Area = 0.625 ac, 59.51% Impervious, Inflow Depth > 2.34" for 10-YR event

Inflow = 1.71 cfs @ 12.11 hrs, Volume= 0.122 af

Outflow = 0.17 cfs @ 13.01 hrs, Volume= 0.122 af, Atten= 90%, Lag= 53.8 min

Discarded = 0.17 cfs @ 13.01 hrs, Volume= 0.122 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 84.92'@ 13.01 hrs Surf.Area= 0.018 ac Storage= 0.051 af

Plug-Flow detention time=117.3 min calculated for 0.122 af (100% of inflow)

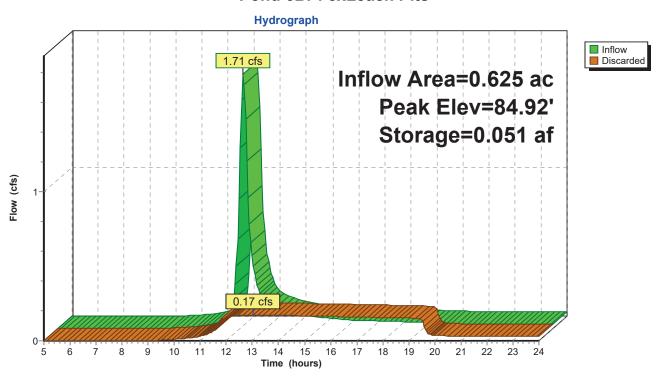
Center-of-Mass det. time=116.2 min (958.9 - 842.8)

Invert	Avail.Storage	Storage Description
80.00'	0.087 af	14.00'D x 12.00'H 4' Stone Surround 5
		0.212 af Overall - 0.039 af Embedded = 0.173 af x 50.0% Voids
80.00'	0.039 af	6.00'D x 12.00'H Vertical Cone/Cylinder 5 Inside #1
	0.125 af	Total Available Storage
	80.00'	80.00' 0.087 af 80.00' 0.039 af

Device	Routing	Invert	Outlet Devices
#1	Discarded	80.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'

Discarded OutFlowMax=0.17 cfs @ 13.01 hrs HW=84.92' (Free Discharge) 1=Exfiltration (Controls 0.17 cfs)

Pond 6BP: 5xLeach Pits



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Time span=5.00-24.00 hrs, dt=0.05 hrs, 381 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchmentl &2: OCEANPINES-POSTFLOW Runoff Area=6,195 sf 0.00% Impervious Runoff Depth>0.43" Flow Length=104' Tc=7.1 min CN=39 Runoff=0.04 cfs 0.005 af

Subcatchment3: WILDWOOD-POSTFLOWRunoff Area=7,030 sf 0.00% Impervious Runoff Depth>0.43"
Flow Length=48' Slope=0.1250 '/' Tc=5.7 min CN=39 Runoff=0.05 cfs 0.006 af

Subcatchment4-BYP:UNRESTRICTEDNORTH Runoff Area=24,134 sf 0.00% Impervious Runoff Depth>0.43" Flow Length=325' Tc=15.0 min CN=39 Runoff=0.11 cfs 0.020 af

Subcatchment4-HSE:BLDG4/5/6/7 Runoff Area=12,277 sf 100.00% Impervious Runoff Depth>5.51" Tc=5.0 min CN=98 Runoff=2.42 cfs 0.129 af

Subcatchment6A: WESTCB INFLOW

Runoff Area=16,884 sf 81.81% Impervious Runoff Depth>4.46"

Tc=5.0 min CN=87 Runoff=2.94 cfs 0.144 af

Subcatchment6B: MID CB INFLOWRunoff Area=27,241 sf 59.51% Impervious Runoff Depth>3.13"
Flow Length=374' Tc=18.2 min CN=74 Runoff=2.29 cfs 0.163 af

Reach4: NORTH Inflow=2.41 cfs 0.076 af Outflow=2.41 cfs 0.076 af

Pond 4-CUL:CULTECRECHARGE
Peak Elev=84.84' Storage=0.016 af Inflow=2.42 cfs 0.129 af
Discarded=0.07 cfs 0.073 af Primary=2.41 cfs 0.057 af Outflow=2.48 cfs 0.129 af

Pond 6AP: 4xLeachPits

Peak Elev=83.90' Storage=0.066 af Inflow=2.94 cfs 0.144 af
Outflow=0.15 cfs 0.144 af

Pond 6BP: 5xLeachPits

Peak Elev=87.16' Storage=0.075 af Inflow=2.29 cfs 0.163 af
Outflow=0.18 cfs 0.163 af

Total Runoff Area = 2.152 ac Runoff Volume = 0.467 af Average Runoff Depth = 2.60" 54.88% Pervious = 1.181 ac 45.12% Impervious = 0.971 ac

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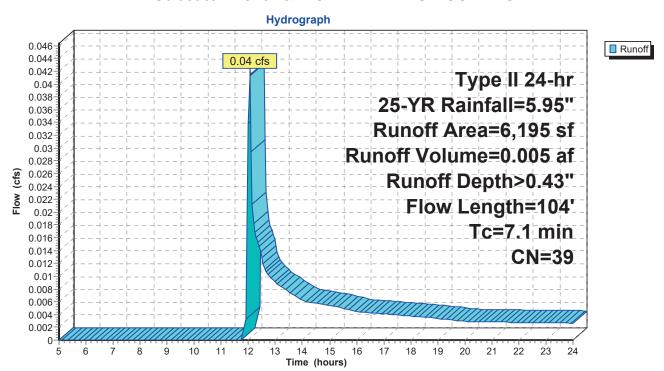
Summary for Subcatchment 1&2: OCEAN PINES-POST FLOW

Runoff = 0.04 cfs @ 12.04 hrs, Volume= 0.005 af, Depth> 0.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR Rainfall=5.95"

_	Aı	rea (sf)	CN D	escription				
	6,195 39 >75% Grass cover, Good, HSG A							
		6,195	1	00.00% P	ervious Are	ea		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
-	7.0	50	0.0800	0.12		Sheet Flow, A-B		
	0.1	54	0.3700	9.79		Grass: Bermuda n= 0.410 P2= 3.41" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps		
	7.1	104	Total					

Subcatchment 1&2: OCEAN PINES-POST FLOW



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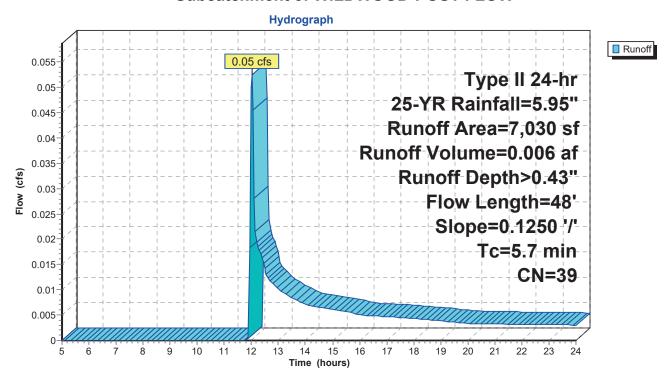
Summary for Subcatchment 3: WILDWOOD-POST FLOW

Runoff = 0.05 cfs @ 12.02 hrs, Volume= 0.006 af, Depth> 0.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR Rainfall=5.95"

A	rea (sf)	CN E	Description						
	7,030	39 >	39 >75% Grass cover, Good, HSG A						
	7,030	1	00.00% P	ervious Are	rea				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	/ Description				
5.7	48	0.1250	0.14		Sheet Flow, A-B				
					Grass: Bermuda n= 0.410 P2= 3.41"				

Subcatchment 3: WILDWOOD-POST FLOW



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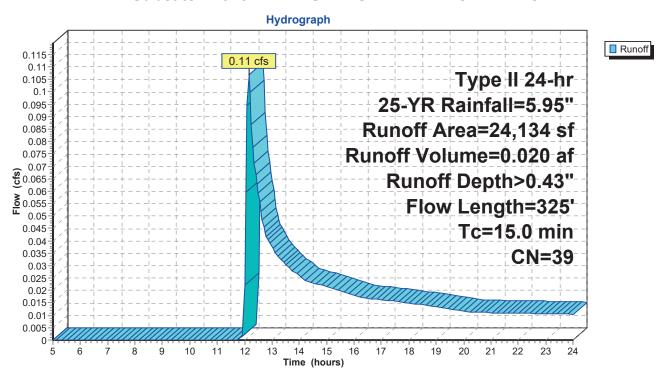
Summary for Subcatchment 4-BYP: UNRESTRICTED NORTH FLOW

Runoff = 0.11 cfs @ 12.16 hrs, Volume= 0.020 af, Depth> 0.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR Rainfall=5.95"

	Aı	rea (sf)	CN D	escription			
-		24,134				ood, HSG A	_
-	24,134 100.00% Pervious Area					,	_
	_						
	Tc	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		_
	13.7	50	0.0150	0.06		Sheet Flow, A-B	
						Grass: Bermuda n= 0.410 P2= 3.41"	
	1.3	275	0.0518	3.66		Shallow Concentrated Flow, B-C	
						Unpaved Kv= 16.1 fps	
_	15.0	325	Total				_

Subcatchment 4-BYP: UNRESTRICTED NORTH FLOW



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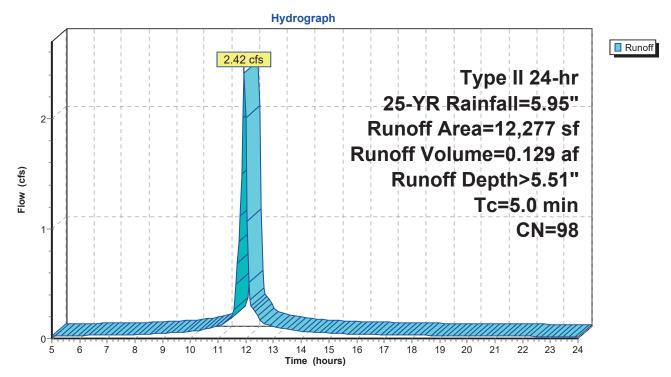
Summary for Subcatchment 4-HSE: BLDG 4/5/6/7

Runoff = 2.42 cfs @ 11.95 hrs, Volume= 0.129 af, Depth> 5.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR Rainfall=5.95"

Area (sf) CN	Description		
12,2				
12,2	77	100.00% In	npervious A	Area
Tc Ler (min) (fo	gth Slopet) (ft/	pe Velocity ft) (ft/sec)	Capacity (cfs)	Description
5.0				Direct Entry, DIRECT (MIN)

Subcatchment 4-HSE: BLDG 4/5/6/7



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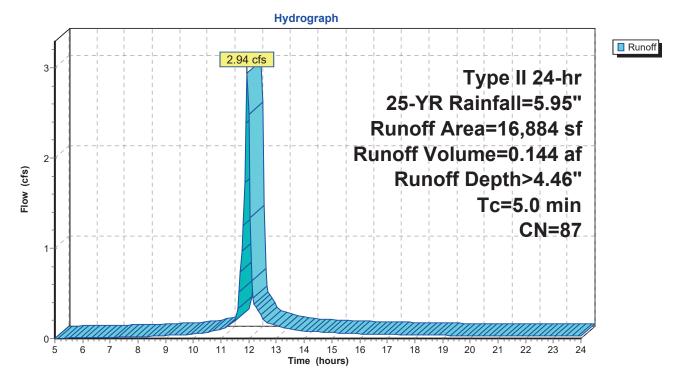
Summary for Subcatchment 6A: WEST CB INFLOW

Runoff = 2.94 cfs @ 11.95 hrs, Volume= 0.144 af, Depth> 4.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR Rainfall=5.95"

Area	(sf) CN						
5,	147 98	1					
3,	071 39	>75% Grass	>75% Grass cover, Good, HSG A				
8,	666 98	Roofs, HSG	iΑ				
16	884 87	Weighted A	verage				
3,	071	18.19% Per	vious Area				
13,	813	81.81% Imp	ervious Ar	ea			
Tc Le	ength Slo	ope Velocity	Capacity	Description			
(min)	feet) (f	ft/ft) (ft/sec)	(cfs)				
5.0				Direct Entry, DIRECT (MIN)			

Subcatchment 6A: WEST CB INFLOW



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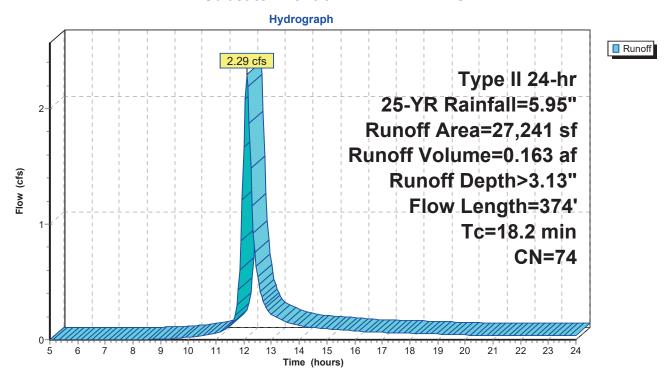
Summary for Subcatchment 6B: MID CB INFLOW

Runoff = 2.29 cfs @ 12.11 hrs, Volume= 0.163 af, Depth> 3.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-YR Rainfall=5.95"

	Aı	rea (sf)	CN E	escription		
		16,212			ing, HSG A	
		11,029	39 >	<u> 75% Gras</u>	s cover, Go	ood, HSG A
		27,241	74 V	Veighted A	verage	
		11,029	4	0.49% Pe	rvious Area	l .
		16,212	5	9.51% lm	pervious Ar	rea
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	16.1	50	0.0100	0.05		Sheet Flow, A-B
						Grass: Bermuda n= 0.410 P2= 3.41"
	0.1	27	0.1850	6.92		Shallow Concentrated Flow, B-C
						Unpaved Kv= 16.1 fps
	2.0	297	0.0155	2.53		Shallow Concentrated Flow, C-D
_						Paved Kv= 20.3 fps
	18.2	374	Total			

Subcatchment 6B: MID CB INFLOW



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Summary for Reach 4: NORTH

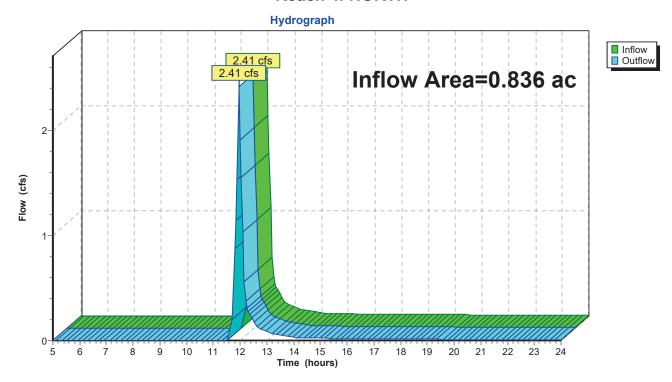
0.836 ac, 33.72% Impervious, Inflow Depth > 1.10" for 25-YR event Inflow Area =

Inflow 0.076 af

2.41 cfs @ 11.96 hrs, Volume= 2.41 cfs @ 11.96 hrs, Volume= Outflow 0.076 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs

Reach 4: NORTH



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Summary for Pond 4-CUL: CULTEC RECHARGE

Inflow Area = 0.282 ac,100.00% Impervious, Inflow Depth > 5.51" for 25-YR event
Inflow = 2.42 cfs @ 11.95 hrs, Volume= 0.129 af
Outflow = 2.48 cfs @ 11.96 hrs, Volume= 0.129 af, Atten= 0%, Lag= 0.4 min
Discarded = 0.07 cfs @ 11.96 hrs, Volume= 0.073 af
Primary = 2.41 cfs @ 11.96 hrs, Volume= 0.057 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 84.84'@ 11.96 hrs Surf.Area= 0.008 ac Storage= 0.016 af

Plug-Flow detention time=27.5 min calculated for 0.129 af (100% of inflow) Center-of-Mass det. time=27.0 min (786.2 - 759.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	80.00'	0.007 af	6.33'W x 52.50'L x 3.54'H Field A
			0.027 af Overall - 0.009 af Embedded = 0.018 af x 40.0% Voids
#2A	80.50'	0.009 af	Cultec R-330XLHDx 7 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 1 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	80.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'
#2	Primary	82.00'	6.0" Round Culvert X 2.00 L= 25.0' Ke= 0.900
	•		Inlet / Outlet Invert= 82.00' / 81.00' S= 0.0400' /' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 0.20 sf

Discarded OutFlowMax=0.07 cfs @ 11.96 hrs HW=84.72' (Free Discharge) **1=Exfiltration** (Controls 0.07 cfs)

Primary OutFlowMax=2.34 cfs @ 11.96 hrs HW=84.70' (Free Discharge) 2=Culvert (Inlet Controls 2.34 cfs @ 5.95 fps)

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Pond 4-CUL: CULTEC RECHARGE - Chamber Wizard Field A

ChamberModel = CultecR-330XLHD(CultecRecharger®330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 1 rows

7 Chambers/Row x 7.00' Long \pm 1.50' Row Adjustment \pm 50.50' Row Length \pm 12.0" End Stone x 2 \pm 52.50' Base Length

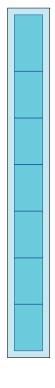
1 Rows x 52.0" Wide + 12.0" Side Stone x 2 = 6.33' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

7 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 1 Rows = 376.3 cf Chamber Storage

1,177.6 cf Field - 376.3 cf Chambers = 801.3 cf Stone x 40.0% Voids = 320.5 cf Stone Storage

Chamber Storage + Stone Storage = 696.8 cf = 0.016 af Overall Storage Efficiency = 59.2% Overall System Size = 52.50' x 6.33' x 3.54'

7 Chambers 43.6 cy Field 29.7 cy Stone

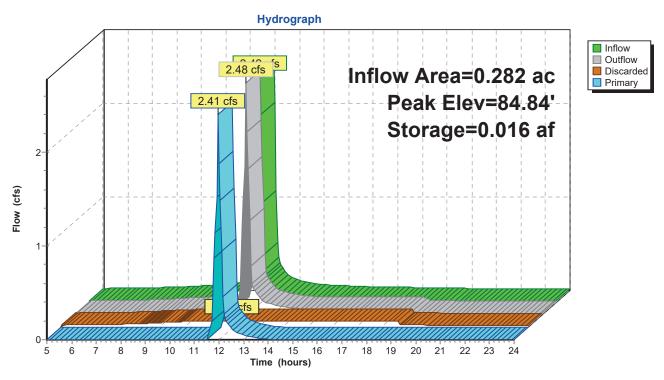




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Pond 4-CUL: CULTEC RECHARGE



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Summary for Pond 6AP: 4xLeach Pits

Inflow Area = 0.388 ac, 81.81% Impervious, Inflow Depth > 4.46" for 25-YR event

Inflow = 2.94 cfs @ 11.95 hrs, Volume= 0.144 af

Outflow = 0.15 cfs @ 12.89 hrs, Volume= 0.144 af, Atten= 95%, Lag= 56.0 min

Discarded = 0.15 cfs @ 12.89 hrs, Volume= 0.144 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 83.90'@ 12.89 hrs Surf.Area= 0.014 ac Storage= 0.066 af

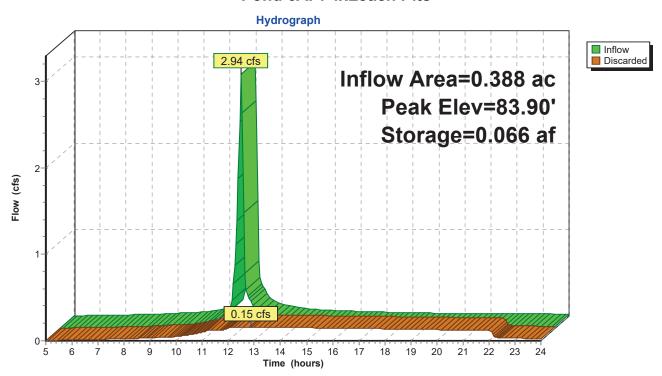
Plug-Flow detention time=167.4 min calculated for 0.144 af (100% of inflow) Center-of-Mass det. time=166.4 min (957.1 - 790.7)

Volume	Invert	Avail.Storage	Storage Description
#1	76.00'	0.069 af	14.00'D x 12.00'H 4' Stone Surround 4
			0.170 af Overall - 0.031 af Embedded = 0.138 af x 50.0% Voids
#2	76.00'	0.031 af	6.00'D x 12.00'H Vertical Cone/Cylinder 4 Inside #1
		0.100 af	Total Available Storage
Davidaa	Davidina	lance and Occ	Alak Davida a

Device	Routing	Invert	Outlet Devices
#1	Discarded	76.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'

Discarded OutFlowMax=0.15 cfs @ 12.89 hrs HW=83.90' (Free Discharge) **1=Exfiltration** (Controls 0.15 cfs)

Pond 6AP: 4xLeach Pits



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Summary for Pond 6BP: 5xLeach Pits

Inflow Area = 0.625 ac, 59.51% Impervious, Inflow Depth > 3.13" for 25-YR event

Inflow = 2.29 cfs @ 12.11 hrs, Volume= 0.163 af

Outflow = 0.18 cfs @ 13.27 hrs, Volume= 0.163 af, Atten= 92%, Lag= 69.6 min

Discarded = 0.18 cfs @ 13.27 hrs, Volume= 0.163 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 87.16'@ 13.27 hrs Surf.Area= 0.018 ac Storage= 0.075 af

Plug-Flow detention time=172.3 min calculated for 0.163 af (100% of inflow)

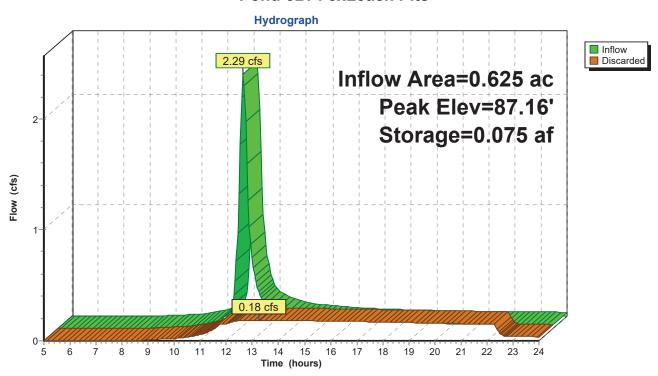
Center-of-Mass det. time=171.2 min (1,005.7 - 834.6)

Invert	Avail.Storage	Storage Description
80.00'	0.087 af	14.00'D x 12.00'H 4' Stone Surround 5
		0.212 af Overall - 0.039 af Embedded = 0.173 af x 50.0% Voids
80.00'	0.039 af	6.00'D x 12.00'H Vertical Cone/Cylinder 5 Inside #1
	0.125 af	Total Available Storage
	80.00'	80.00' 0.087 af 80.00' 0.039 af

Device	Routing	Invert	Outlet Devices
#1	Discarded	80.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'

Discarded OutFlowMax=0.18 cfs @ 13.27 hrs HW=87.16' (Free Discharge) **1=Exfiltration** (Controls 0.18 cfs)

Pond 6BP: 5xLeach Pits



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Time span=5.00-24.00 hrs, dt=0.05 hrs, 381 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchmentl &2: OCEANPINES-POSTFLOW Runoff Area=6,195 sf 0.00% Impervious Runoff Depth>0.94" Flow Length=104' Tc=7.1 min CN=39 Runoff=0.16 cfs 0.011 af

Subcatchment3: WILDWOOD-POSTFLOW
Runoff Area=7,030 sf 0.00% Impervious Runoff Depth>0.94"
Flow Length=48' Slope=0.1250 '/' Tc=5.7 min CN=39 Runoff=0.20 cfs 0.013 af

Subcatchment4-BYP:UNRESTRICTEDNORTH Runoff Area=24,134 sf 0.00% Impervious Runoff Depth>0.93" Flow Length=325' Tc=15.0 min CN=39 Runoff=0.43 cfs 0.043 af

Subcatchment4-HSE:BLDG4/5/6/7 Runoff Area=12,277 sf 100.00% Impervious Runoff Depth>6.94" Tc=5.0 min CN=98 Runoff=3.03 cfs 0.163 af

Subcatchment6A: WESTCB INFLOW

Runoff Area=16,884 sf 81.81% Impervious Runoff Depth>5.91"

Tc=5.0 min CN=87 Runoff=3.83 cfs 0.191 af

Subcatchment6B: MID CB INFLOWRunoff Area=27,241 sf 59.51% Impervious Runoff Depth>4.43"
Flow Length=374' Tc=18.2 min CN=74 Runoff=3.24 cfs 0.231 af

Reach4: NORTH Inflow=3.19 cfs 0.123 af Outflow=3.19 cfs 0.123 af

Pond 4-CUL:CULTECRECHARGE
Peak Elev=86.60' Storage=0.016 af Inflow=3.03 cfs 0.163 af
Discarded=0.08 cfs 0.083 af Primary=3.11 cfs 0.080 af Outflow=3.19 cfs 0.163 af

Pond 6AP: 4xLeachPits

Peak Elev=87.06' Storage=0.093 af Inflow=3.83 cfs 0.191 af
Outflow=0.17 cfs 0.179 af

Pond 6BP: 5xLeachPits

Peak Elev=91.01' Storage=0.115 af Inflow=3.24 cfs 0.231 af
Outflow=0.20 cfs 0.204 af

Total Runoff Area = 2.152 ac Runoff Volume = 0.651 af Average Runoff Depth = 3.63" 54.88% Pervious = 1.181 ac 45.12% Impervious = 0.971 ac

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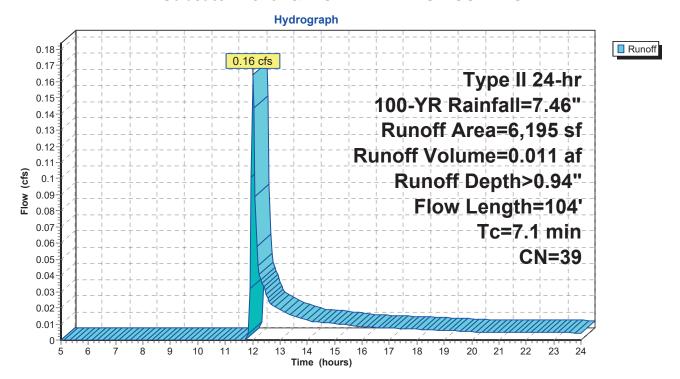
Summary for Subcatchment 1&2: OCEAN PINES-POST FLOW

Runoff = 0.16 cfs @ 12.01 hrs, Volume= 0.011 af, Depth> 0.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR Rainfall=7.46"

	Aı	rea (sf)	CN D	escription			
6,195 39 >75% Grass cover, Good, HSG A							
		6,195	1	00.00% P	ervious Are	ea	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
•	7.0	50	0.0800	0.12		Sheet Flow, A-B	
	0.1	54	0.3700	9.79		Grass: Bermuda n= 0.410 P2= 3.41" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps	
	7.1	104	Total				

Subcatchment 1&2: OCEAN PINES-POST FLOW



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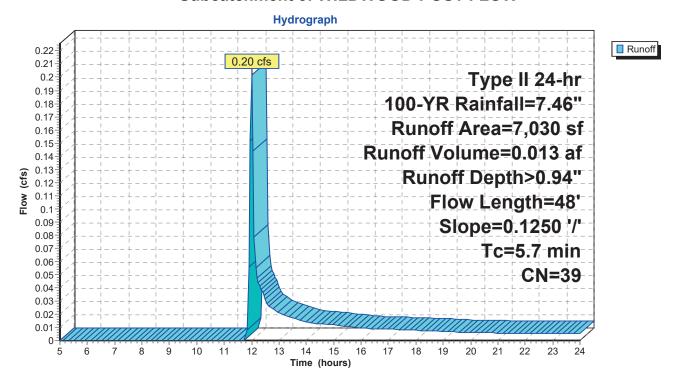
Summary for Subcatchment 3: WILDWOOD-POST FLOW

Runoff = 0.20 cfs @ 12.00 hrs, Volume= 0.013 af, Depth> 0.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR Rainfall=7.46"

_	Aı	rea (sf)	CN E	escription				
	7,030 39 >75% Grass cover, Good, HSG A							
	7,030 100.00% Pervious Area					ea		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_	5.7	48	0.1250	0.14		Sheet Flow, A-B Grass: Bermuda n= 0.410 P2= 3.41"		

Subcatchment 3: WILDWOOD-POST FLOW



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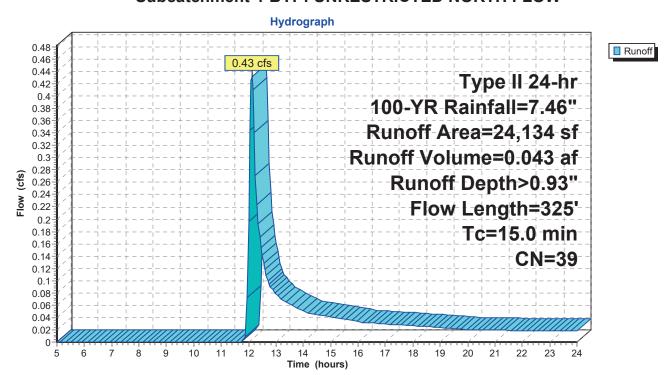
Summary for Subcatchment 4-BYP: UNRESTRICTED NORTH FLOW

Runoff = 0.43 cfs @ 12.12 hrs, Volume= 0.043 af, Depth> 0.93"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR Rainfall=7.46"

	Aı	rea (sf)	CN D	escription			
-		24,134				ood, HSG A	_
24,134 100.00% Pervious Are						,	_
	_				_		
	Tc	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		_
	13.7	50	0.0150	0.06		Sheet Flow, A-B	
						Grass: Bermuda n= 0.410 P2= 3.41"	
	1.3	275	0.0518	3.66		Shallow Concentrated Flow, B-C	
						Unpaved Kv= 16.1 fps	
_	15.0	325	Total				_

Subcatchment 4-BYP: UNRESTRICTED NORTH FLOW



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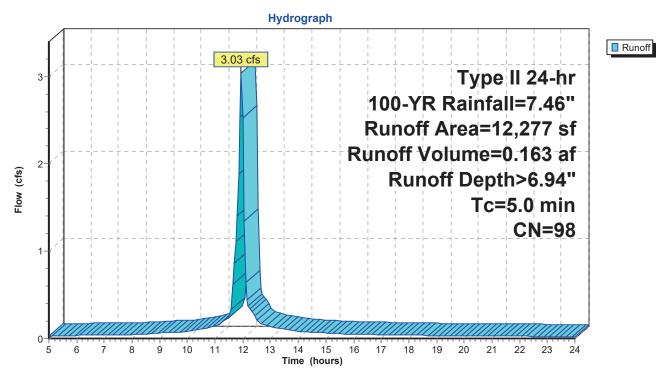
Summary for Subcatchment 4-HSE: BLDG 4/5/6/7

Runoff = 3.03 cfs @ 11.95 hrs, Volume= 0.163 af, Depth> 6.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR Rainfall=7.46"

Area (sf) CN	Description		
12,2	77 98	Roofs, HSC	A S	
12,2	77	100.00% In	npervious A	Area
Tc Ler (min) (f	ngth Slo eet) (ft/		Capacity (cfs)	Description
5.0				Direct Entry, DIRECT (MIN)

Subcatchment 4-HSE: BLDG 4/5/6/7



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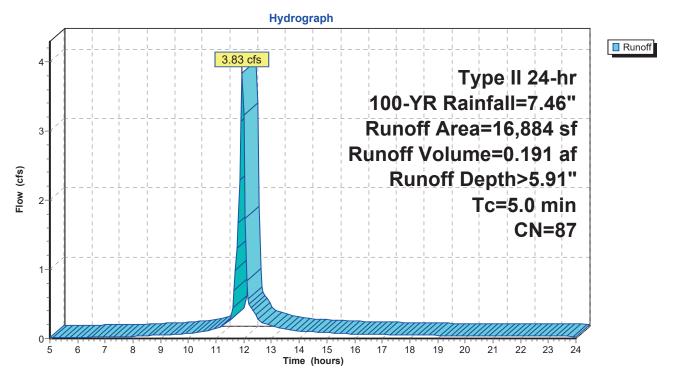
Summary for Subcatchment 6A: WEST CB INFLOW

Runoff = 3.83 cfs @ 11.95 hrs, Volume= 0.191 af, Depth> 5.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR Rainfall=7.46"

Area	(sf) CN	Description					
5,	147 98	Paved parki	aved parking, HSG A				
3,	071 39	>75% Grass	75% Grass cover, Good, HSG A				
8,	666 98	Roofs, HSG	oofs, HSG A				
16	884 87	Weighted A	verage				
3,	,071 18.19% Pervious Area						
13,	813	81.81% Imp	81.81% Impervious Area				
Tc Le	ength Slo	ope Velocity	Capacity	Description			
(min)	feet) (f	ft/ft) (ft/sec)	(cfs)				
5.0				Direct Entry, DIRECT (MIN)			

Subcatchment 6A: WEST CB INFLOW



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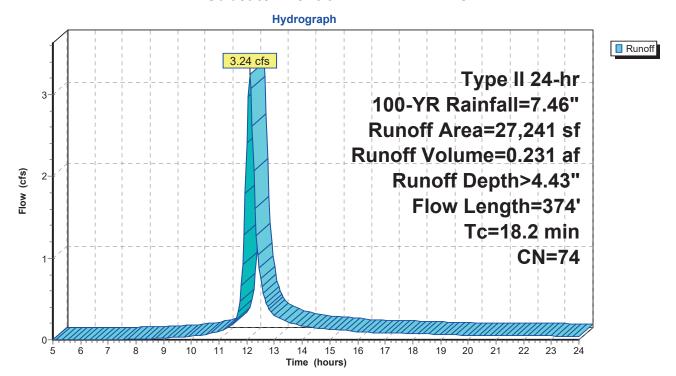
Summary for Subcatchment 6B: MID CB INFLOW

Runoff = 3.24 cfs @ 12.11 hrs, Volume= 0.231 af, Depth> 4.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-YR Rainfall=7.46"

	Α	rea (sf)	CN [Description					
	16,212 98 Paved parking, HSG A 11,029 39 >75% Grass cover, Good, HSG A								
_		11,029	39 >	•75% Gras	s cover, Go	ood, HSG A			
27,241 74 Weighted Average									
		11,029	4	0.49% Pe	rvious Area	1			
		16,212		9.51% Imp	pervious Ar	rea			
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	16.1	50	0.0100	0.05		Sheet Flow, A-B			
						Grass: Bermuda n= 0.410 P2= 3.41"			
	0.1	27	0.1850	6.92		Shallow Concentrated Flow, B-C			
						Unpaved Kv= 16.1 fps			
	2.0	297	0.0155	2.53		Shallow Concentrated Flow, C-D			
_						Paved Kv= 20.3 fps			
	18 2	374	Total						

Subcatchment 6B: MID CB INFLOW



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Summary for Reach 4: NORTH

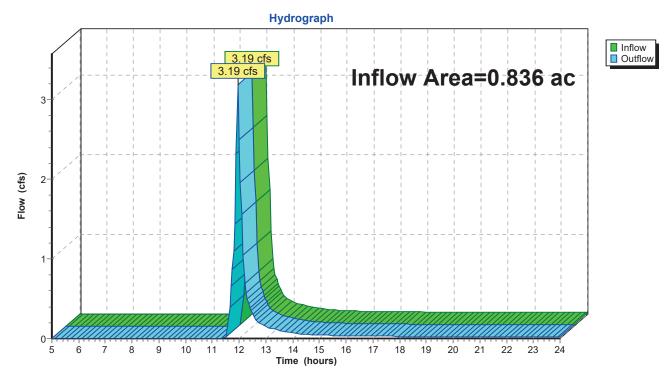
0.836 ac, 33.72% Impervious, Inflow Depth > 1.77" for 100-YR event Inflow Area =

Inflow 0.123 af

3.19 cfs @ 11.95 hrs, Volume= 3.19 cfs @ 11.95 hrs, Volume= Outflow 0.123 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs

Reach 4: NORTH



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Summary for Pond 4-CUL: CULTEC RECHARGE

Inflow Area = 0.282 ac,100.00% Impervious, Inflow Depth > 6.94" for 100-YR event
Inflow = 3.03 cfs @ 11.95 hrs, Volume= 0.163 af
Outflow = 3.19 cfs @ 11.95 hrs, Volume= 0.163 af, Atten= 0%, Lag= 0.0 min
Discarded = 0.08 cfs @ 11.95 hrs, Volume= 0.083 af
Primary = 3.11 cfs @ 11.95 hrs, Volume= 0.080 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 86.60'@ 11.95 hrs Surf.Area= 0.008 ac Storage= 0.016 af

Plug-Flow detention time=27.5 min calculated for 0.163 af (100% of inflow) Center-of-Mass det. time=27.1 min (785.4 - 758.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	80.00'	0.007 af	6.33'W x 52.50'L x 3.54'H Field A
			0.027 af Overall - 0.009 af Embedded = 0.018 af x 40.0% Voids
#2A	80.50'	0.009 af	Cultec R-330XLHDx 7 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 1 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	80.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'
#2	Primary	82.00'	6.0" Round Culvert X 2.00 L= 25.0' Ke= 0.900
	•		Inlet / Outlet Invert= 82.00' / 81.00' S= 0.0400' /' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 0.20 sf

Discarded OutFlowMax=0.08 cfs @ 11.95 hrs HW=86.59' (Free Discharge) **1=Exfiltration** (Controls 0.08 cfs)

Primary OutFlowMax=3.11 cfs @ 11.95 hrs HW=86.59' (Free Discharge) —2=Culvert (Inlet Controls 3.11 cfs @ 7.92 fps)

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Pond 4-CUL: CULTEC RECHARGE - Chamber Wizard Field A

ChamberModel = CultecR-330XLHD(CultecRecharger®330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 1 rows

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length

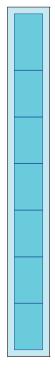
1 Rows x 52.0" Wide + 12.0" Side Stone x 2 = 6.33' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

7 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 1 Rows = 376.3 cf Chamber Storage

1,177.6 cf Field - 376.3 cf Chambers = 801.3 cf Stone x 40.0% Voids = 320.5 cf Stone Storage

Chamber Storage + Stone Storage = 696.8 cf = 0.016 af Overall Storage Efficiency = 59.2% Overall System Size = 52.50' x 6.33' x 3.54'

7 Chambers 43.6 cy Field 29.7 cy Stone

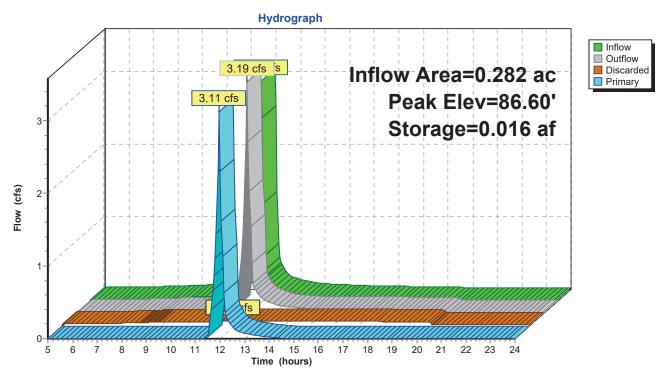




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Pond 4-CUL: CULTEC RECHARGE



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Summary for Pond 6AP: 4xLeach Pits

Inflow Area = 0.388 ac, 81.81% Impervious, Inflow Depth > 5.91" for 100-YR event

Inflow = 3.83 cfs @ 11.95 hrs, Volume= 0.191 af

Outflow = 0.17 cfs @ 13.11 hrs, Volume= 0.179 af, Atten= 96%, Lag= 69.3 min

Discarded = 0.17 cfs @ 13.11 hrs, Volume= 0.179 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 87.06'@ 13.11 hrs Surf.Area= 0.014 ac Storage= 0.093 af

Plug-Flow detention time=232.2 min calculated for 0.179 af (94% of inflow)

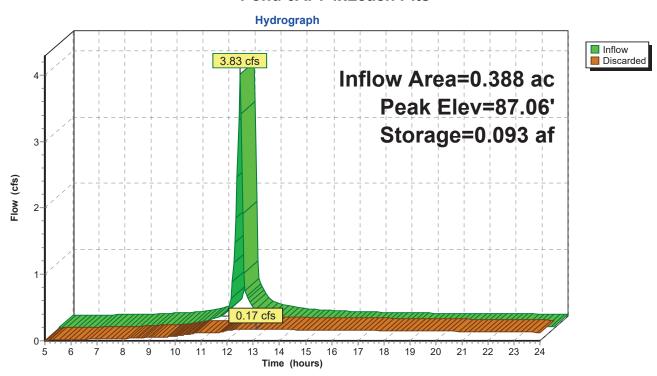
Center-of-Mass det. time=198.2 min (982.1 - 783.9)

Volume	Invert	Avail.Storage	Storage Description
#1	76.00'	0.069 af	14.00'D x 12.00'H 4' Stone Surround 4
			0.170 af Overall - 0.031 af Embedded = 0.138 af x 50.0% Voids
#2	76.00'	0.031 af	6.00'D x 12.00'H Vertical Cone/Cylinder 4 Inside #1
		0.100 af	Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	76.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'

Discarded OutFlowMax=0.17 cfs @ 13.11 hrs HW=87.06' (Free Discharge) —1=Exfiltration (Controls 0.17 cfs)

Pond 6AP: 4xLeach Pits



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Summary for Pond 6BP: 5xLeach Pits

Inflow Area = 0.625 ac, 59.51% Impervious, Inflow Depth > 4.43" for 100-YR event

Inflow = 3.24 cfs @ 12.11 hrs, Volume= 0.231 af

Outflow = 0.20 cfs @ 13.64 hrs, Volume= 0.204 af, Atten= 94%, Lag= 91.9 min

Discarded = 0.20 cfs @ 13.64 hrs, Volume= 0.204 af

Routing by Stor-Ind method, Time Span= 5.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 91.01'@ 13.64 hrs Surf.Area= 0.018 ac Storage= 0.115 af

Plug-Flow detention time=257.0 min calculated for 0.204 af (88% of inflow)

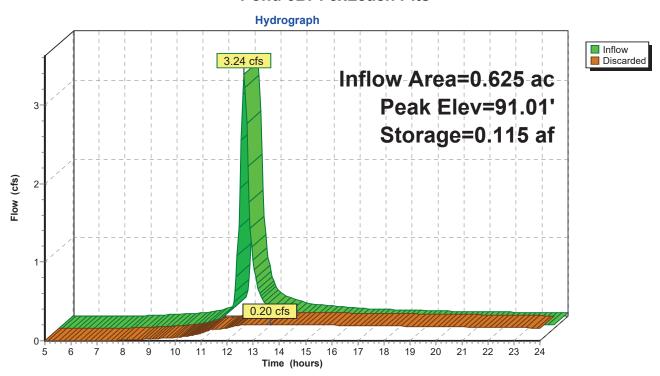
Center-of-Mass det. time=200.9 min (1,025.7 - 824.8)

Volume	Invert	Avail.Storage	Storage Description
#1	80.00'	0.087 af	14.00'D x 12.00'H 4' Stone Surround 5
			0.212 af Overall - 0.039 af Embedded = 0.173 af x 50.0% Voids
#2	80.00'	0.039 af	6.00'D x 12.00'H Vertical Cone/Cylinder 5 Inside #1
		0.125 af	Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	80.00'	8.270 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 50.00'

Discarded OutFlowMax=0.20 cfs@ 13.64 hrs HW=91.01' (Free Discharge) **1=Exfiltration** (Controls 0.20 cfs)

Pond 6BP: 5xLeach Pits





Stormwater Recharge Volume Calculations

Subcatchment 4

Area Impervious = A_1 = 12,277 sf (0.282 ac)

Roofs: 0.282 Acres
TOTAL: 0.282 Acres

All development within HSG A = 0.60"

 $Re_{Vol} = 0.60'' \times A_{I} = 0.60'' \times 1 \text{ ft} / 12'' \times 12,277 \text{ sf} = 613.85 \text{ cf}$

 $Re_{VReq'd}$ =**614 cf**

Recharge Volume Provided = 696 cf (cultec)

 $Re_V 696 cf > Re_{V Req's} 614 cf : OK$

Subcatchment 6A

Area Impervious = A_i = 13,813 sf (0.317 ac)

Roofs: 0.199 Acres Parking: 0.118 Acres **TOTAL: 0.317 Acres**

All development within HSG A = 0.60"

 Re_{Vol} = 0.60" x A_i= 0.60" x 1ft/12" x 13,813 sf= 690.65 cf

 $Re_{VReq'd}$ =**691 cf**

Recharge Volume Provided = 4,356 cf (drywells)

 $Re_V 4,356 cf > Re_{V Req's} 691 cf : OK$

Subcatchment 6B

Area Impervious = A_i = 16,212 sf (0.372 ac)

Parking: 0.372 Acres **TOTAL: 0.372 Acres**

All development within HSG A = 0.60"

 Re_{Vol} = 0.60" x A_i = 0.60" x 1ft/12" x 16,212 sf= 810.60 cf

Re_{V Reg'd}=**811 cf**

Recharge Volume Provided = 5,445 cf (drywells)

 Re_V 5,445 cf > $Re_{VReq's}$ 811 cf : OK

INSTRUCTIONS:

Version 1, Automated: Mar. 4, 2008

- In BMP Column, click on Blue Cell to Activate Drop Down Menu
 Select BMP from Drop Down Menu
 After BMP is selected, TSS Removal and other Columns are automatically completed.

	Location:	61 Wildwood Lane, Bourne			
	В	С	D	E	F
	4	TSS Removal	Starting TSS	Amount	Remaining
	BMP ¹	Rate ¹	Load*	Removed (C*D)	Load (D-E)
,	Street Sweeping - 10%	0.10	1.00	0.10	0.90
oval	Deep Sump and Hooded Catch Basin	0.25	0.90	0.23	0.68
TSS Removal	Dry Well	0.80	0.68	0.54	0.14
TSS		0.00	0.14	0.00	0.14
(Ca	0.00	0.14	0.00	0.14
			SS Removal =	87%	Separate Form Needs to be Completed for Each Outlet or BMP Train
	Froject.	1292			
	Prepared By:			*Equals remaining load from	n previous BMP (E)
	Date:	1/3/2024		which enters the BMP	



NOAA Atlas 14, Volume 10, Version 3 Location name: Sagamore Beach, Massachusetts, USA*

Latitude: 41.7895°, Longitude: -70.5398° Elevation: 98.46 ft** * source: ESRI Maps



* source: ESRI Maps
** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-k	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹									
Duration				Average	recurrence	interval (ye	ears)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.289 (0.235-0.352)	0.360 (0.293-0.440)	0.477 (0.387-0.584)	0.574 (0.463-0.706)	0.708 (0.552-0.906)	0.807 (0.616-1.05)	0.913 (0.678-1.23)	1.04 (0.722-1.41)	1.23 (0.820-1.72)	1.39 (0.904-1.97)
10-min	0.409 (0.334-0.499)	0.511 (0.416-0.623)	0.677 (0.549-0.828)	0.814 (0.657-1.00)	1.00 (0.782-1.28)	1.14 (0.873-1.49)	1.29 (0.961-1.75)	1.47 (1.02-2.00)	1.74 (1.16-2.43)	1.97 (1.28-2.79)
15-min	0.482 (0.392-0.587)	0.601 (0.489-0.733)	0.795 (0.645-0.974)	0.957 (0.771-1.18)	1.18 (0.920-1.51)	1.34 (1.03-1.75)	1.52 (1.13-2.06)	1.73 (1.20-2.35)	2.05 (1.37-2.86)	2.32 (1.51-3.29)
30-min	0.693 (0.565-0.846)	0.863 (0.703-1.05)	1.14 (0.925-1.40)	1.37 (1.11-1.69)	1.69 (1.32-2.16)	1.93 (1.47-2.51)	2.18 (1.62-2.94)	2.48 (1.72-3.37)	2.93 (1.96-4.10)	3.32 (2.16-4.71)
60-min	0.905 (0.738-1.10)	1.13 (0.916-1.37)	1.49 (1.21-1.82)	1.79 (1.44-2.20)	2.20 (1.71-2.81)	2.50 (1.91-3.27)	2.83 (2.11-3.83)	3.23 (2.24-4.38)	3.82 (2.55-5.33)	4.32 (2.81-6.13)
2-hr	1.22 (1.00-1.48)	1.52 (1.25-1.84)	2.01 (1.64-2.44)	2.42 (1.96-2.95)	2.97 (2.34-3.78)	3.39 (2.61-4.39)	3.83 (2.88-5.15)	4.38 (3.07-5.89)	5.20 (3.50-7.19)	5.91 (3.89-8.30)
3-hr	1.44 (1.19-1.74)	1.79 (1.47-2.16)	2.35 (1.93-2.85)	2.82 (2.30-3.43)	3.46 (2.74-4.38)	3.94 (3.05-5.08)	4.46 (3.37-5.95)	5.08 (3.59-6.80)	6.03 (4.09-8.29)	6.85 (4.54-9.56)
6-hr	1.88 (1.56-2.26)	2.30 (1.90-2.75)	2.97 (2.46-3.57)	3.54 (2.90-4.26)	4.31 (3.43-5.40)	4.88 (3.81-6.22)	5.50 (4.18-7.24)	6.23 (4.44-8.25)	7.33 (5.02-9.97)	8.26 (5.53-11.4)
12-hr	2.39 (2.00-2.85)	2.86 (2.38-3.40)	3.62 (3.01-4.32)	4.25 (3.51-5.09)	5.12 (4.10-6.34)	5.77 (4.53-7.26)	6.45 (4.92-8.36)	7.24 (5.22-9.48)	8.37 (5.81-11.3)	9.31 (6.31-12.7)
24-hr	2.89 (2.43-3.41)	(2.87-4.03)	4.26 (3.57-5.05)	4.98 (4.14-5.92)	5.95 (4.80-7.30)	6.69 (5.29-8.33)	7.46 (5.72-9.53)	8.31 (6.05-10.8)	9.50 (6.66-12.6)	(7.16-14.1)
2-day	3.33 (2.82-3.90)	3.93 (3.33-4.61)	4.91 (4.15-5.78)	5.73 (4.81-6.76)	6.85 (5.57-8.32)	7.70 (6.13-9.49)	8.58 (6.63-10.8)	9.54 (7.03-12.2)	10.9 (7.72-14.3)	12.0 (8.29-16.0)
3-day	3.65 (3.11-4.26)	4.28 (3.64-5.00)	5.31 (4.50-6.21)	6.16 (5.19-7.24)	7.33 (5.99-8.87)	8.22 (6.58-10.1)	9.14 (7.10-11.5)	10.1 (7.51-12.9)	11.5 (8.23-15.1)	12.6 (8.80-16.7)
4-day	3.93 (3.36-4.58)	4.57 (3.90-5.33)	5.62 (4.78-6.56)	6.49 (5.49-7.60)	7.69 (6.30-9.26)	8.60 (6.90-10.5)	9.53 (7.43-11.9)	10.5 (7.84-13.4)	11.9 (8.55-15.5)	13.0 (9.12-17.2)
7-day	4.67 (4.01-5.40)	5.33 (4.58-6.17)	6.42 (5.49-7.45)	7.32 (6.23-8.52)	8.56 (7.06-10.2)	9.52 (7.68-11.5)	10.5 (8.20-12.9)	11.5 (8.62-14.5)	12.8 (9.28-16.5)	13.8 (9.79-18.1)
10-day	5.35 (4.61-6.16)	6.04 (5.20-6.96)	7.17 (6.15-8.28)	8.10 (6.92-9.40)	9.39 (7.77-11.1)	10.4 (8.42-12.5)	11.4 (8.94-13.9)	12.4 (9.36-15.5)	13.7 (9.99-17.6)	14.7 (10.5-19.1)
20-day	7.36 (6.40-8.42)	8.15 (7.07-9.33)	9.43 (8.16-10.8)	10.5 (9.04-12.1)	12.0 (9.98-14.1)	13.1 (10.7-15.6)	14.2 (11.2-17.2)	15.3 (11.7-19.0)	16.6 (12.3-21.1)	17.6 (12.7-22.6)
30-day	9.06 (7.91-10.3)	9.93 (8.66-11.3)	11.4 (9.87-13.0)	12.5 (10.8-14.4)	14.2 (11.9-16.5)	15.4 (12.7-18.2)	16.7 (13.2-20.0)	17.8 (13.7-21.9)	19.2 (14.3-24.1)	20.1 (14.6-25.7)
45-day	11.2 (9.83-12.7)	12.2 (10.7-13.8)	13.8 (12.0-15.7)	15.1 (13.1-17.2)	16.9 (14.2-19.6)	18.4 (15.1-21.5)	19.7 (15.7-23.4)	20.9 (16.2-25.6)	22.3 (16.7-27.9)	23.3 (17.0-29.5)
60-day	13.0 (11.5-14.8)	14.1 (12.4-16.0)	15.8 (13.9-17.9)	17.3 (15.0-19.6)	19.2 (16.3-22.2)	20.8 (17.2-24.3)	22.3 (17.8-26.3)	23.5 (18.3-28.7)	25.0 (18.8-31.1)	25.9 (19.1-32.7)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical

1 of 4 11/9/2022, 9:31 AM

04627540

0847294

70° 32' 33" W

4627720

41° 47' 28" N

0997294

0097294

N. 35. 33. M

41° 47' 16" N

0247294

Web Soil Survey National Cooperative Soil Survey

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1 25,000

contrasting soils that could have been shown at a more detailed Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of Warning: Soil Map may not be valid at this scale.

Please rely on the bar scale on each map sheet for map measurements.

scale.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Barnstable County, Massachusetts Survey Area Data: Version 19, Sep 9, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Sep 5, 2020—Sep 7,

Not rated or not available

B/D

S

Soil Rating Points

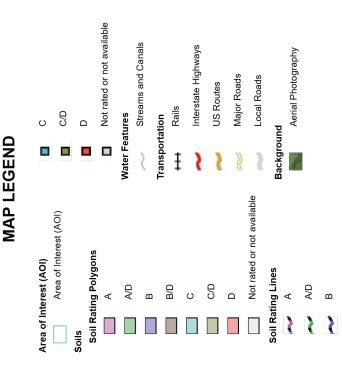
⋖

ΑD

B/D

В

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.





USDA

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
380B	Nantucket sandy loam, 3 to 8 percent slopes	В	11.8	38.3%
430B	Barnstable sandy loam, 3 to 8 percent slopes	А	5.1	16.4%
430C	Barnstable sandy loam, 8 to 15 percent slopes	А	6.6	21.5%
435C	Plymouth loamy coarse sand, 8 to 15 percent slopes	A	4.5	14.6%
435D	Plymouth loamy coarse sand, 15 to 35 percent slopes	A	2.8	9.2%
Totals for Area of Interest			30.8	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

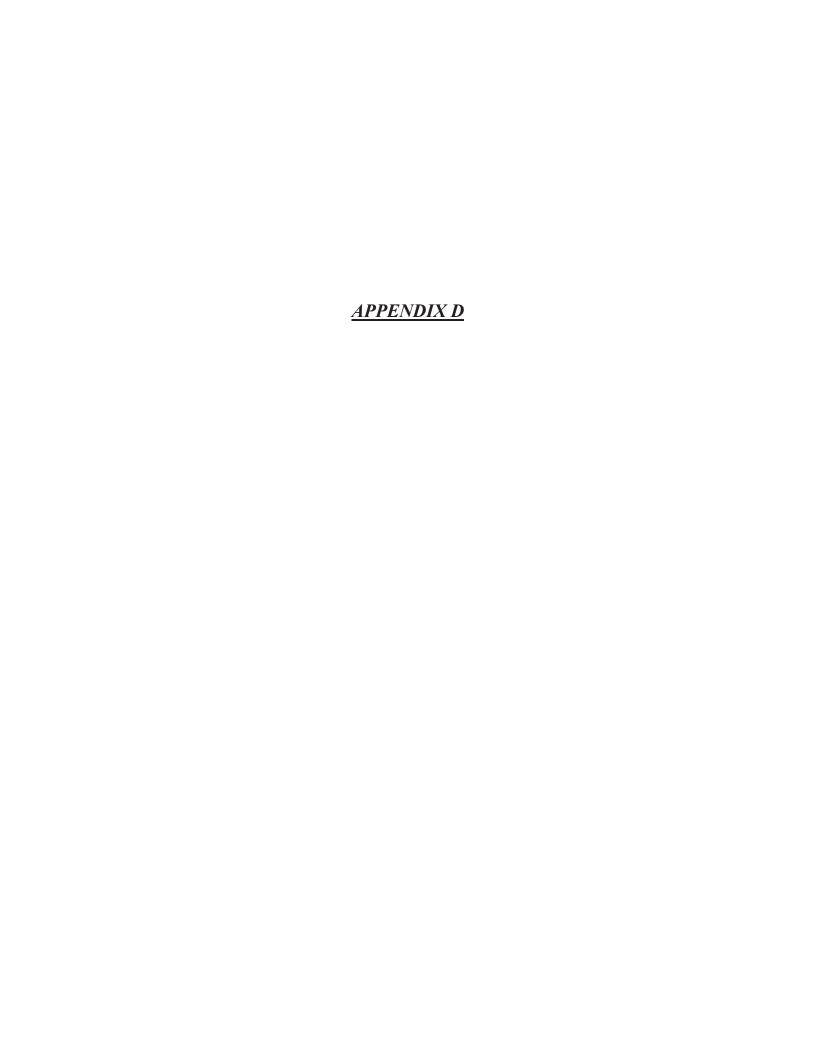
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan

for

Wildwood Lane- Lot 61

Bourne, Massachusetts

Prepared for:

Ocean Dunes, LLC 498 Newtown Road Littleton, Massachusetts 01460

Prepared by:

Existing Grade, Inc. 62 Riedell Road Douglas, Massachusetts 01516

> January 03, 2024 EGI Project No. 1292

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- 1. Introduction
- 2. Project Narrative
- 3. Erosion and Sedimentation Control Best Management Practices (BMPs)
- 4. Construction Sequencing Plan

1. Introduction

The erosion and sediment produced by the construction of the proposed development will be controlled on the property utilizing Erosion and Sedimentation Control Best Management Practices (BMPs). These practices are shown in detail on the Proposed Site Plans prepared by Existing Grade, Inc. These plans shall be hereinafter referred to as the "Site Plans".

The party responsible for the implementation, routine inspections and maintenance of the Erosion and Sedimentation Control BMPs shall be the Owner:

Ocean Dunes, LLC 498 Newtown Road Littleton, Massachusetts

2. Project Narrative

The proposent, Ocean Dunes, LLC, proposes to construct 7 townhouse style buildings (Lot 61 on the proposed site plans) for the property located at 61 Wildwood Lane, Bourne MA. The proposed project will include the construction of 7 new multifamily style townhouse buildings, one new pass through parking lot consisting of: bituminous concrete surface, asphalt sloped curbing, storm water management infrastructures inclusive of catch basins, drain manholes, pipe conveyance systems, and drywells as shown on the design plans. All of the proposed buildings will be tied into a total of 6 proposed septic systems with connections to town water via new mains through the property. The proposed project will be conducted per the Massachusetts Department of Environmental Protection requirements, Local Town and State bylaws, as well as using best management practices.

The property is listed by the Town of Bourne Assessor's Department as Lot 62, Parcel 99 on Assessors Map 7 and historically laid within the Residential 20 (R-20) zoning district at the time of original permitting based upon a review of records on file at the Town of Bourne Planning and Zoning Offices. The property is located within the FEMA Flood Zone X Area (area outside mapped flood plain) based upon a review of FIRM Map 25001C0316K, Panel 316 of 550, last revised July 06, 2021. Currently there is municipal water as well as underground electric telephone/ cable to service the property.

The property's address is recorded as 61 Wildwood Lane, Bourne MA and abuts Ocean Pines Road to the West, Wildwood Lane to the South, and dedicated open space parcels and private residential properties to the North and East. Access to the site is via proposed pass through driveway along Wildwood Lane to the South and Ocean Pines Road to the West. The existing site is comprised a cleared storage lot which was permitted under the original historic site plan approval.

The Barnstable County Soil Survey, issued by the US Department of Agriculture was referenced to determine the type and hydrologic group of the soils located on the property. The property is comprised of mostly hydrologic soil group A type soils, as confirmed via numerous percolation and soil tests for the property.

3. Erosion and Sedimentation Control Best Management Practices (BMPs)

A. Sediment Fence/Straw Wattle Barrier Controls

A sediment fence/straw wattle barrier combination will be constructed along disturbed downward slopes, along the limit of work boundary and other locations as shown on the Site Plans. The sediment fence portion will be up gradient of the straw wattle. This control BMP shall be installed prior to any disturbance on the property.

Specifications

Sediment fence shall be Amoco woven polypropylene 1198 or approved equivalent.

<u>Installation Requirements</u>

- 1. Straw wattle shall be installed as directed by the owner's representative in accordance to manufacturer's Installation Guidelines, Staking Pattern Guide, and CAD details. The extent of straw wattle shall be as shown on the project drawings.
- 2. Straw wattle should be installed to intercept water flow and collect sediment on site. They may be placed over bare soil or on top of erosion control blankets. Straw wattles are typically installed in a 2 inch trench with the ends of the wattle facing upstream.
- 3. They shall be secured to the subgrade by wood stakes every four lineal feet across the length of the straw wattle. The stakes shall be driven through the center of the straw wattle only and driven into the ground a minimum of 24 inches.
- 4. Straw wattle installed in a swale or channel bottom shall allow the installation to continue up the slopes three feet above the anticipated high water mark and perpendicular to the flow of water.
- 5. The sediment fence shall be installed up gradient of the hay bale in accordance with the detail as shown on the Site Plans.
- 6. Spacing of straw wattle shall be such that the elevation of the bottom of the straw wattle upstream will be equal to the elevation of the top of the straw wattle downstream.

- 7. Straw wattle shall remain in place until fully established vegetation and root systems are present.
- 8. The sediment fence shall be installed to the up gradient side of the support net in a continuous length with a minimum of twelve (12) inches of the fence placed along the bottom and down gradient face of the trench. Break joints in the sediment fence shall be overlapped in accordance with the detail as shown on the Site Plans with care taken to avoid break joints in low points along the barrier line.
- 9. The sediment fence/straw wattle barrier shall be entrench and backfilled. The trench should be excavated to a width of the proposed straw wattle width plus six (6) inches and to a depth between four (4) to six (6) inches. After the installation of the barrier, the barrier shall be backfilled with the down gradient fill conforming to the existing ground level and the up gradient fill built up a minimum of four (4) inches against the barrier.
- 10. The barriers should be removed when they have served their usefulness, but not before all upslope areas have been permanently stabilized and permission to remove the barrier has been approved by the Town of Auburn Conservation Commission.

Inspection and Maintenance

- 1. The sediment fence/straw wattle barrier shall be inspected weekly and after every rainfall event of one (1) inch or greater and at least daily during prolonged storm events.
- 2. Inspect the barrier system for any signs of down gradient erosion or breakout, sediment fence tears, depth of sediment and integrity of the barrier anchor system. All deficiencies shall be repaired or replaced immediately or over burden of sediment shall be removed.
- 3. The sediment deposits shall be removed after every storm event to reduce pressure on the barrier system and to provide adequate storage volume for the next storm event. Care shall be taken to avoid undermining the barrier system during removal operations.

B. Construction Entrance

A stabilized construction entrance shall be installed at the proposed development entrance off of the existing parking lot. The construction entrance shall be installed immediately after any clearing/grubbing operations and all cut/fill activities, required to provide access to the proposed site, has been completed. The purpose of the construction entrance is to keep mud and sediment from being tracked off of the construction site and into the existing parking lot.

The construction entrance shall be constructed in accordance with the detail and shown on the Site Plans.

Specifications

Filter fabric shall be Mirafi 140 N or approved equivalent. Stone shall be in accordance with the Massachusetts Highway Department Specifications.

<u>Installation Requirements</u>

- 1. Grade construction entrance to produce positive drainage toward temporary sedimentation controls on the property.
- 2. Stone for the construction entrance shall consist of two (2) to four (4) inch stone fill placed on the graded base.
- 3. The minimal length of the construction entrance should extend onto the site a minimum of fifty (50) feet and should have a width equal to the full width of the proposed roadway or twenty (20) feet, whichever is greater.
- 4. Place filter fabric shall be between the stone fill and the earth surface below to reduce the migration of soil particles from the underlying soil into the stone and vice versa.

Inspection and Maintenance

- 1. The construction entrance and sediment disposal area shall be inspected weekly and after every rainfall event of one (1) inch or greater.
- 2. Mud and sediment, tracked or washed onto public roads, shall be immediately removed by sweeping.
- 3. Provide periodic topdressing with additional stone to maintain the entrance in a condition that will prevent tracking or flowing of sediment onto public roads.

C. Temporary Sediment Basins

The Contractor shall construct temporary sediment basins where required to filter out sediment from stormwater until the permanent drainage system is functioning properly.

The temporary sediment basins shall be lined with sediment fence/straw wattle barrier controls. All stormwater runoff from disturbed areas shall be directed toward the temporary sediment basins prior to discharging from the site.

<u>Installation Requirements</u>

- 1. The sediment basins should be located as close to the sediment source as possible.
- 2. The sediment basins shall have a minimum length to width ratio of 2:1 and shall have minimum side slopes of 3:1.
- 3. The bottom of the sediment basin shall be lined with gravel/stone.
- 4. The sediment basin shall have a minimum storage volume of 3,600 cubic feet for each acre of disturbed drainage area.

Inspection and Maintenance

- 1. The sediment basins shall be inspected weekly and after every rainfall event of one (1) inch or greater.
- 2. Inspect the sediment basin for and settlement, seepage and erosion damage. All deficiencies shall be repaired or replaced immediately.
- 3. Remove and properly dispose of sediment when it accumulates to one-half (½) of the basin design volume. All trash and other debris shall be removed from the sediment basin on weekly basis.
- 4. Remove and replace gravel/stone when sediment basin does not drain properly.

D. Temporary Drainage Swales

The Contractor shall construct temporary drainage swales to transport stormwater runoff from the disturbed areas of the site to the temporary sediment basins. Check dams shall be utilized along the temporary drainage swales.

Installation Requirements

- 1. The temporary drainage swales cross-section shall be constructed with a top width between two (2) to four (4) feet and a minimum height of one and on-half (1½) feet. The side slopes of the swale shall be between 2:1 and 4:1.
- 2. The maximum channel grade shall be one and on-half $(1\frac{1}{2})$ percent and shall have a positive grade to the outlet.
- 3. The stormwater runoff shall outlet through check dams and into temporary sediment basins.

Inspection and Maintenance

- 1. The temporary drainage swales shall be inspected weekly and after every rainfall event of one (1) inch or greater.
- 2. Inspect the drainage swales for construction induced damage, settlement and erosion damage. All deficiencies shall be repaired or replaced immediately.
- 3. Remove and properly dispose of sediment when it accumulates into the flow area. All trash and other debris shall be removed from the drainage swale on weekly basis.

E. Temporary Check Dam

The Contractor shall install temporary check dams along the temporary drainage swales to lower the runoff velocities of stormwater flows to reduce erosion and promoting the settlement of sediments.

<u>Installation Requirements</u>

- 1. Check dams shall be constructed of anchored hay bales or other approved means with a small sump located immediately upstream of the check dam.
- 2. The hay bales shall be either wire or nylon bound or string-tied. String-tied bales shall be installed so that the bindings are orientated around the sides, rather than along the tops and bottoms, to prevent the deterioration of the bindings.
- 3. Each hay bale shall be anchored with a minimum of two (2) wood stakes or steel rebar with the first anchor driven toward the previously laid hay bale to force bales together. The anchors shall be driven deep enough into the ground to securely anchor the bales or to a minimum of eighteen (18) inches.

- 4. All gaps between hay bales shall be filled by wedging with straw, to prevent water from escaping between the bales, and should be done with care in order not to separate the hay bales.
- 5. The maximum spacing between check dams shall be that the toe of the up gradient dam is at the same elevation as the top of the down gradient dam.

Inspection and Maintenance

- 1. The check dams shall be inspected weekly and after every rainfall event of one (1) inch or greater.
- 2. Inspect the check dams for damage and erosion damage. All deficiencies shall be repaired or replaced immediately.
- 3. Remove and properly dispose of sediment when it accumulates to a depth of one-half the dam height. All trash and other debris shall be removed from the check dam sump on weekly basis.

F. Drainage System Inlet Protection

The Contractor shall install Siltsack or approved equivalent at catch basin grate locations to allow the drainage system to be utilized before final site stabilized as long as the infiltration basin is constructed and stabilized.

Specifications

Siltsack by ACF Environmental, Inc.

<u>Installation Requirements</u>

1. Siltsack should be installed at all catch basin grate locations in accordance with the manufacturer recommendations and specifications.

Inspection and Maintenance

- 1. Siltsacks shall be inspected weekly and after every rainfall event of one (1) inch or greater.
- 2. Inspect the siltsack for damage. All deficiencies shall be repaired or replaced immediately.

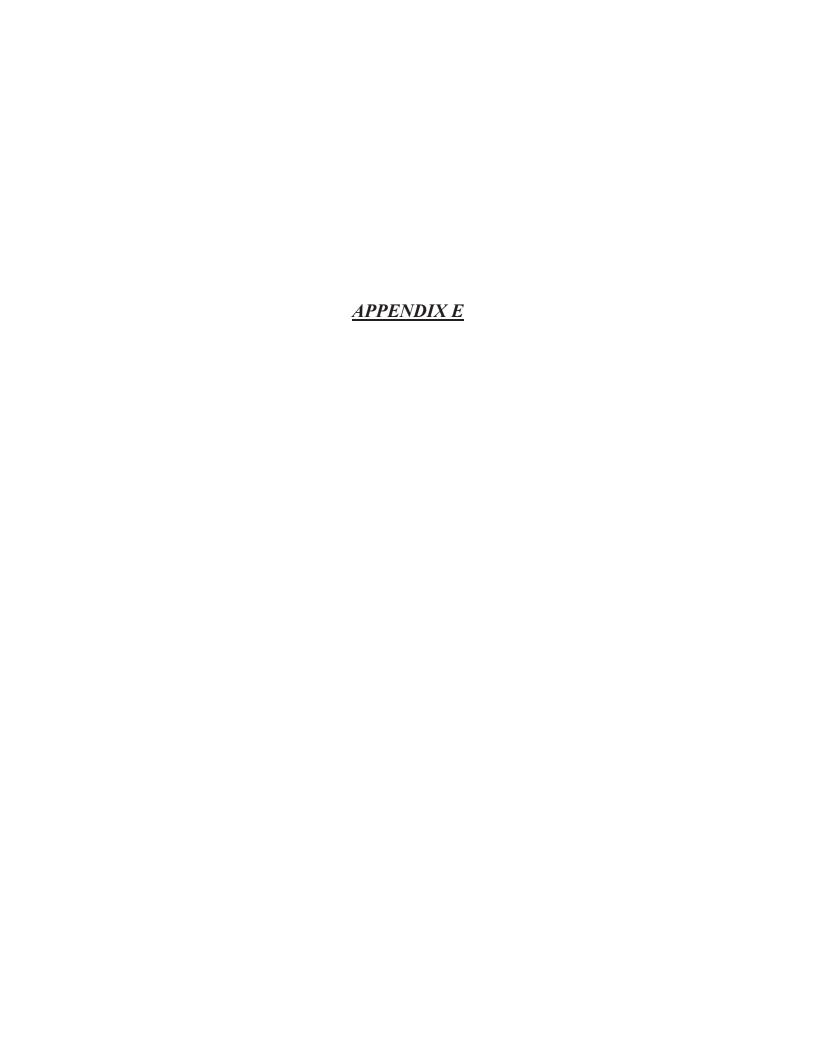
3. Remove and properly dispose of sediment when it accumulates to a depth of one-half the siltsack storage volume.

4. Construction Sequencing Plan

Anticipated Construction Schedule

- 1. Demarcate the proposed limit of work as well as trees and other buffer zone areas for protection.
- 2. Hold a pre-construction meeting a minimum of one (1) week prior to the start of construction.
- 3. Notify Dig-Safe to demarcate all underground utilities prior to start of construction.
- 4. Install sediment fence/straw wattle barrier at locations indicated on the Site Plans.
- 5. Construct all temporary drainage swales to collect and divert stormwater runoff from undisturbed areas of the site to bypass construction area.
- 6. Clear and construct temporary construction entrance.
- 7. Clear and grub all areas associated with the construction of the development.
- 8. Excavate topsoil and subsoil from cut areas, install erosion control barriers and stockpile soil on site. Consideration should be given to locating soil stockpiles on the up gradient side of disturbed areas, where possible, to act as temporary diversions.
- 9. Fill areas in twelve (12) inch lifts and compact to 95% standard proctor. Install slope protection or retaining walls with reinforcement, where required.
- 10. Rough grade the site.
- 11. Construct temporary drainage swales with check dams along the sides of the proposed roadway as well as all temporary sediment basins.
- 12. Construct fine grading of roadway.

- 13. Install closed drainage system and other utilities. Install Siltsack or approved equivalent at all catch basin grate locations.
- 14. Complete final grading of roadway with gravel sub base. Add additional erosion control measures as necessary.
- 15. Place the bituminous concrete binder course on roadways and sidewalk areas and permanently vegetate and landscape including the installation of trees. All slopes greater than 3:1 shall be stabilized with jute mesh.
- 16. Place final wearing surface of both the roadway and sidewalk.
- 17. After site is stabilized, remove all temporary measures and install permanent vegetation on all disturbed areas



POST-CONSTRUCTION STORM WATER OPERATIONS AND MAINTENANCE PLAN

GENERAL NOTES

- 1. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROPER INSPECTION AND MAINTENANCE OF ALL STORMWATER AND EROSION CONTROL FACILITIES UNTIL THE PROJECT CONSTRUCTION IS COMPLETED. THE CONTRACTOR SHALL CLEAN ALL COMPONENTS OF THE STORM WATER MANAGEMENT SYSTEM AND SWEEP ALL PAVED AREAS AT THE COMPLETION OF CONSTRUCTION, IMMEDIATELY PRIOR TO TURNING OVER OPERATION AND MAINTENANCE RESPONSIBILITY TO THE OWNER.
- 2. UPON COMPLETION OF CONSTRUCTION, THE OPERATION AND MAINTENANCE OF ALL COMPONENTS OF THE STORMWATER MANAGEMENT SYSTEM WILL BE THE RESPONSIBILITY OF THE OWNER:

Ocean Dunes, LLC

498 Newtown Road Littleton, Massachusetts

3. DISPOSAL OF ACCUMULATED SEDIMENT AND HYDROCARBONS TO BE IN ACCORDANCE WITH APPLICABLE LOCAL, STATE AND FEDERAL GUIDELINES AND REGULATIONS.

EROSION CONTROL BMPs

STREET SWEEPING:

ALL PAVED AREAS SHOULD BE SWEPT TWICE A MONTH DURING CONSTRUCTION AND TWO TIMES PER YEAR DURING THE EARLY SPRING AND LATE FALL SEASONS AFTER CONSTRUCTION.

INFILTRATION SYSTEMS:

INSPECT AFTER EVERY MAJOR STORM EVENT (1" OR GREATER) DURING CONSTRUCTION AND FOR TWELVE (12) MONTHS AFTER CONSTRUCTION TO ENSURE PROPER STABILIZATION AND FUNCTION. THEREAFTER, INSPECT AT

LEAST TWICE PER YEAR DURING WET WEATHER TO ENSURE THE SYSTEM IS DRAINING PROPERLY. CHECK FOR ACCUMULATION OF SEDIMENT AND PONDING WATER. IF PONDING WATER IS VISIBLE INSIDE THE SYSTEM FOR SEVERAL DAYS AFTER A STORM EVENT, NOTIFY THE ENGINEER FOR POSSIBLE REMEDIAL MEASURES. REMOVE SEDIMENT AS NECESSARY DURING CONSTRUCTION, WHILE THE SYSTEM IS DRY, AND AT LEAST ONCE EVERY FIVE YEARS AFTER CONSTRUCTION.

CULTEC UNITS (ROOF INFILTRATION):

- A. QUARTERLY INSPECTIONS DURING THE FIRST YEAR OF INSTALLATION AND ANNUALLY THEREAFTER.
- B. CHECK FOR OIL (USING A DIPSTICK TUBE).
- C. REMOVE OIL AND SEDIMENT THROUGH THE INSPECTION RISER PIPE ALTERNATIVELY, REMOVE FLOATABLES AND HYDROCARBONS THROUGH THE UNIT'S INSPECTION PORT.
- D. REMOVE ANY OIL SEPARATELY USING A SMALL PORTABLE PUMP.
- E. IF APPLICABLE, REMOVE THE SLUDGE FROM THE BOTTOM OF THE UNIT USING A VACUUM TRUCK.

DEEP SUMP CATCH BASINS:

FREQUENCY:

- -INSPECTION -FOUR TIMES PER YEAR
- -CLEANING FOUR TIMES PER YEAR OR WHENEVER THE DEPTH OF DEPOSITS IS GREATER THAN OR EQUAL TO ONE HALF THE DEPTH FROM THE BOTTOM INVERT OF THE LOWEST PIPE IN THE BASIN.

DESCRIPTION: BASINS ARE TO BE CLEANED FOUR TIMES PER YEAR OR WHEN THE DEPTH OF DEPOSITS IS GREATER THAN OR EQUAL TO ONE HALF THE DEPTH FROM THE BOTTOM OF THE SUMP TO THE INVERT OF THE LOWEST PIPE IN THE BASIN. THE OWNER WILL INSPECT SUMPS POST CONSTRUCTION A MINIMUM OF FOUR TIMES PER YEAR. PRECAUTIONS SHALL TAKE PLACE TO MAINTAIN THE INTEGRITY OF THE OIL TRAPPING HOODS DURING CLEANING. THE HOODS SHALL BE INSPECTED AND REPAIRED AS NECESSARY. ACCUMULATED HYDROCARBONS SHALL BE COLLECTED SEPARATELY FROM ACCUMULATED SEDIMENT. ALL MATERIAL SHALL BE DISPOSED OF IN ACCORDANCE WITH DEP REGULATIONS.

INSPECTIONS:

- -FRAME AND GRATE
- -INLET AND OUTLET CONDITION

- -CRACKS AND SETTLEMENT
- -JOINT FAILURE
- -LEAKING
- -SEDIMENT ACCUMULATION
- -OIL/GAS SHEEN IN WATER
- -CONDITION OF TRAP HOOD
- -GENERAL INSPECTION OF STRUCTURE



